



## An overview of the HIT-SI research program and its implications for magnetic fusion energy

Derek Sutherland, Tom Jarboe, and The HIT-SI Research Group University of Washington

36<sup>th</sup> Annual Fusion Power Associates Meeting – **Strategies to Fusion Power** December 16-17, 2015, Washington, D.C.

### Motivation

- Spheromaks configurations are attractive for fusion power applications.
- Previous spheromak experiments relied on coaxial helicity injection, which precluded good confinement during sustainment.
- Fully inductive, non-axisymmetric helicity injection may allow us to overcome the limitations of past spheromak experiments.
- Promising experimental results and an attractive reactor vision motivate continued exploration of this possible path to fusion power.



#### Outline

- Coaxial helicity injection NSTX and SSPX
- Overview of the HIT-SI experiment
- Motivating experimental results
- Leading theoretical explanation
- Reactor vision and comparisons
- Conclusions and next steps

### Coaxial helicity injection (CHI) has been used successfully on NSTX to aid in non-inductive startup



Figures: Raman, R., et al., Nucl. Fusion 53 (2013) 073017

- Reducing the need for inductive flux swing in an ST is important due to central solenoid flux-swing limitations.
- Biasing the lower divertor plates with ambient magnetic field from coil sets in NSTX allows for the injection of magnetic helicity.
- A ST plasma configuration is formed via CHI that is then augmented with other current drive methods to reach desired operating point, reducing or eliminating the need for a central solenoid.
- Demonstrated on HIT-II at the University of Washington and successfully scaled to NSTX.

Though CHI is useful on startup in NSTX, Cowling's theorem removes the possibility of a steady-state, axisymmetric dynamo of interest for reactor applications

- Cowling\* argued that it is impossible to have a steady-state axisymmetric MHD dynamo (sustain current on magnetic axis against resistive dissipation).
- At first glance, the requirement for non-axisymmetry seems to require the breaking of nested, closed-flux surfaces.
- In previous CHI-driven spheromak experiments, instability during sustainment was observed, leading to severe degradation in confinement quality.
- From these results, steady-state spheromak configurations did not look attractive for fusion power applications.

\*Cowling, T.G., *Monthly Notices of Royal Astronomical Society* **94** (1934) 39-48.

Previous spheromak experiments used coaxial helicity injection (CHI) for current drive (SSPX shown\*)



\*B. Hudson, et al., *Phys. Plasmas* **15** (2008) 056112.

## HIT-SI seeks to overcome the issues of CHI with fully-inductive, non-axisymmetric helicity injection

HIT-SI coils and geometry



Taylor state equilibrium  $\nabla \times \vec{B} = \lambda \vec{B}$ , where  $\lambda \equiv \mu_o \vec{J} / \vec{B}$ 



A spheromak forms after an ample amount of helicity is injected, and relaxation occurs. The spheromak is then sustained by continued injector operation.

transformer

# Record current gains are observed at higher injector frequencies

14.5 kHz results

68.5 kHz results



- Current amplification of 3.9 at high frequency, a new spheromak record.
- 90 kA of toroidal current at lower frequencies.
- Stable, sustained equilibria Ohmically heat to the beta limit, achieving the current drive goal of HIT-SI.

### The only significant magnetic fluctuations observed are those that are imposed after relaxation\*



Mode amplitudes vs time

Mode amplitudes minus the imposed perturbations vs time

n=1 amplitude and the injector current vs time

Toroidal current vs time

- During sustainment, the n = 1 component of the magnetic fields in the system is almost entirely imposed.
- HIT-SI is capable of testing MHD stability, which has been the problem with sustained spheromaks until now.

\*B.S. Victor, et al., *Physics of Plasmas* **21** (2014) 082504.

## HIT-SI sees a transition to higher $\beta$ and increased stability as $\omega_{inj}$ is increased\*



- Internal magnetic probes show larger Shafranov shift due to higher β (5% vs 25%) at high frequency.
- Centroid measurements at four toroidal locations show better symmetry and larger outward shift at high frequency.
- At high frequency, the imposed-fluctuations appear to be controlling the pressure driven modes (greater symmetry and running above  $\beta$  limit).

<sup>\*</sup>B.S. Victor, et al., *Physics of Plasmas* **21** (2014) 082504.

# Imposed-dynamo current drive (IDCD) is the leading theory to explain HIT-SI results

- IDCD\* requires driving the edge-λ higher than the spheromak λ, while imposing nonaxisymmetric, magnetic perturbations.
- The dynamo terms in Hall-MHD Generalized Ohm's Law leads to a dynamo electric field that drives current parallel to current.
- This dynamo electric field gives rise to an electrostatic field along the magnetic field that is able to drive current parallel to magnetic field.
- The dynamo electric field, by itself, does not sustain current parallel to B, complying with Cowling's theorem.\*\*

<sup>\*</sup>T.R. Jarboe, et al., Imposed-dynamo current drive, *Nuclear Fusion* **52** (2012) 083017.

\*\*T.R. Jarboe, B.A. Nelson, and D.A. Sutherland, *Phys. Plasmas* 22 (2015) 072503.



IDCD 2-step  $\lambda$  model

Using the IDCD model, the dynomak reactor study was conducted to determine what a eventual reactor based on the HIT-SI experiment may look like

- Due to the favorable results from the HIT-SI experiment, a reactor concept study was performed based on a scale-up of HIT-SI.
- Due to the lack of a TF coil, the overall engineering of the reactor concept is simpler and more compact than a tokamak or stellarator system.
- The reactor vision based on an imposed-dynamo driven spheromak is called the *dynomak* concept.



\* Extensive details and development path published in Fusion Engineering and Design:

Sutherland, D.A., et al., The dynomak: An advanced spheromak reactor concept with imposed-dynamo current drive and next-generation nuclear power technologies, *Fus. Eng. Design* **89** (2014) 412-425.

# The operating point of the dynomak reactor system

- 1 GWe scale fusion power plant based on a scale up of HIT-SI.
- Major radius of 3.75 m and a minor radius of 2.5 m.
- Tritium breeding ratio of 1.125 with un-enriched FLiBe.
- Total current drive power to sustain 42 MA toroidal plasma current is estimated from the IDCD model to be 58.5 MW.
- 41% experimental CD coupling efficiency used from HIT-SI experiment.

Parameter	Value
Major radius [m]	3.75
Aspect ratio	1.5
Toroidal I <sub>p</sub> [MA]	41.7
Number density [10 <sup>20</sup> m <sup>-3</sup> ]	1.5
Wall-averaged β [%]	16.6
Peak T <sub>e</sub> [keV]	20.0
Neutron wall loading	4.2
[MW m <sup>-2</sup> ]	
Tritium breeding ratio (TBR)	1.125
Current drive power [MW]	58.5
Blanket flow rate [m <sup>3</sup> s <sup>-1</sup> ]	5.2
Thermal power [MW]	2486
Electrical power [MW]	1000
Thermal efficiency [%]	<u>&gt;</u> 45
Global efficiency [%]	<u>&gt;</u> 40

### Dynomak reactor concept is attractive when compared to other DEMO fusion reactor concepts

Parameters	Compact Stellarator*	Tokamak*	Spherical Torus*	Dynomak
R <sub>o</sub> [m]	7.1	6.0	3.2	3.75
A = R <sub>o</sub> /a [m]	4.5	4.0	1.7	1.5
I <sub>p</sub> [MA]	3.3	11.6	26.2	41.7
P <sub>fusion</sub> [MW]	1794	2077	2290	1953
P <sub>aux</sub> [MW]	18	100	60	58.5
<b>Q</b> <sub>p</sub> - Plasma	100	20.8	38.2	33
<b>Q</b> <sub>e</sub> - Engineering	6.5	3.4	2.8	9.5
<w<sub>n&gt; [MW m<sup>-2</sup>]</w<sub>	2.8	3.0	3.4	4.2
P <sub>electric</sub> [MW]	1000	1000	1000	1000

\*J.E. Menard et al. **Prospects for pilot plants based on the tokamak, spherical tokamak, and stellarator**. *Nucl. Fusion* 51 (2011) 103014 (13pp)

#### IDCD must be demonstrated in a larger, highertemperature plasma

- IDCD has been demonstrated on the HIT-SI device successfully, but uncertainty lies in whether it will scale to reactor relevant plasmas.
- The next step of the development path (HIT-SIX) is devoted to answering this critical question.
- Currently, IDCD theory predicts successful scaling to reactor relevant plasmas, which must be demonstrated experimentally.

### IDCD must be compatible with good confinement quality at high temperature

- Evidence of pressure confinement on HIT-SI suggests that IDCD may be compatible with good confinement quality.
- We must ensure the good confinement resulting from axisymmetric flux surfaces is not severely degraded by the magnetic fluctuations required to maintain a flat- $\lambda$  profile for IDCD ( $\delta B_r/B \approx 10^{-4}$ ).
- This question will also be addressed in the HIT-SIX experiment as well.
- Should 100s of eV to 1 keV temperatures be reached, this is direct confirmation of high-temperature confinement with IDCD active.

The HIT-SIX experiment: Build a high-performance plasma experiment optimized for flat- $\lambda$  and impose sufficiently large magnetic fluctuations to maintain the profile.

- In maintaining a flat- $\lambda$  profile by applying sufficiently large magnetic perturbations, the free energy to drive instabilities is greatly reduced.
- In choosing a compact aspect ratio device, significant q-shear is still present to ensure good confinement characteristics → optimized flux conserver geometry.

Parameter	Value
R <sub>o</sub> [m]	0.85
a [m]	0.55
I <sub>p</sub> [MA]	1.35
T [keV]	0.5-1+
$eta_{wall}$ [%]	16
$ au_{pulse}$ [s]	2
Cost [\$M]	≈ 35

#### Conclusions and next steps

- The spheromak configuration may provide a path to fusion power.
- Have evidence of sustainment with confined pressure via nonaxisymmetric, inductive helicity injection without gross kink instabilities present.
- Imposed-dynamo current drive (IDCD) is the leading model of behavior in HIT-SI, and allows for the sustainment of current without breaking closed-flux surfaces.
- The dynomak, a compact-aspect-ratio reactor vision based on HIT-SI, has sufficient  $Q_E$ , high neutron wall loading (\$/m<sup>2</sup>), and relatively simple engineering requirements.
- The IDCD-driven spheromak is ready for a high-temperature test in the HIT-SIX experiment.
- Provided with a successful HIT-SIX experiment, the uncertainty in whether a spheromak could be a fusion relevant plasma configuration will be greatly reduced.

#### **Key References**

<sup>1</sup>T.R. Jarboe, et al., Imposed-dynamo current drive, *Nuclear Fusion* **52** (2012) 083017.

<sup>2</sup>B.S. Victor, et al., Sustained spheromaks with ideal n=1 kink stability and pressure confinement, *Physics of Plasmas* **21** (2014) 082504.

<sup>3</sup>D.A. Sutherland, et al., The dynomak: An advanced spheromak reactor concept with imposed-dynamo current drive and next-generation nuclear power technologies, *Fusion Engineering and Design* **89** (2014) *4*, 412-425.

<sup>4</sup>T.R. Jarboe, B.A. Nelson, and D.A. Sutherland, A mechanism for the dynamo terms to sustain closed-flux current, including helicity balance, by driving current which crosses the magnetic field, *Phys. Plasmas* **22** (2015) 072503.

### Backup Slides

#### Helicity injection fundamentally allows for the steadystate sustainment of a plasma configuration

• Helicity injection is described by the following expression:

$$\frac{dK}{dt} = 2 \int_{V} \vec{E} \cdot \vec{B} \, dV$$

• Line integrating along the electric field linking magnetic flux provides another helicity injection equation form:

$$\frac{dK}{dt} = 2V\psi$$

- Thus, applying a voltage that links magnetic flux will lead to helicity injection into a plasma configuration.
- The central solenoid is a helicity injector in a tokamak.

$$\frac{dK}{dt} = 2V_{ohmic}\phi_{tor}$$

Thus, helicity injection is closely linked with current drive.

#### Key assumptions in the analysis of IDCD\*

- An equilibrium and perturbative component of relevant quantities (e.g. J, B) are assumed.
- A n = 1, m > 0 magnetic perturbation is imposed and is frozen into the electron fluid.
- In the lab frame, the plasma is at rest (i.e. the plasma velocity is zero).
- In the lab frame, the electron fluid (which carries the current) is moving with a speed  $V_o = J_o/ne$  since ions are assumed to be at rest.
- The computations and pictures presented are done from the perturbation frame of reference (i.e. the plasma velocity is non-zero).





\* T.R. Jarboe, B.A. Nelson, and D.A. Sutherland, Phys. Plasmas 22 (2015) 072503.

# The dynamo electric field drives current parallel to current

Assume  $\vec{J} = \vec{J_o} + \delta \vec{j}$ ,  $\vec{V} = \vec{V_o}$ ,  $\vec{B} = \vec{B_o} + \delta \vec{b}$ , and that perturbation is small compared to equilibrium field.

Generalized Hall-MHD Ohm's Law

$$\vec{E} = -\vec{V} \times \vec{B} + \frac{\vec{J} \times \vec{B}}{ne} + \eta \vec{J}$$

Component of dynamo terms (Lorentz + Hall) in direction of perturbative portion of total current  $\vec{J}$ .

$$-\left[\overline{V_o} \times \left(\overline{B_o} + \delta \vec{b}\right)\right] \cdot \frac{\left(\overline{J_o} + \delta \vec{j}\right)}{\left|\overline{J_o} + \delta \vec{j}\right|} + \frac{\left(\overline{J_o} + \delta \vec{j}\right) \times \left(\overline{B_o} + \delta \vec{b}\right)}{ne} \cdot \frac{\left(\overline{J_o} + \delta \vec{j}\right)}{\left|\overline{J_o} + \delta \vec{j}\right|}$$
$$= \frac{-\left(\overline{V_o} \times \delta \vec{b}\right) \cdot \delta \vec{j}}{\left|\overline{J_o} + \delta \vec{j}\right|} = \frac{\left(\delta \vec{b} \times \overline{V_o}\right) \cdot \delta \vec{j}}{\left|\overline{J_o} + \delta \vec{j}\right|} + O(\delta^2)$$

A toroidal view of imposed magnetic perturbations and current crossing the magnetic field



### This cartoon shows the critical ingredients for IDCD, magnetic perturbations and electron flow.

- The key acting dynamo term is  $\delta \vec{b} \times \vec{V_o}$ , which requires an electron flow velocity and a perturbative magnetic field.
- The dynamo electric field,  $\delta \vec{b} \times \vec{V_o}$  has a finite component parallel to  $\vec{J}$ , which crosses the magnetic field
- Thus, the dynamo drives current parallel to current.
- A space charge is created by the dynamo electric field, which produces a electrostatic  $E_V$  is able to drive current parallel to B.
- This electrostatic  $\vec{E}_V$  field dotted with  $\overrightarrow{B_o}$  also provides helicity injection.
- Thus, the electrostatic  $\vec{E}_V$  field drives current parallel to  $\vec{B_o}$ , but the dynamo electric field **does not**.
- Therefore, there is no need for the gross breaking of flux surfaces for steadystate dynamo current drive with the IDCD conditions met.

#### Proposed development path and goals

Current ——→ stage	<b>HIT-SI3</b> : Advance understanding of injector physics, plasma rotation, power coupling.
Next→ step	<b>HIT-SIX</b> : IDCD scaling confirmation, confinement development, copper coils, 1 keV, 2 second pulse.
Optional:	<b>HIT-PoP</b> : Confinement development, copper coils, 3 keV, 10 second pulse.
	<b>HIT-PX</b> : Add HTSC magnets, steady-state operation, 8 keV, water cooling.
Active → nuclear site	<b>HIT-FNSF</b> : Add tritium, FLiBe coolant, confirm TBR, 15 keV, materials testing.
Time	<b>HIT-Pilot</b> : Add SC-CO <sub>2</sub> secondary cycle, 20 keV, electricity generation. (~ 20-250 MWe, depending on confinement quality)

### An estimated overnight capital cost breakdown of the dynomak reactor concept

Component(s)	Est. Cost (\$M)
Land and land rights <sup>*</sup>	17.7
Structures and site facilities <sup>*</sup>	424.3
Reactor structural supports	45.0
First wall and blanket	60.0
$ZrH_2$ neutron shielding	267.4
IDCD and feedback systems	38.0
Copper flux exclusion coils	<b>38.5</b>
Pumping and fueling systems	91.7
Tritium processing plant	154.0
Biological containment	50.0
Superconducting coil system	216.0
Supercritical $CO_2$ cycle	293.0
Unit direct cost	1696
Construction services and equipment <sup>*</sup>	288
Home office engineering and services <sup>*</sup>	132
Field office engineering and services <sup>*</sup>	132
Owner's cost*	465
Unit overnight capital cost	2713

\*Asterisks indicate inflation adjusted figures from ARIES-AT.

#### The dynomak reactor concept is costcompetitive with conventional energy sources

Energy source	\$ (USD) for 1 GWe
Coal	$\geq$ 2.8 billion
Natural gas + No CO <sub>2</sub> capture	$\leq$ 1 billion
Natural gas + CO <sub>2</sub> capture	$\geq$ 1.5 billion
Gen III+ nuclear plant	> 3-4 billion
Dynomak reactor concept	$\approx$ 2.7 billion

Schlissel, D. et al. Coal-Fire Power Plant Construction Costs, Synapse Energy Economics Inc., Cambridge, MA. July 2008. <u>www.synapse-energy.com</u>

Schlissel, D. and Biewald, B. Nuclear Power Plant Construction Costs. *Synapse Energy Economics Inc.*, Cambridge, MA. July 2008. www.synapse-energy.com

Black, J. et al., Cost and Performance Baseline for Fossil Energy Plants, Volume 1: Bituminous Coal and Natural Gas to Electricity. *National Energy Technology Laboratory*, sponsored by U.S. DOE, November 2011.

**Updated Capital Cost Estimates for Electricity Generation Plants**, U.S. Energy Information Administration: Independent Statistics and Analysis, U.S. Department of Energy, November 2010.

## In summary, the successes of the HIT-SI research program

- Produced sustained kink-stable spheromaks with imposed-dynamo current drive (IDCD).
- Produced sustained spheromaks with pressure confinement.
- Imposed magnetic fluctuations required for IDCD appear compatible with sufficient confinement, likely due to plasma stability.
- Published an IDCD-driven spheromak (dynomak) concept study that is cost competitive.



The HIT-SI3 experiment, an upgrade of HIT-SI.

### NIMROD simulations are approaching validation at low injector frequency, and are underway at high frequency



- NIMROD simulations indicate pressure confinement and better toroidal symmetry at higher frequencies ( $f_{inj} > 40$  kHz).
- Validation has been achieved with the magnetic portion of the simulation at low frequency.
- High frequency validation is underway.