

ITER RWM benchmarking  
VALEN modeling results  
6th ITPA MHD topical group meeting

Tarragona, Spain 4 July 2005

Presented by J. Bialek

Columbia University

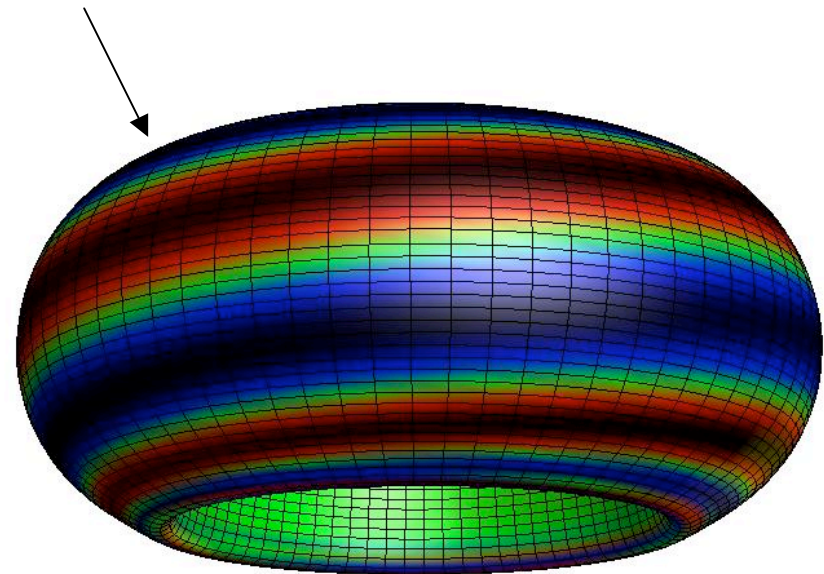
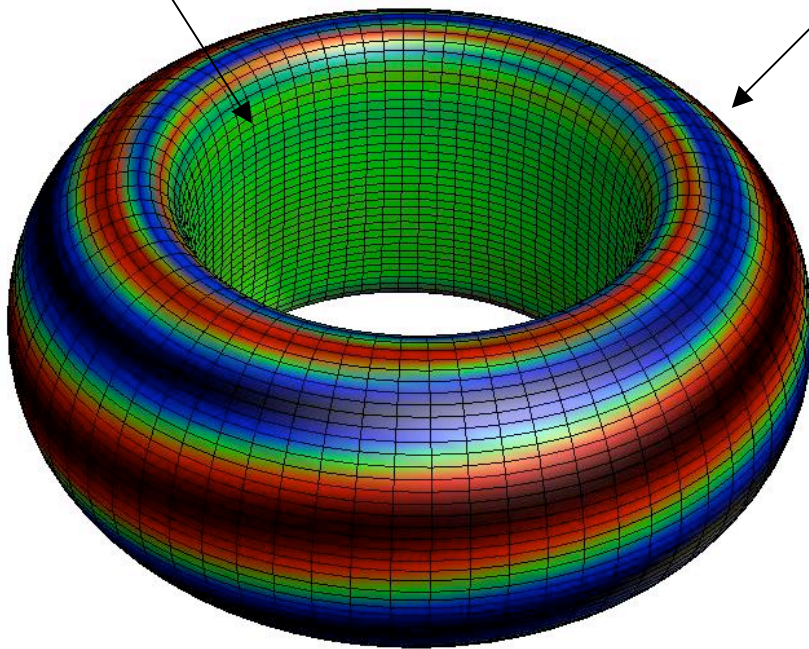
# outline

- RWM mode from CHEASE / DCON
- Benchmarking techniques and models
  - Current control with continuous external coil system
  - Voltage control with 6 coil external coil system
  - Effect of blanket modules
- Extended analysis, interior RWM coils with blanket modules, using voltage control
- summary

CHEASE equilibria for scenario 4 used in VALEN computations,  
the  $n=1$  DCON B-normal distribution ( $B_n$ ) on the plasma surface  
is shown below,  $B_n$  &  $\square W$  are used as VALEN input,  
Color scale: from dark red, to green ( approx zero ) to dark blue.

Field perturbation on inside  
( small R ) is not important

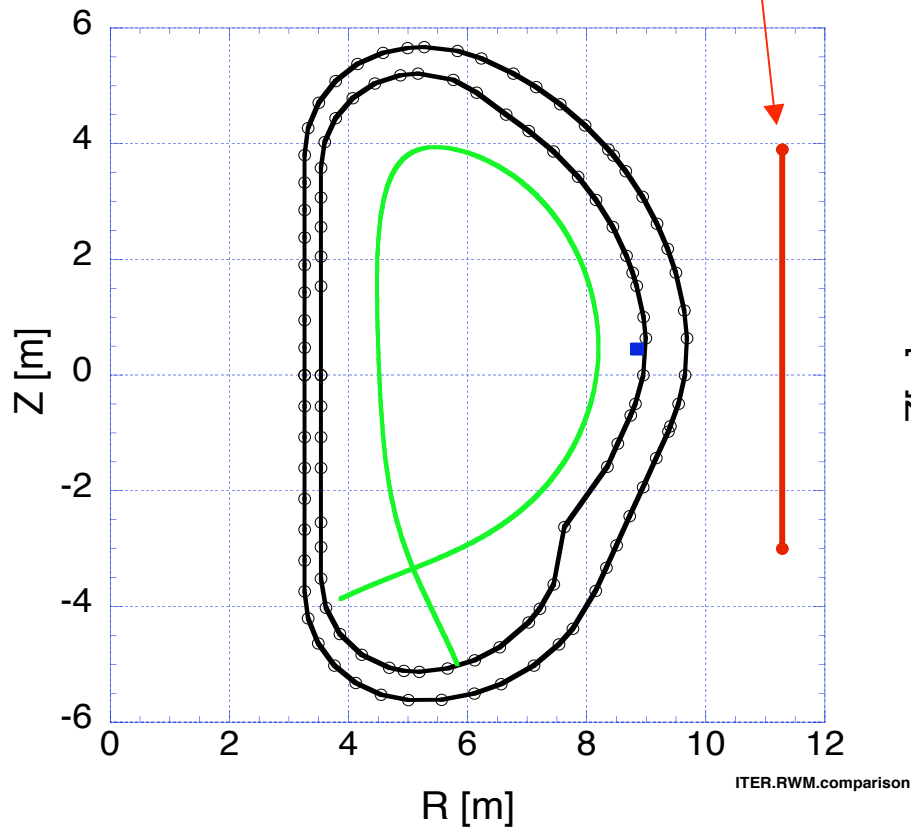
Dominant field perturbation  
on outside ( large R ) of plasma



## Benchmarking model

**continuous** external RWM coil  
axisymmetric VV  
**no** blanket modules

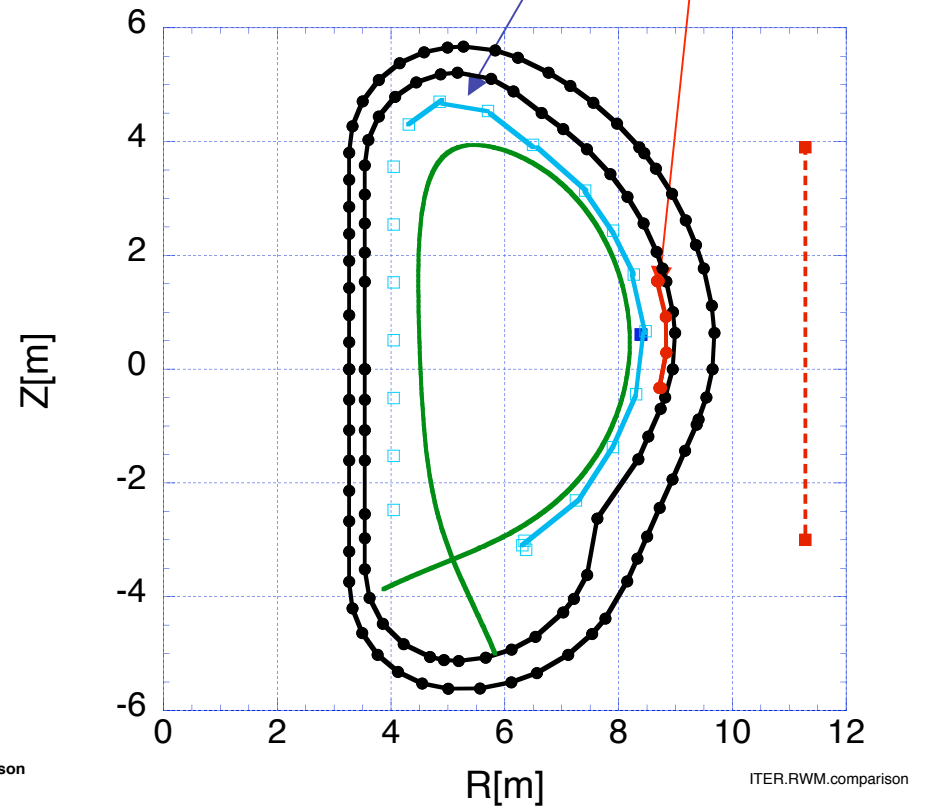
ITER RWM benchmarking  
**plasma**, walls, **control coils**,  
& **Bp** sensor



## Extended ITER model

**discrete** interior RWM coils  
penetrations in VV  
segmented blanket modules

extended ITER RWM analysis  
**plasma**, walls, **control coils**,  
**blanket modules**, & **Bp** sensors



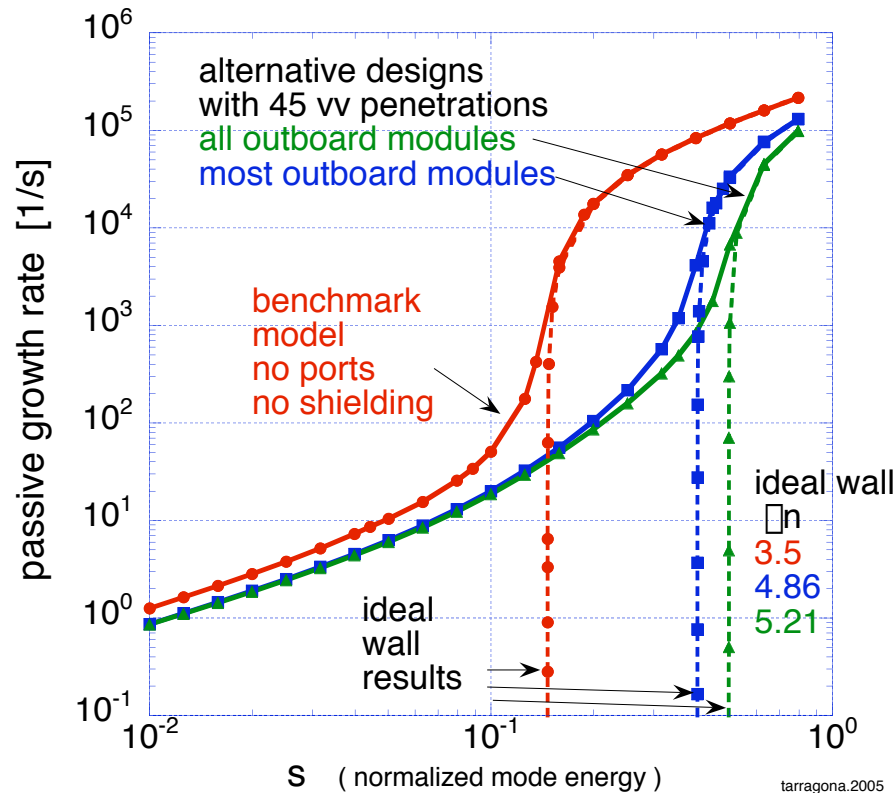
# VALEN calculation of ITER passive RWM growth rates

High conductivity wall allows estimate of ideal wall  $\bar{\kappa}_n$  limit

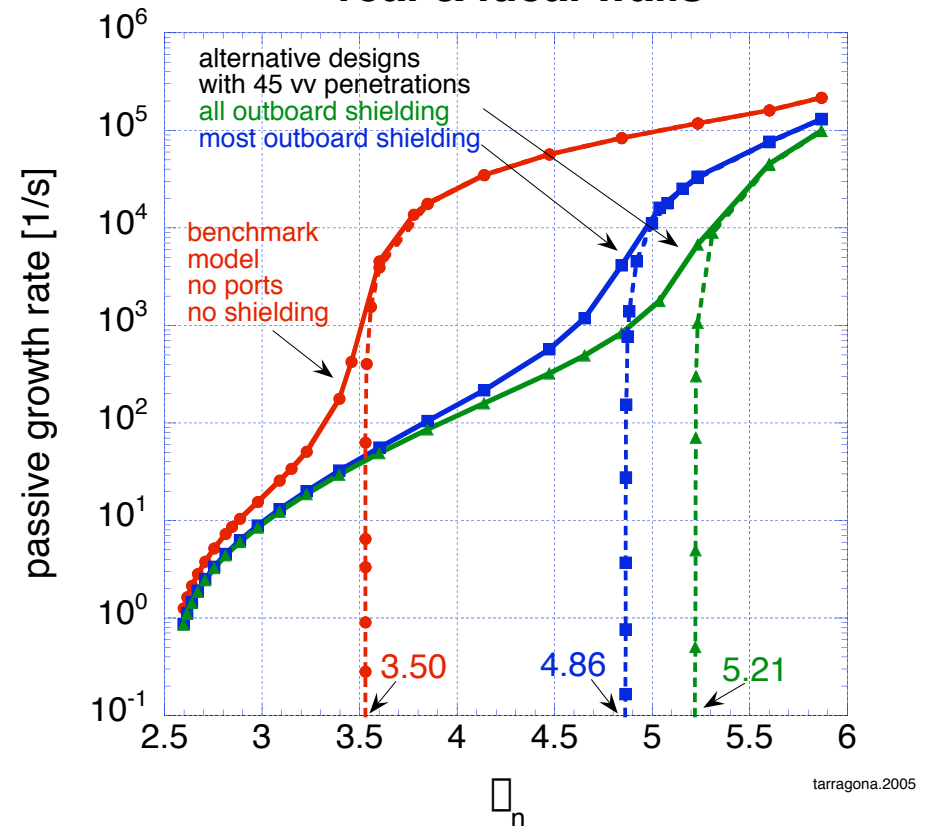
No wall and ideal wall  $\bar{\kappa}_n$  limit define  $C_{\bar{\kappa}}$  scale

no wall  $\bar{\kappa}_n$  limit = 2.52

**VALEN**  
passive growth rates  
real & ideal walls



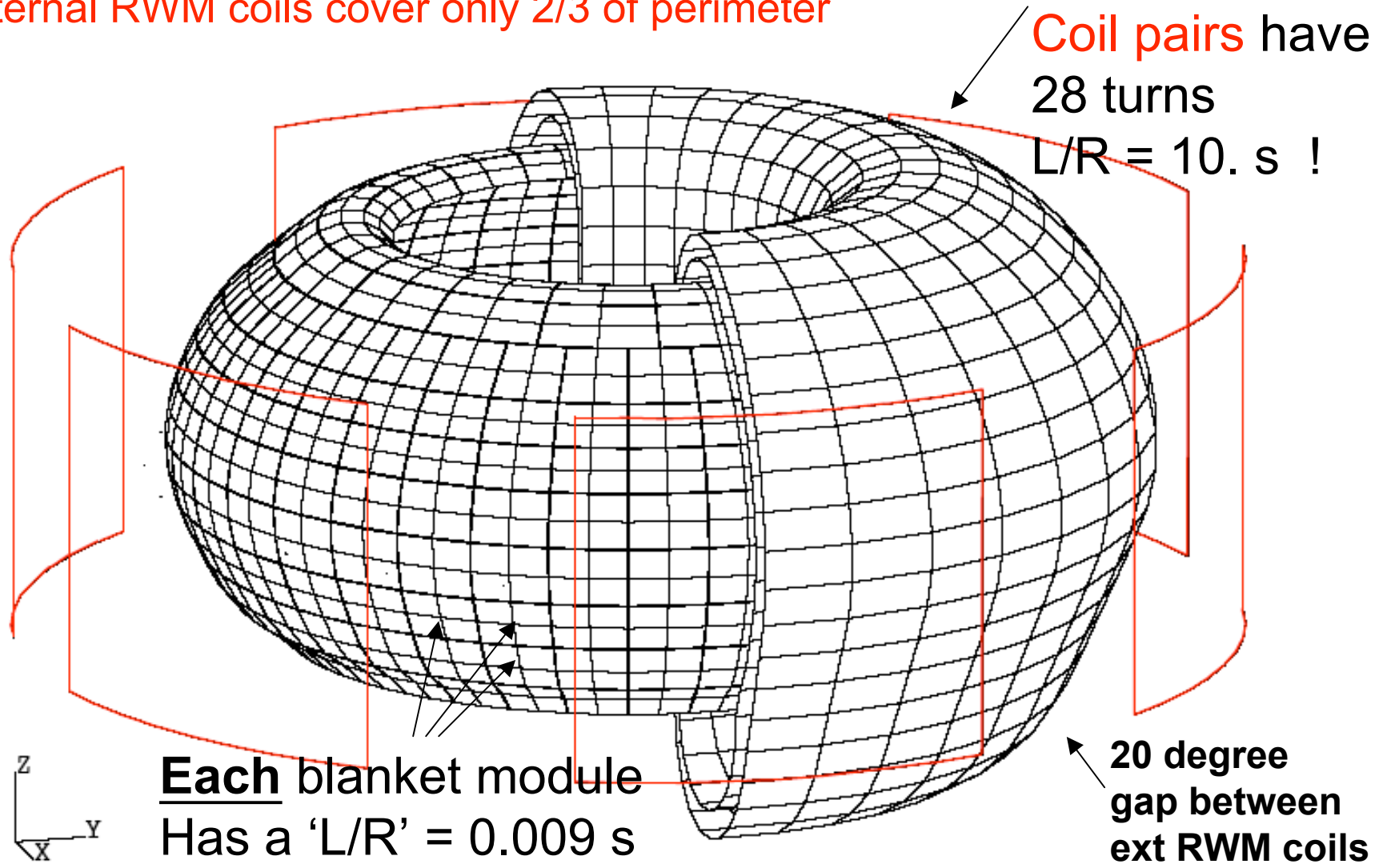
**VALEN**  
passive growth rates  
real & ideal walls



# ITER baseline external RWM coils shown

Cut away view of axisymmetric vacuum vessel  
VALEN blanket modules visible without VV

External RWM coils cover only 2/3 of perimeter



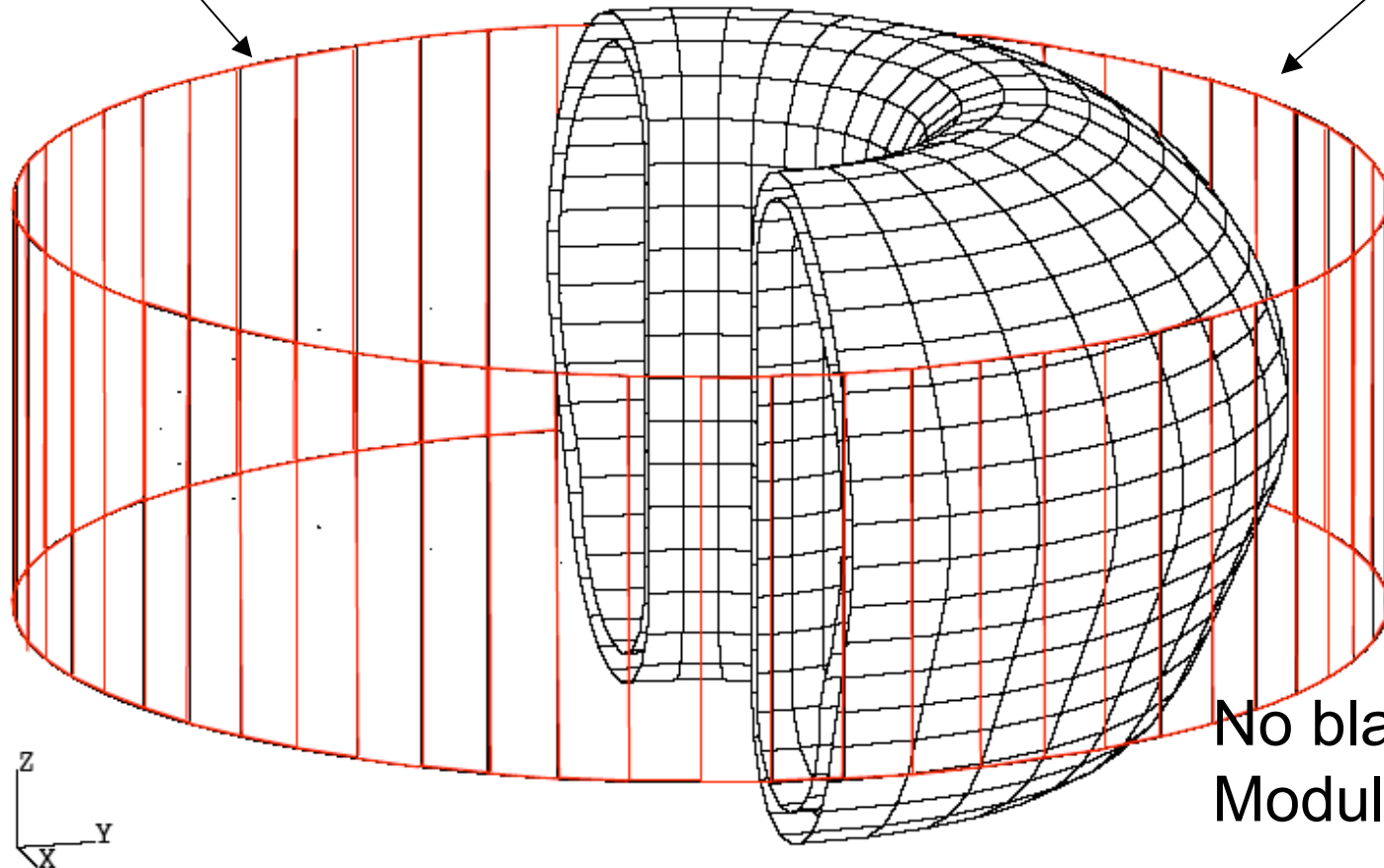
# VALEN benchmark RWM coil and cut away view of axisymmetric vacuum vessel model

Continuous RWM coils system shown

60 picture frame coils with no overlap. The total gap between all Coils = 1 degree

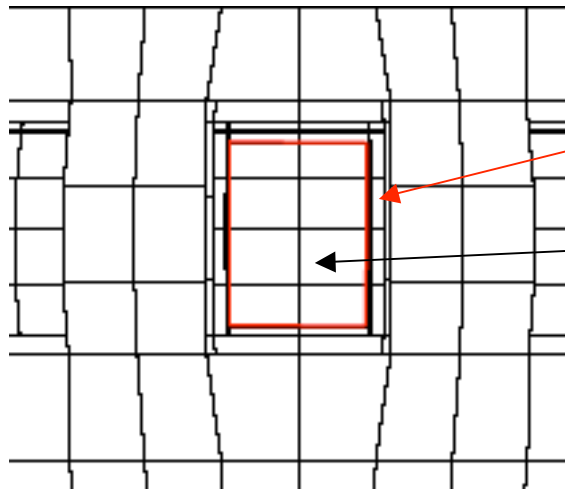
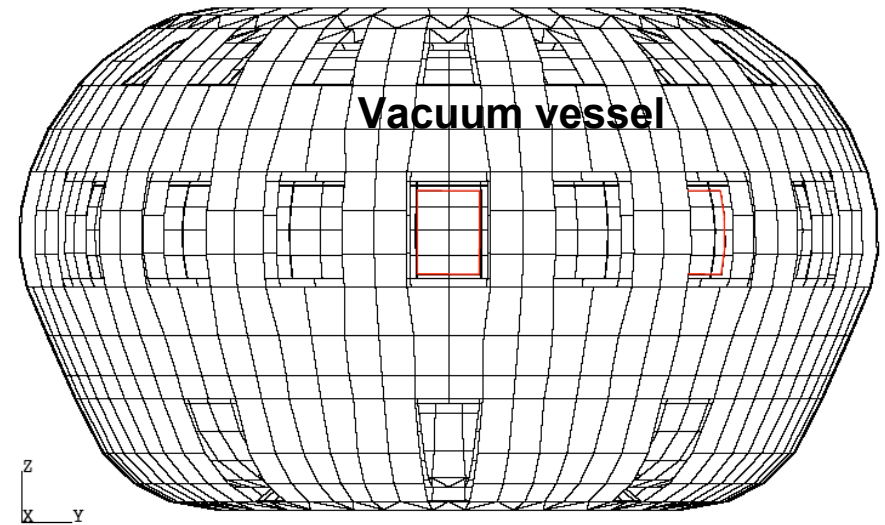
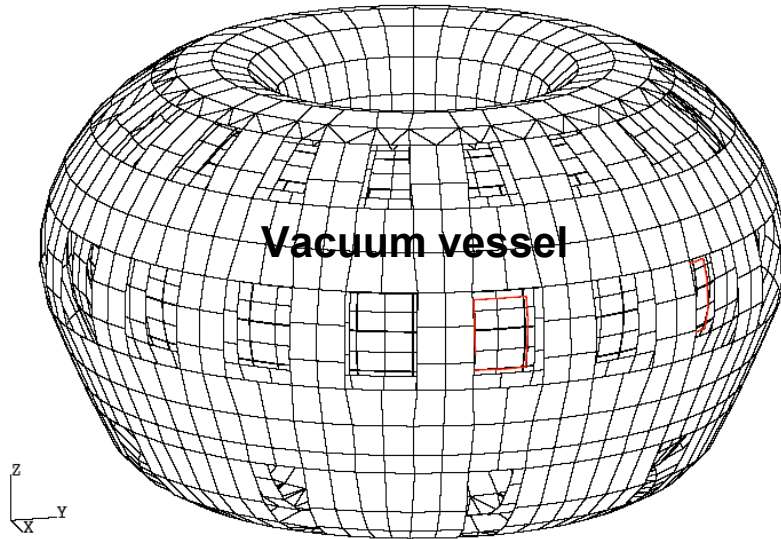
Approximate current control !

Each coil has a different current, this results in a  $n=1$  distribution of current



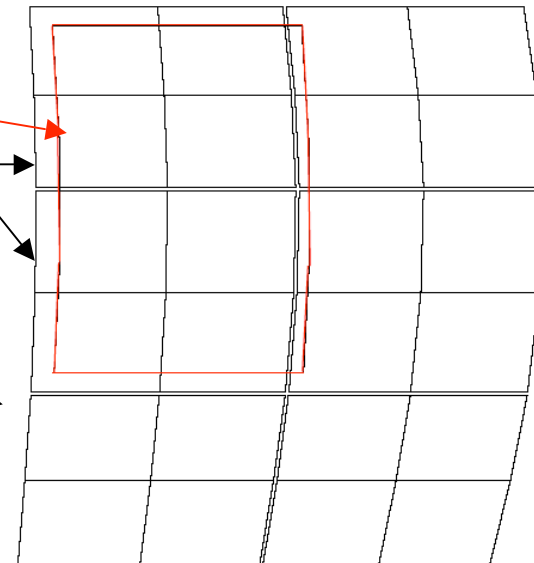
No blanket Modules !

Extended ITER models use internal coils and have penetrations in the vacuum vessel



**Internal coil**  
behind blanket  
modules

**Gaps**  
between  
blanket  
modules





## VALEN benchmark model approximates MARS continuous RWM control coil

- axisymmetric walls
- ignore blanket modules
- continuous external RWM coil
- approximate current control in feedback logic

VALEN implements feedback via voltage control. Sensor signals to control logic determines the voltage applied to the RWM coils.

### Technique:

#### RWM control coils

Model continuous RWM coil system by many small (non overlapping) 'picture frame' coils

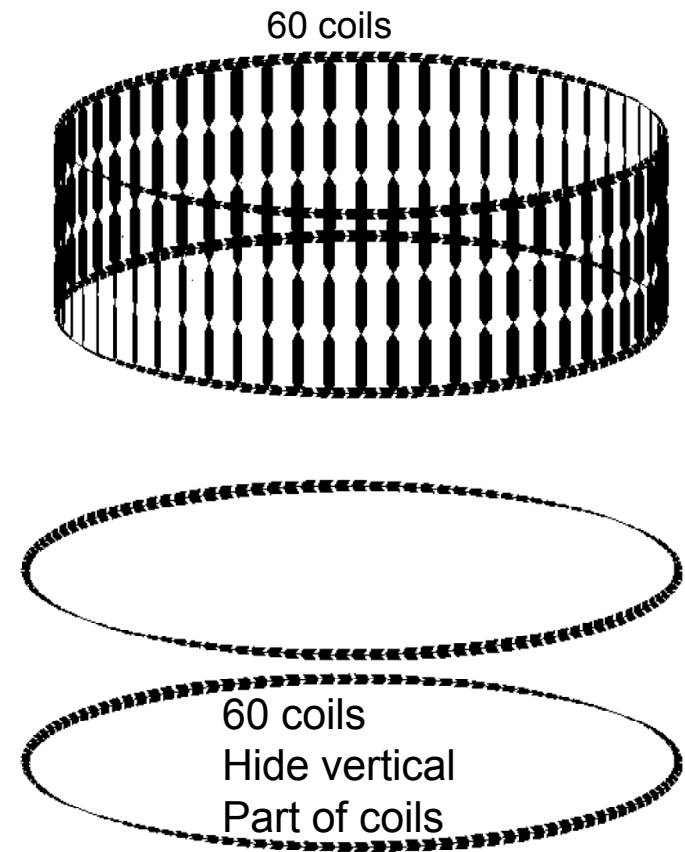
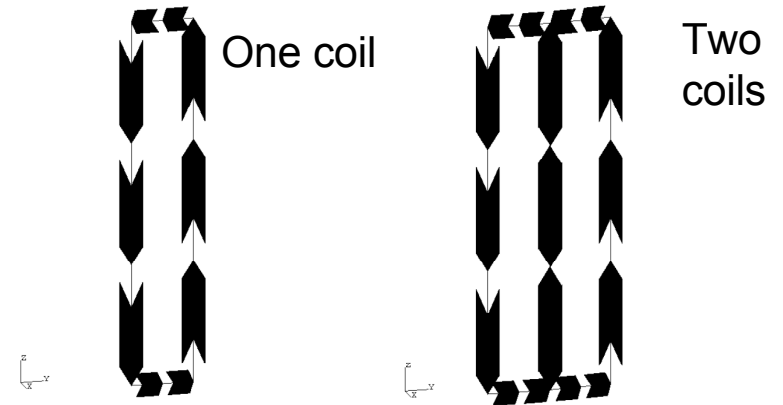
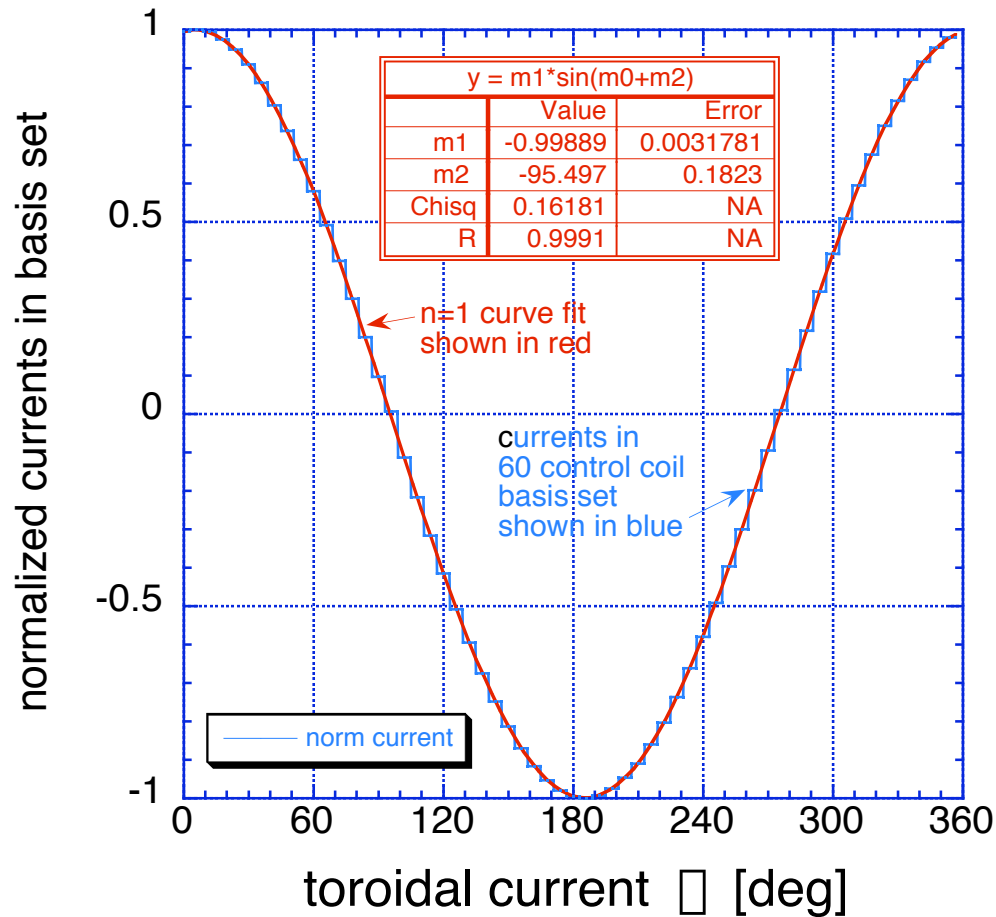
### Technique:

#### current control

Make each sub-coil have fast (L/R) time constant so that requested coil current is obtained with minimal delay

# VALEN can approximate A continuous RWM coil

**VALEN approximation  
to n=1 current distribution  
in 60 control coil basis set**



## Mode control feedback in VALEN RWM model

Sensors track  $B_p$  inside VV & have area =  $10^{-4} \text{ m}^2$

VALEN solution variables are currents in model

i.e.,  $\{I(t)\}$  and  $\{dI/dt\}$  for each wall element & coil & plasma

**Voltage control** is used to specify feed back in VALEN:

$$\text{sensors: } \{ \square_s(t) \} = [M_{sI}] \{ I(t) \} \quad \text{and} \quad \{ -\dot{\square}_s(t) \} = \square [M_{sI}] \{ \dot{I}(t) \}$$

$$\text{voltage feedback: } V_{cc}(t) = \square G_p \square_s(t) + \square G_d (\square \dot{\square}_s(t))$$

### To approximate ideal current control

we adjusted  $R_{cc}$  so  $L_{cc}/R_{cc}$  of coil is fast.

We keep  $L_{cc}$  fixed and increase  $R_{cc}$ .

Studied  $L_{cc}/R_{cc} < 1\text{ms}$  and  $< 1 \mu\text{s}$  !

Each increase in  $R_{cc}$  required an

increase in gain to match performance.

We obtain requested current  $= V_{cc}/R_{cc}$  in  $\sim L_{cc}/R_{cc}$  sec

### We also examine voltage control with actual external coil parameters, i.e.,

$$\begin{aligned} L/R|_{cc(\text{pairs})} &= 39.2\text{e-3H} / 3.92\text{e-3}\square \\ &= 10. \text{ s} \end{aligned}$$

# VALEN RWM dispersion relation

## For ITER benchmark model with fast $L/R < 1 \mu\text{s}$

### [approximates current control]

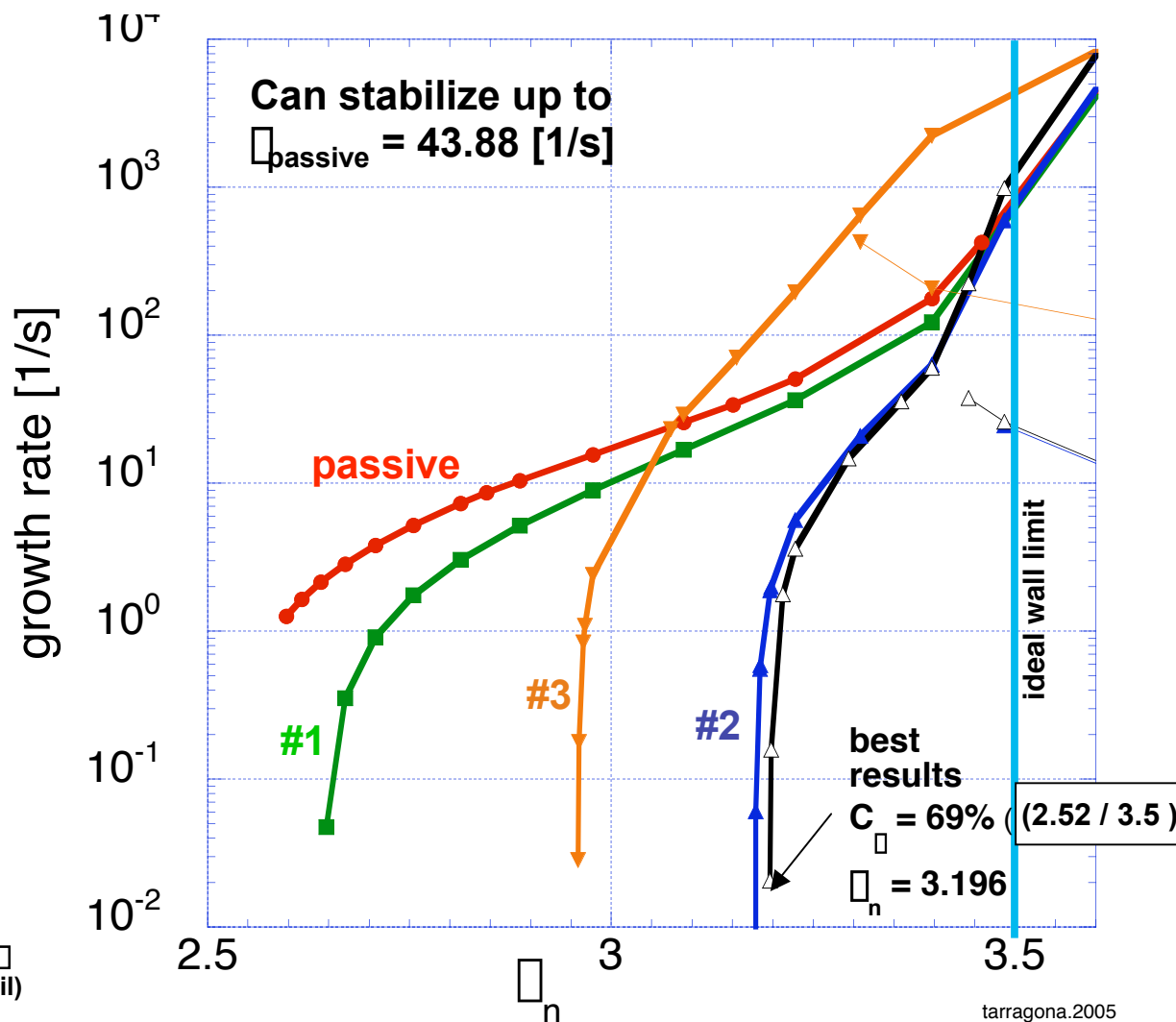
**#1  $G_p = 10^{12} [\text{v/w}]$  (real)**  
 @ 1 gauss  
 $I_{cc} = 0.518 \text{ KA}$

**#2  $G_p = 10^{13}$  (complex c. pairs)**  
 @ 1 gauss  
 $I_{cc} = 5.18 \text{ KA}$

**#3  $G_p = 10^{14}$  (complex c. pairs)**  
 @ 1 gauss  
 $I_{cc} = 51.8 \text{ KA}$

**Best results use**  
 $G_p/G_d = 10^3$

(  $L/R = 16.8 \mu\text{H}/19.29 \mu\text{s}$   
 $= 0.87 \mu\text{s}$  for each coil)

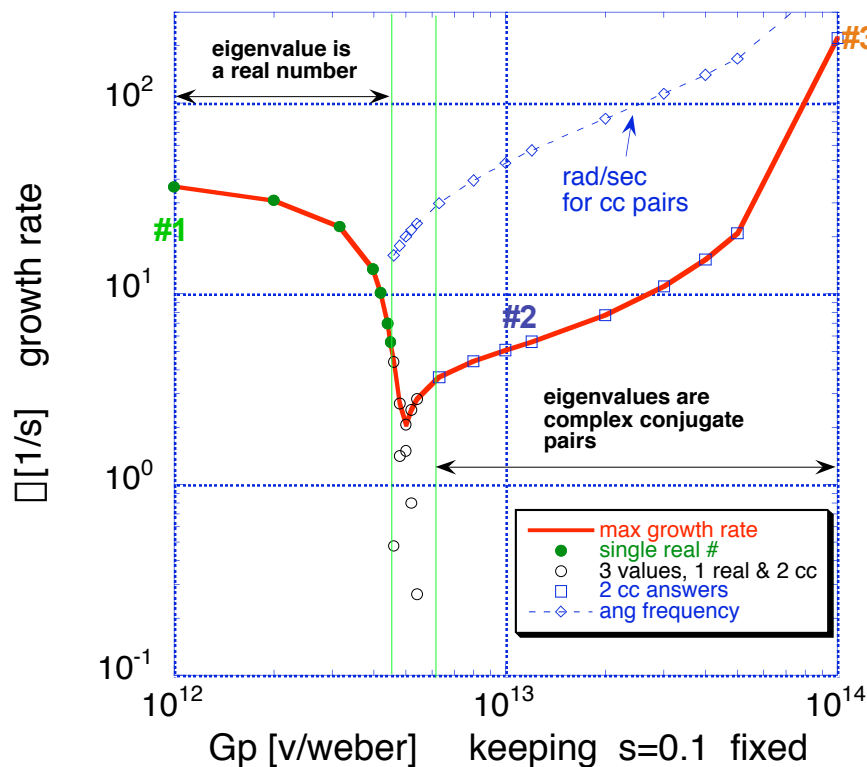


# Investigate RWM feedback performance limits as gain applied to sensor flux & sensor voltage is varied

Look at  $\beta_n = 3.22$ ,  $C_\beta = 72\%$  (2.52 / 3.50), (or  $s=0.1$ )

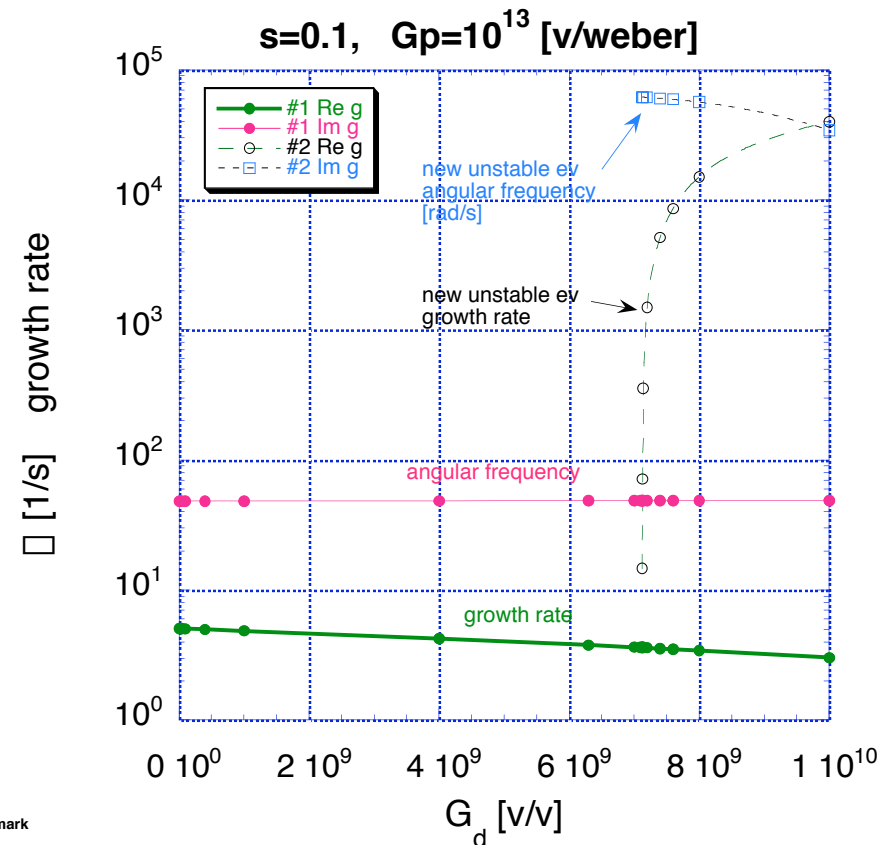
Can not stabilize this growth rate ( $\beta_{\text{passive}} = 50.8$  [1/s])

VALEN results  
ITER RWM benchmarking  
fine scan in  $G_p$



ITER.s.beta.benchmark

VALEN results  
ITER RWM benchmarking model  
scan in  $G_d$  with fixed 's' &  $G_p$

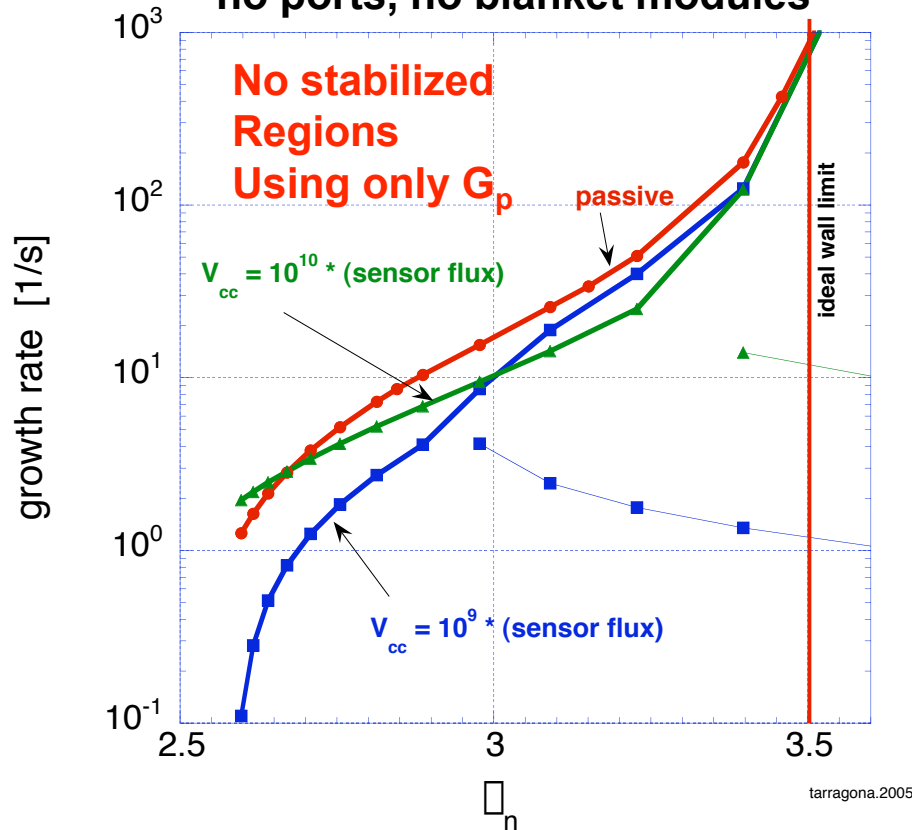


# Performance with 6 external coils with 10 s time constants

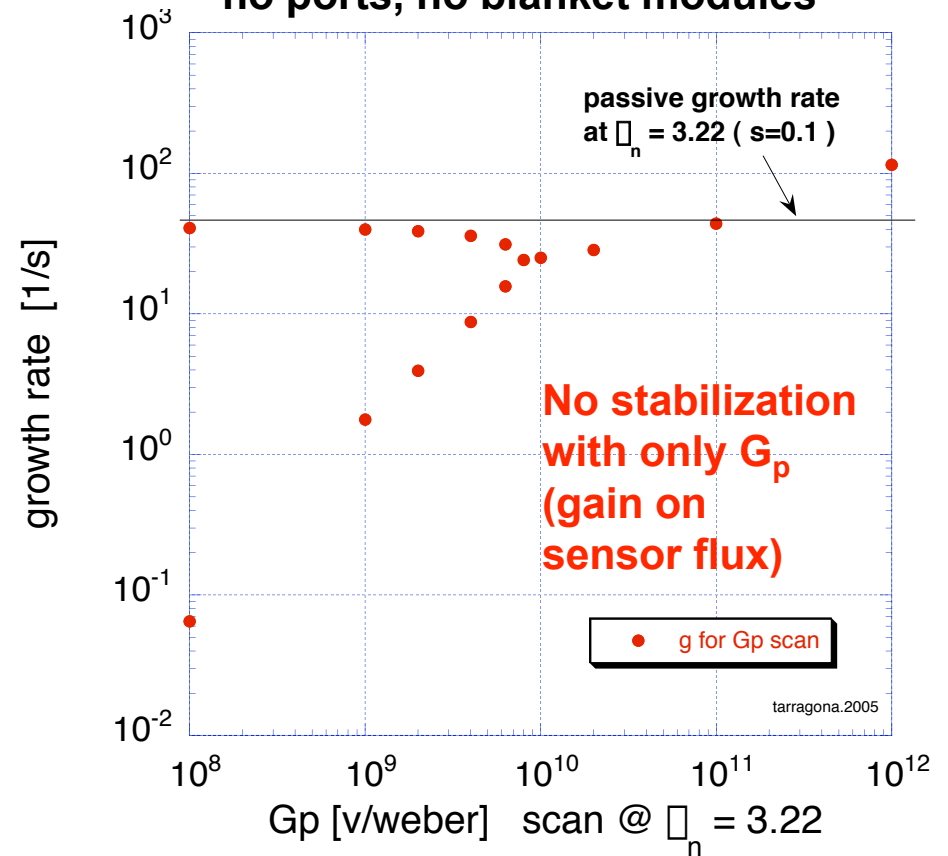
## Can not stabilize RWM with only $G_p$ [v/w] in ITER Baseline Design

$$V_{cc} = (\text{gain} * \text{sensor flux}) \quad \text{still no blanket modules}$$

only  $V_{cc} = \text{sensor flux} * \text{gain}$   
 VALEN results voltage control  
 6 external coils with  $L/R = 10. \text{ s}$   
 no ports, no blanket modules



scan in  $G_p$  (proportional gain)  
 VALEN results voltage control  
 6 external coils with  $L/R = 10. \text{ S}$   
 no ports, no blanket modules

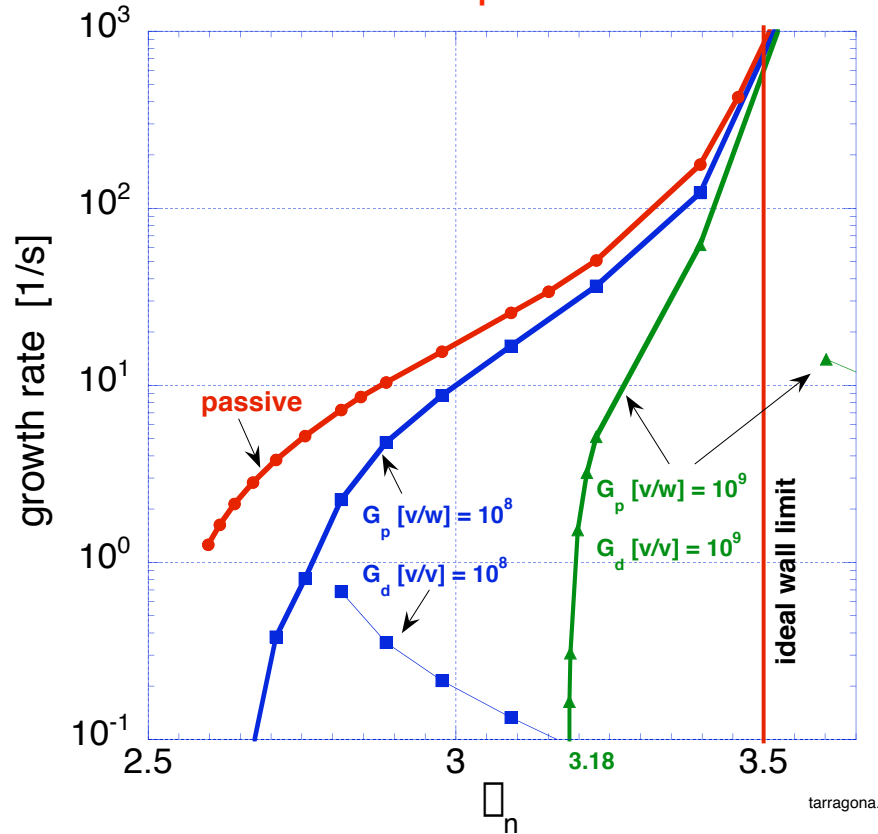


# Performance with 6 external coils with 10 s time constants

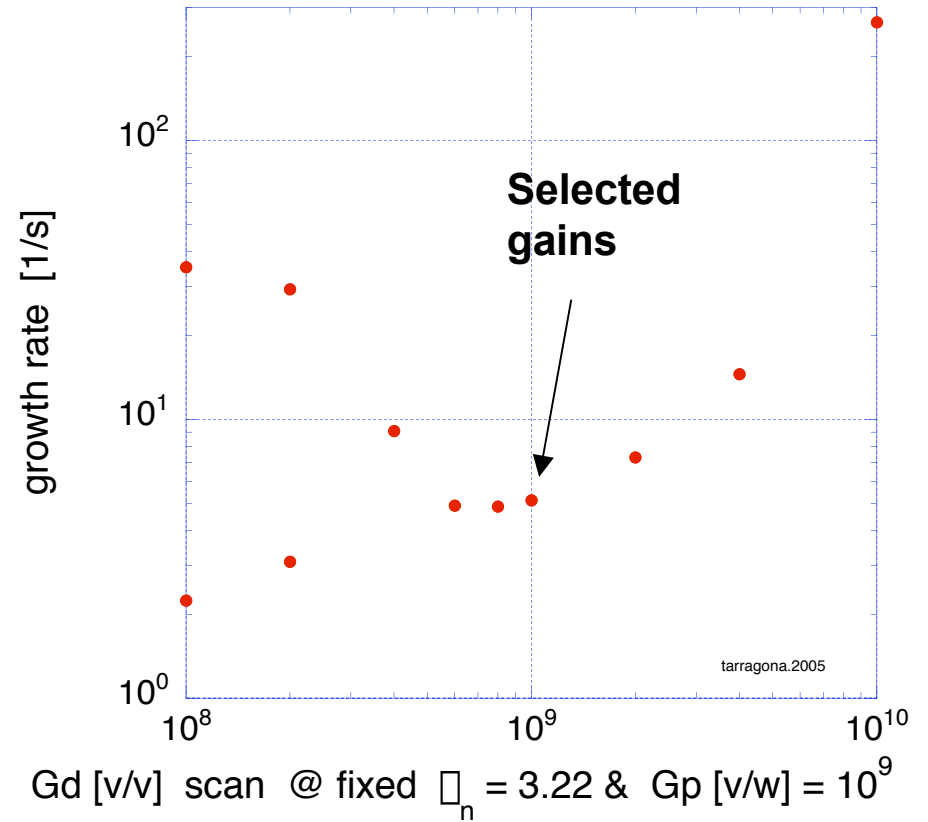
## Investigate combined $G_p$ [v/w] & $G_d$ [v/v] gain

$V_{cc} = G_p \times (\text{sensor flux}) + G_d \times (\text{sensor voltage})$ , still no blanket modules

Stabilized to  $\beta_n = 3.18$   
When both  $G_p$  &  $G_d$  used



Could not reach  
 $\beta_n = 3.22$  with different  $G_d$



$G_d$  [v/v] scan @ fixed  $\beta_n = 3.22$  &  $G_p$  [v/w] = 10<sup>9</sup>

# Performance with 6 external coils with 10 s time constants

Same  $G_p$  &  $G_d$ , **add blanket modules to model** ( no ports)

Gain settings:

$$G_p = 10^9 \text{ [v/w]}$$

$$G_d = 10^9 \text{ [v/v]}$$

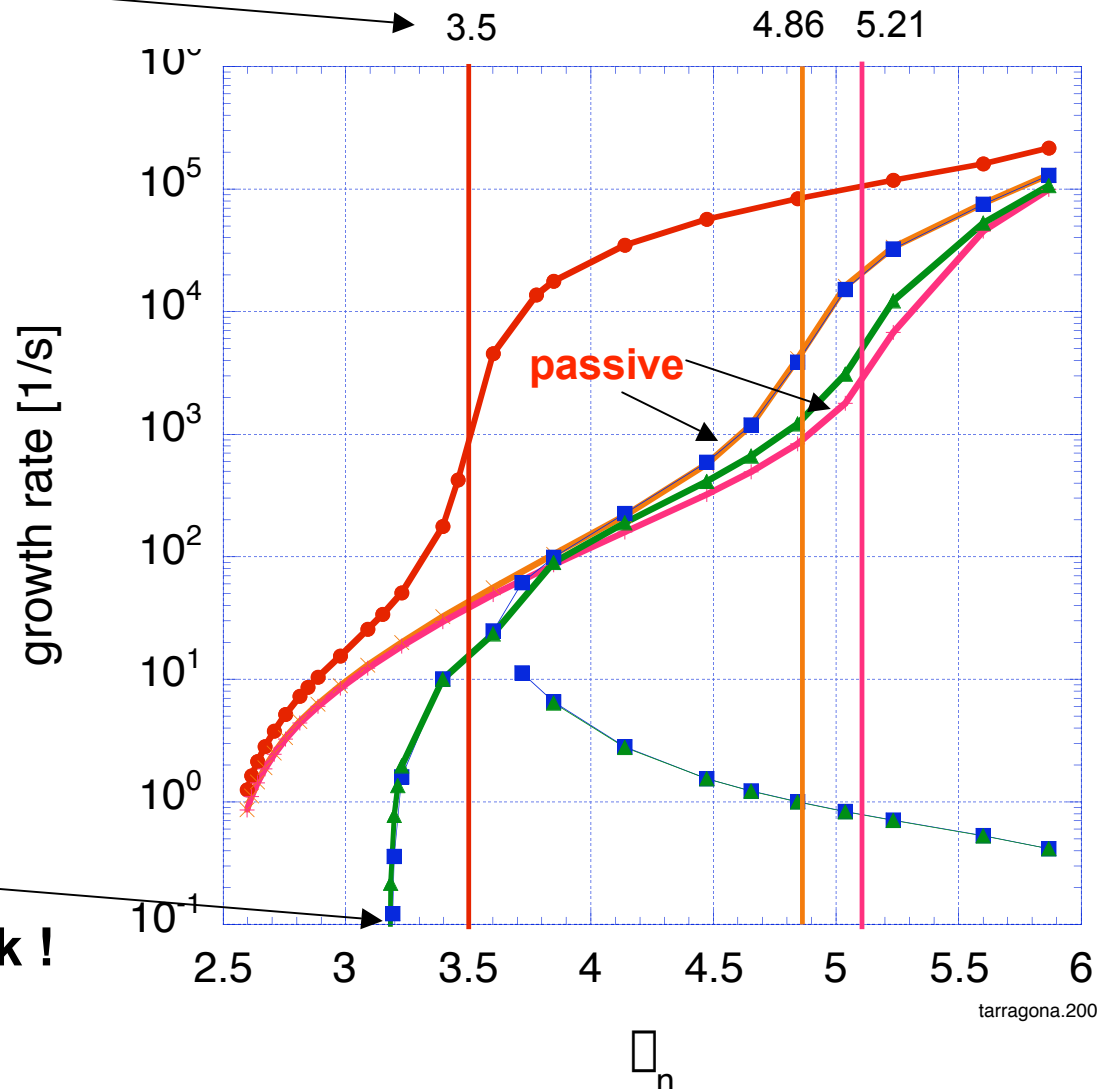
Best  $\beta_n = 3.177$   
( with all blanket modules)

Best  $\beta_n = 3.189$   
( with blanket modules removed from mid plane ports)

Best Results

About same as benchmark !

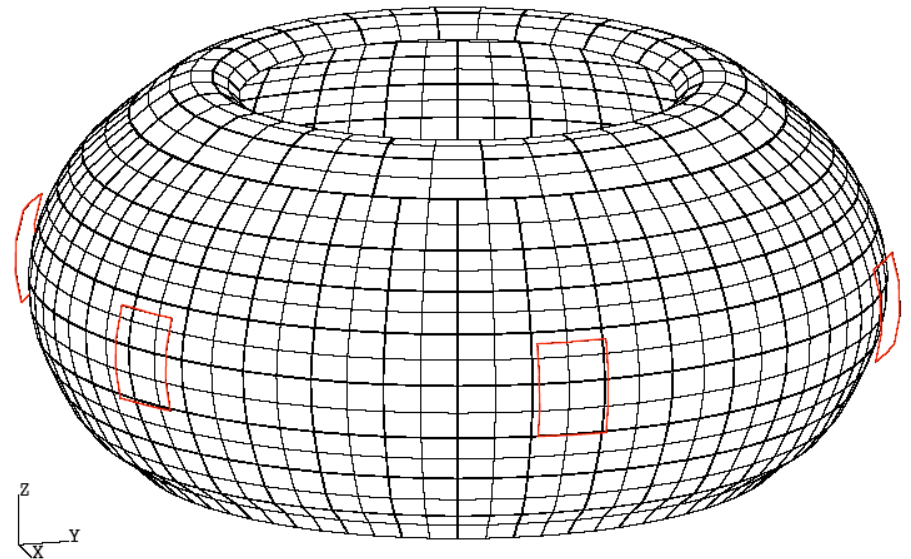
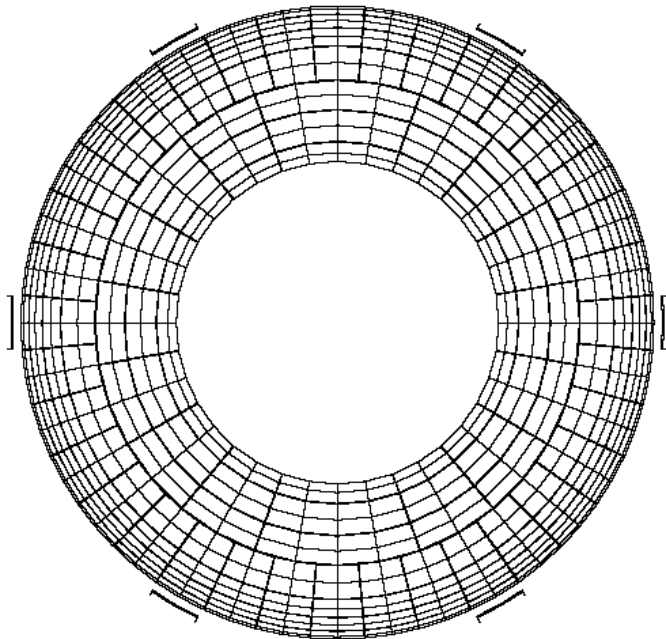
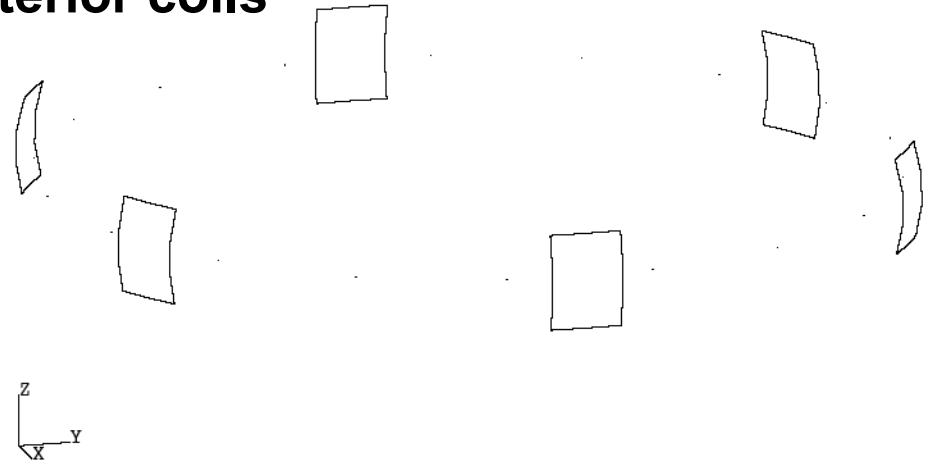
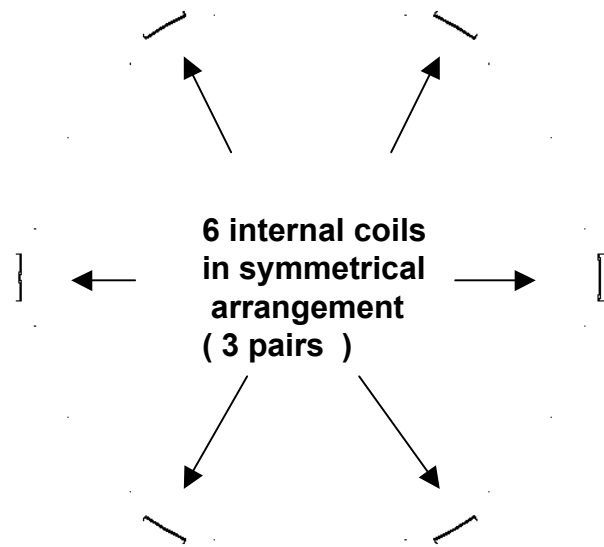
Recall ideal wall  $\beta_n$  limits





## Extended ITER RWM analysis

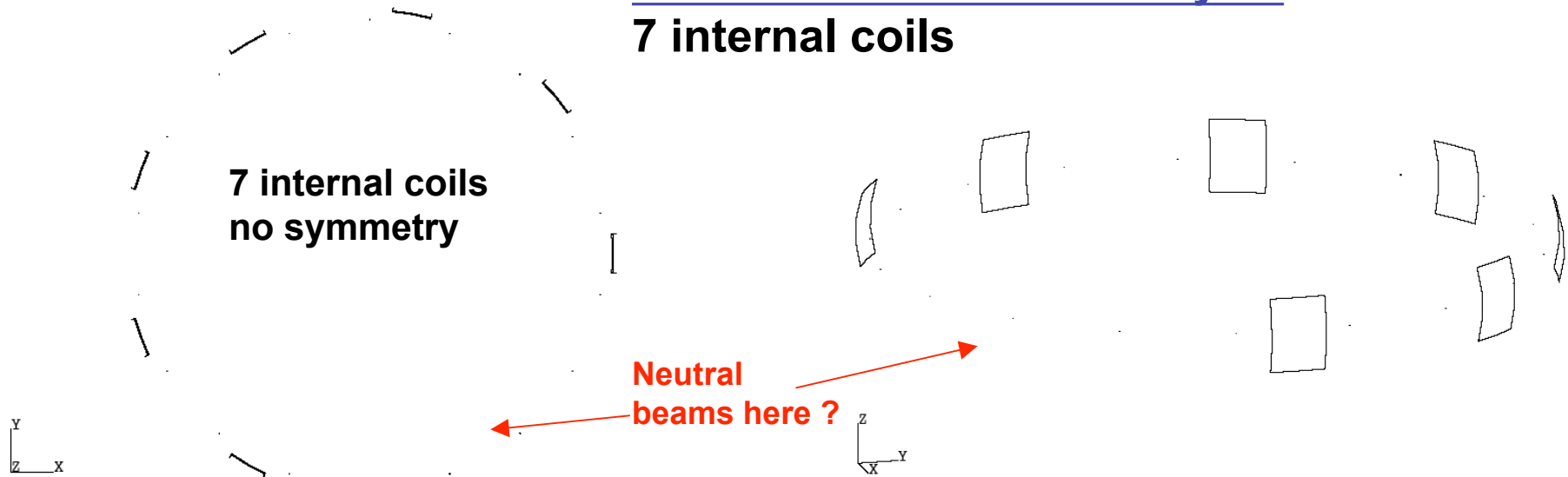
### 6 interior coils



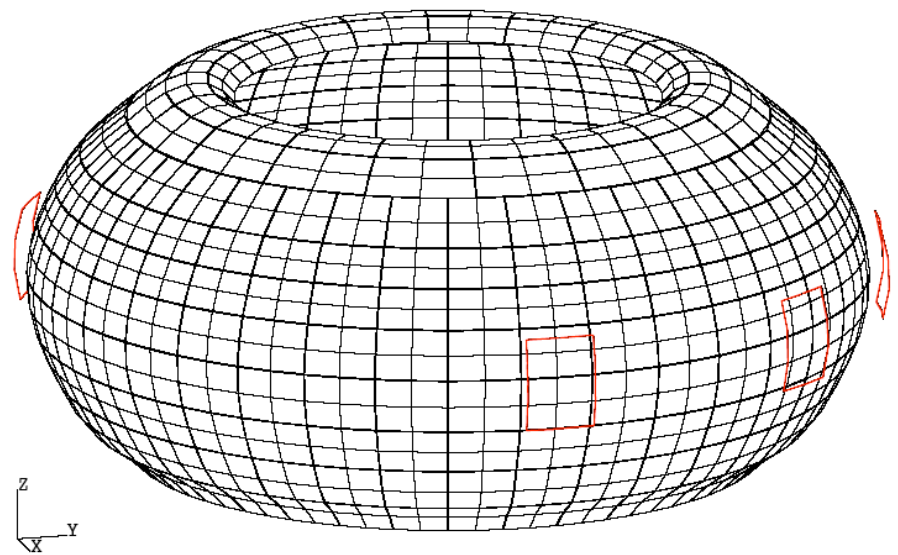
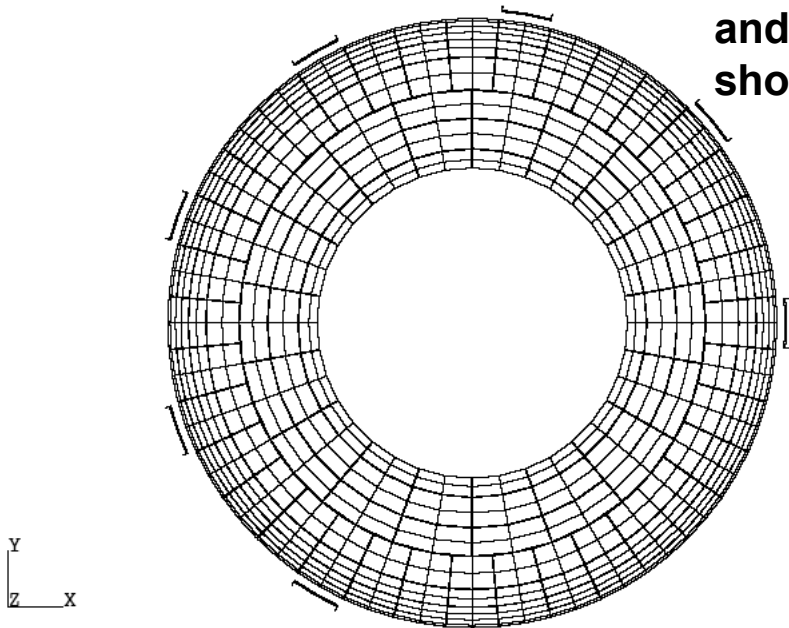
**Blanket modules and  
Interior RWM coils shown above**

## Extended ITER RWM analysis

### 7 internal coils



### 7 internal coils and all blanket modules shown



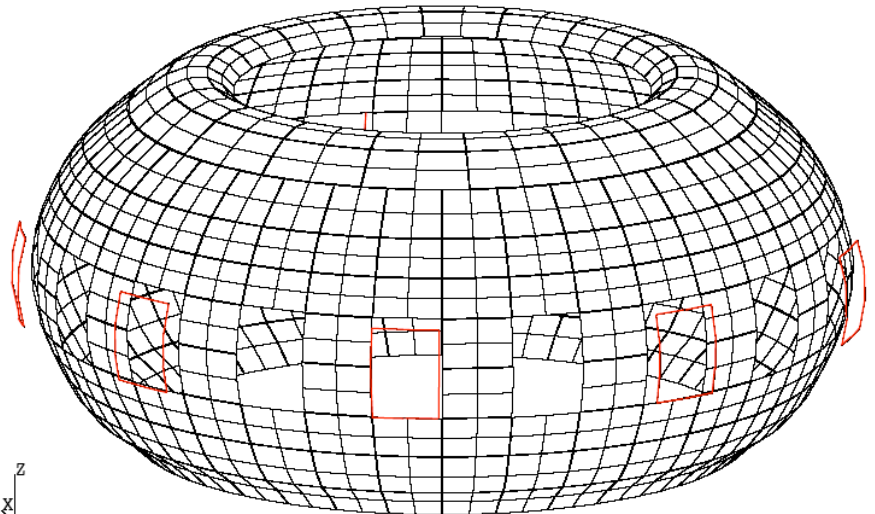
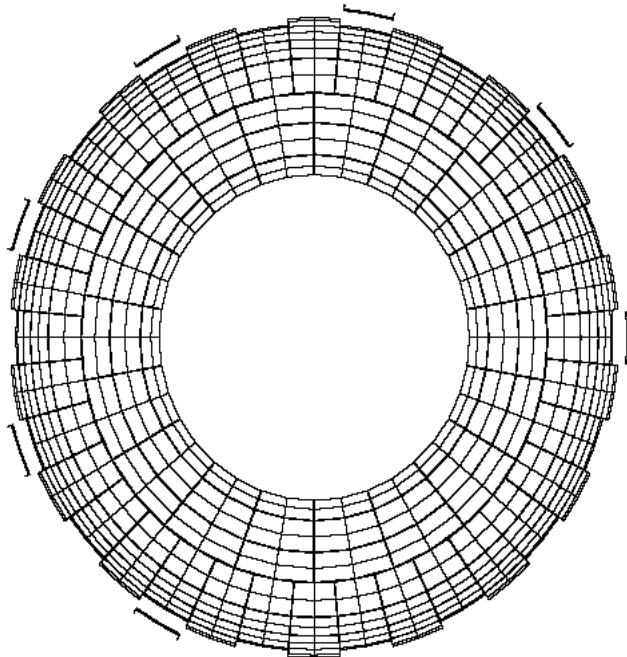
## Extended ITER RWM analysis

Remove blanket modules at mid plane ports

7 internal coils  
no symmetry

Neutral  
beams here ?

7 internal RWM coils  
and blanket modules  
shown, blanket modules removed  
at all radial ports



Performance with 6 internal coils, all blanket modules  
One coil in every third radial port (symmetrical)  
Exceeds best performance with exterior coils

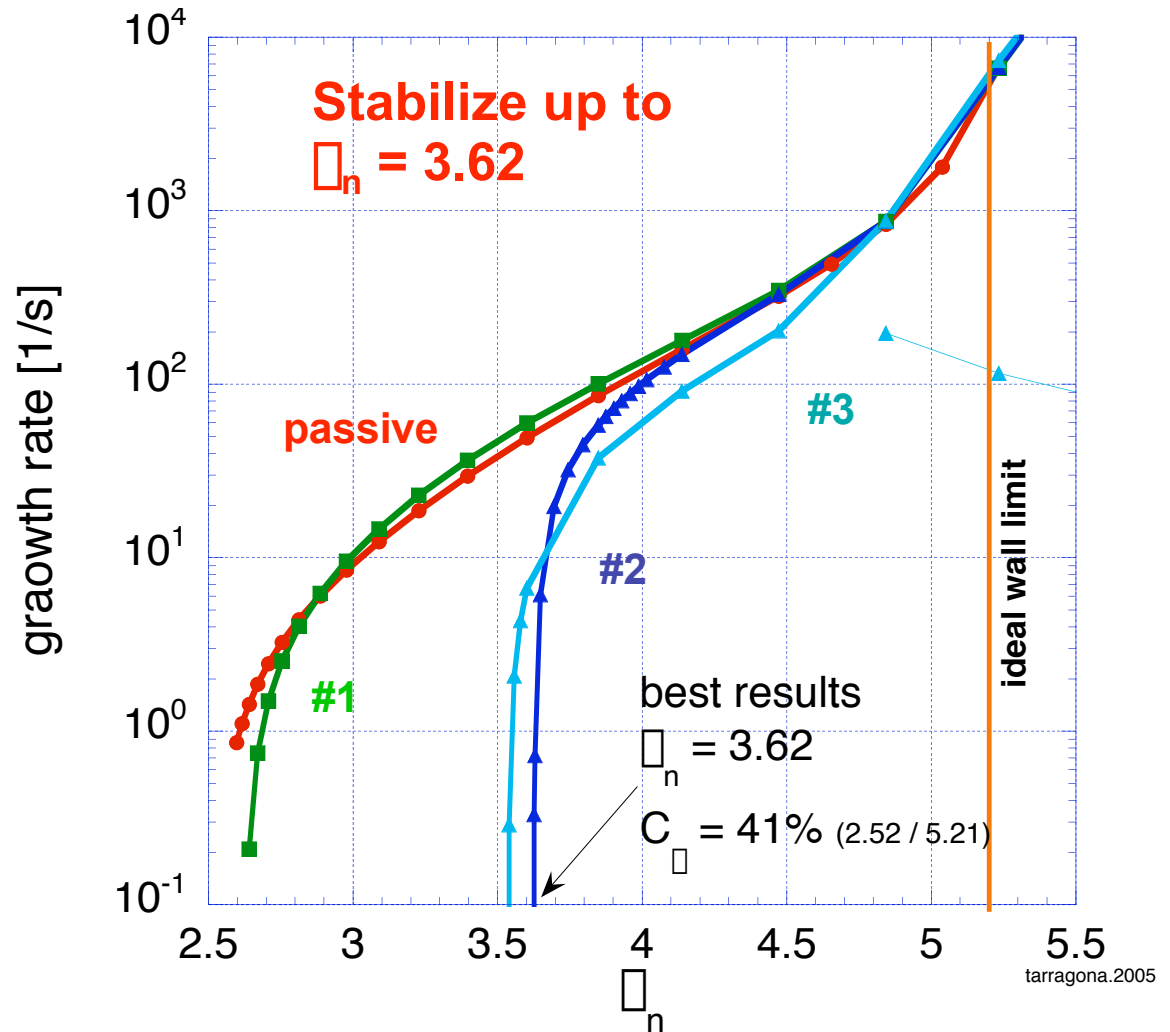
#1  $G_p = 10^7$  [v/w]

#2  $G_p = 10^8$

#3  $G_p = 10^9$

6 internal  
 coils connected  
 Into 3 pairs  
 Each pair has  
 $L/R = 7.2e-6 \text{ H} / 360.e-6 \Omega$   
 $= 20. \text{ ms}$

No optimization  
 was done.  
 Only  $G_p$  used !



Performance with 7 internal coils, again better than external coils, one coil every other radial port  
Has best performance with **all blanket modules**

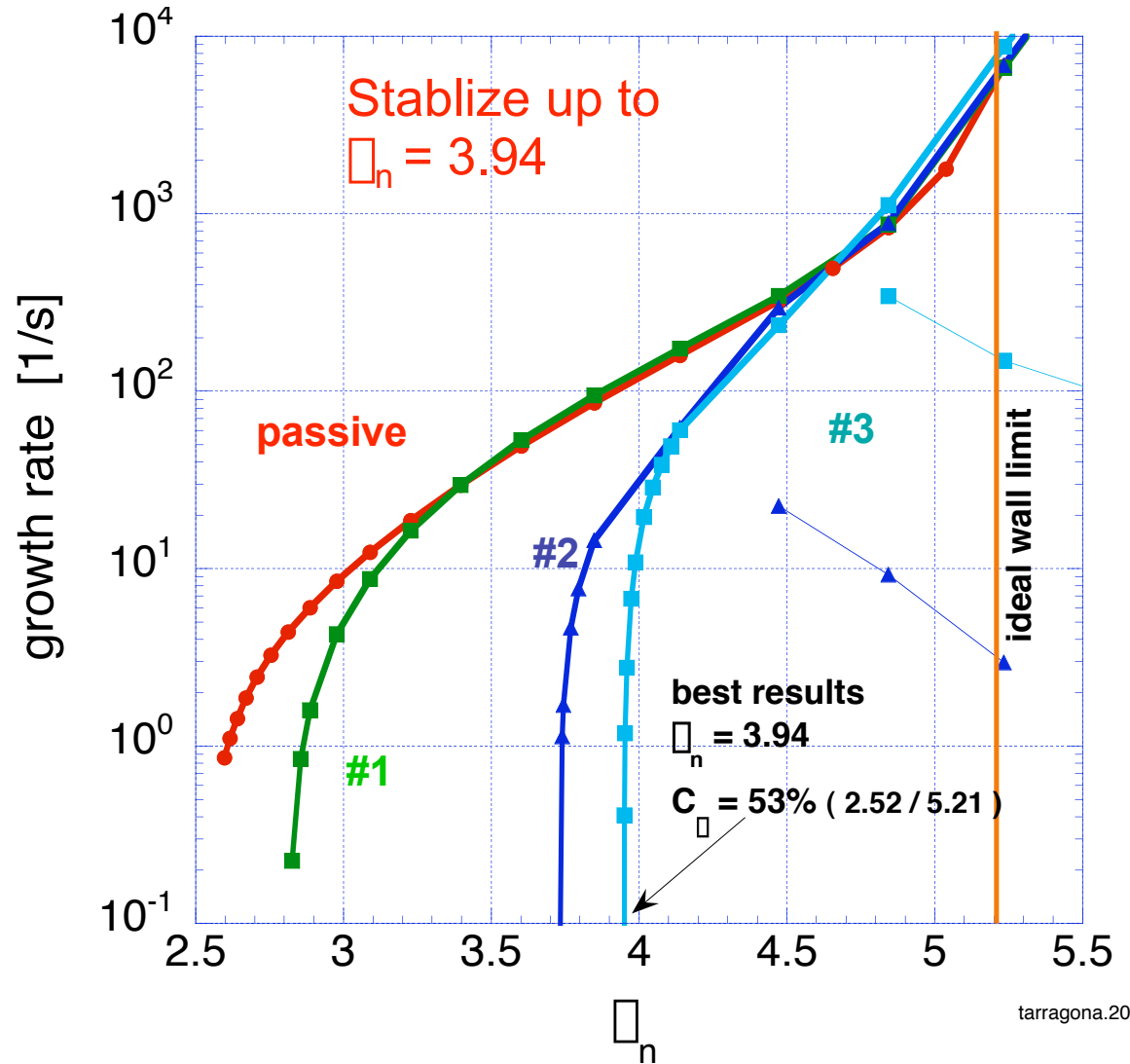
#1  $G_p = 10^7$  [v/w]

#2  $G_p = 10^8$

#3  $G_p = 10^9$

7 single coils  
 Each coil has  
 $L/R = 3.6e-6 \text{ H} / 180.e-6 \text{ } \square$   
 $= 20. \text{ ms}$

No optimization  
 was done.  
 Only  $G_p$  used !



# Removing blanket modules in front of internal coils

Gives best of all cases  $C_{\square} = 98.7\%$  ( 2.52 / 4.86),

7 interior coils with one coil every other radial port

#1  $G_p = 10^7$  [v/w]

#2  $G_p = 10^8$

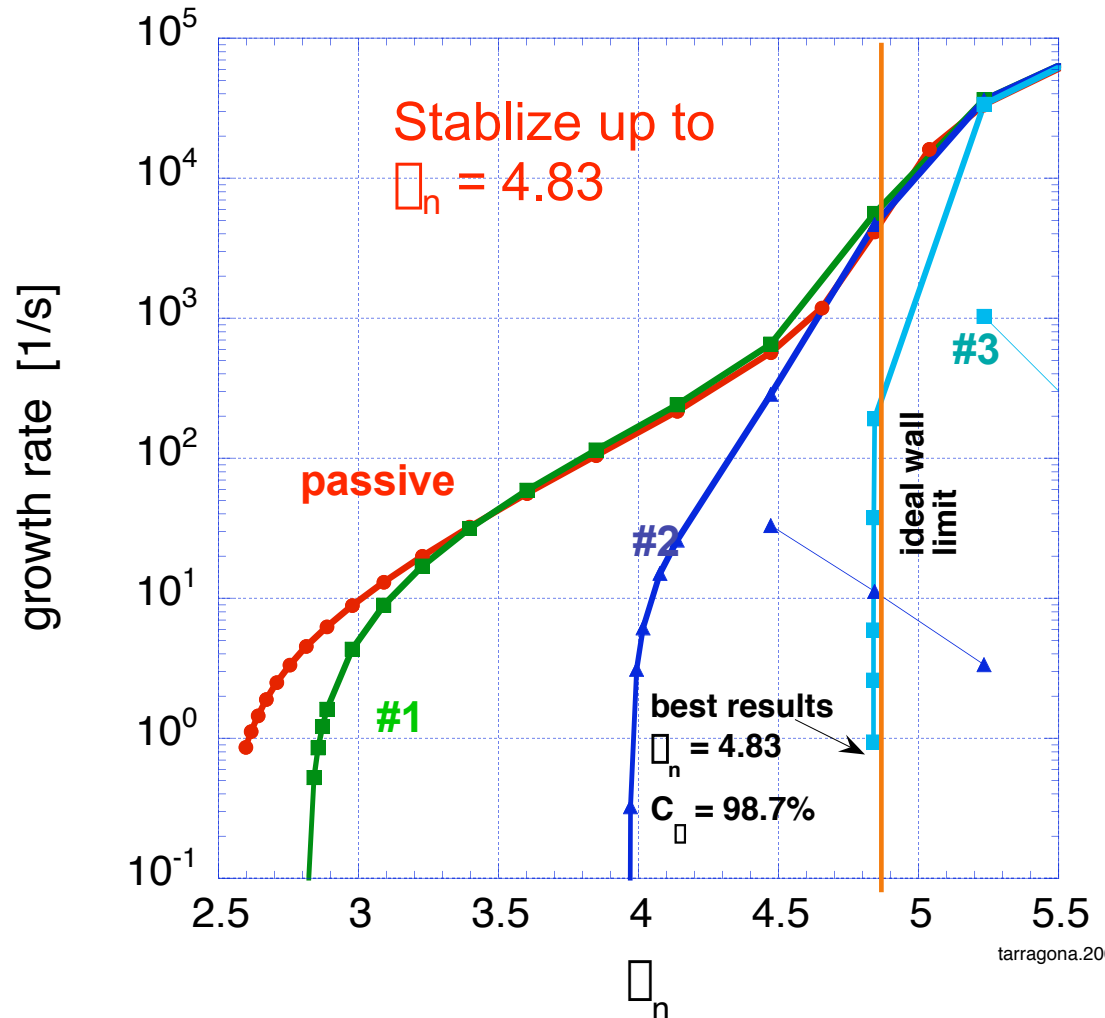
#3  $G_p = 10^9$

7 single coils each coil has  
 $L/R = 3.6e-6$  H /  $180.e-6$   $\square$   
= 20. ms

All blanket modules  
In front of radial ports  
were removed, this  
lowers passive performance

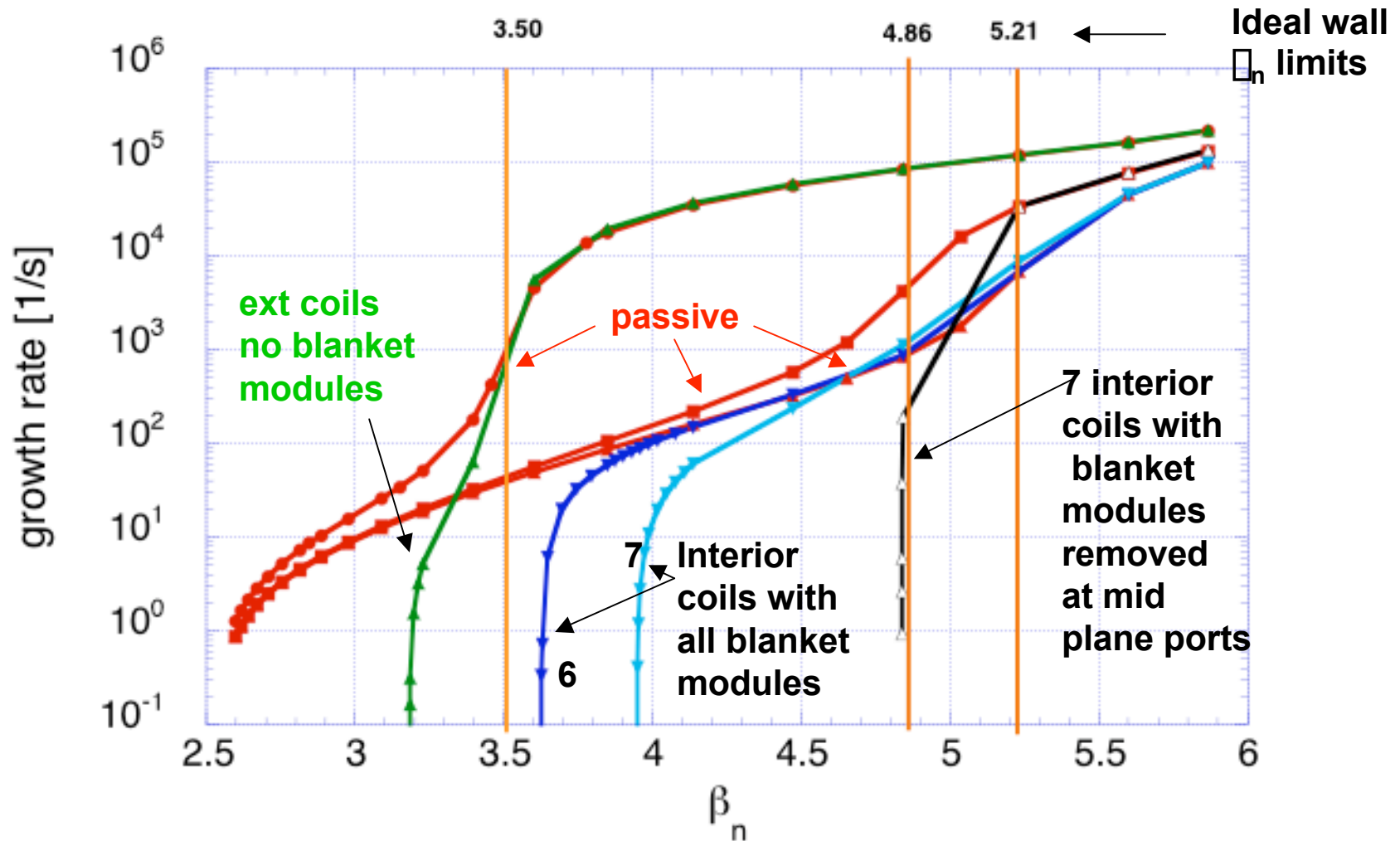
No optimization  
was done.

Only  $G_p$  used !



## Graphical summary VALEN RWM best results

Internal RWM coils perform significantly better than external RWM coils



## VALEN RWM active control performance limits in ITER

ports	blankets	RWM coils	$\beta_n$	$C_\beta$	$\beta[1/s]$ (passive)
no	no	continuous (benchmark)	3.196	69% ( 2.52 / 3.50)	43.9
no	no	6 ext. coils	3.18	67.6% ( 2.52 / 3.50)	40.9
no	9.ms	6 ext coils	3.177	24.4 % ( 2.52 / 5.21)	16.38
yes	9.ms	6 int. coils	3.62	41% ( 2.52 / 5.21)	52.5
yes	9.ms	7 int. coils	3.94	53% ( 2.52 / 5.21)	110.8
yes	9.ms*	7 int. coils	4.83	98.7% ( 2.52 / 4.86 )	4061.

\* (except at ports )



## Conclusions VALEN benchmarking

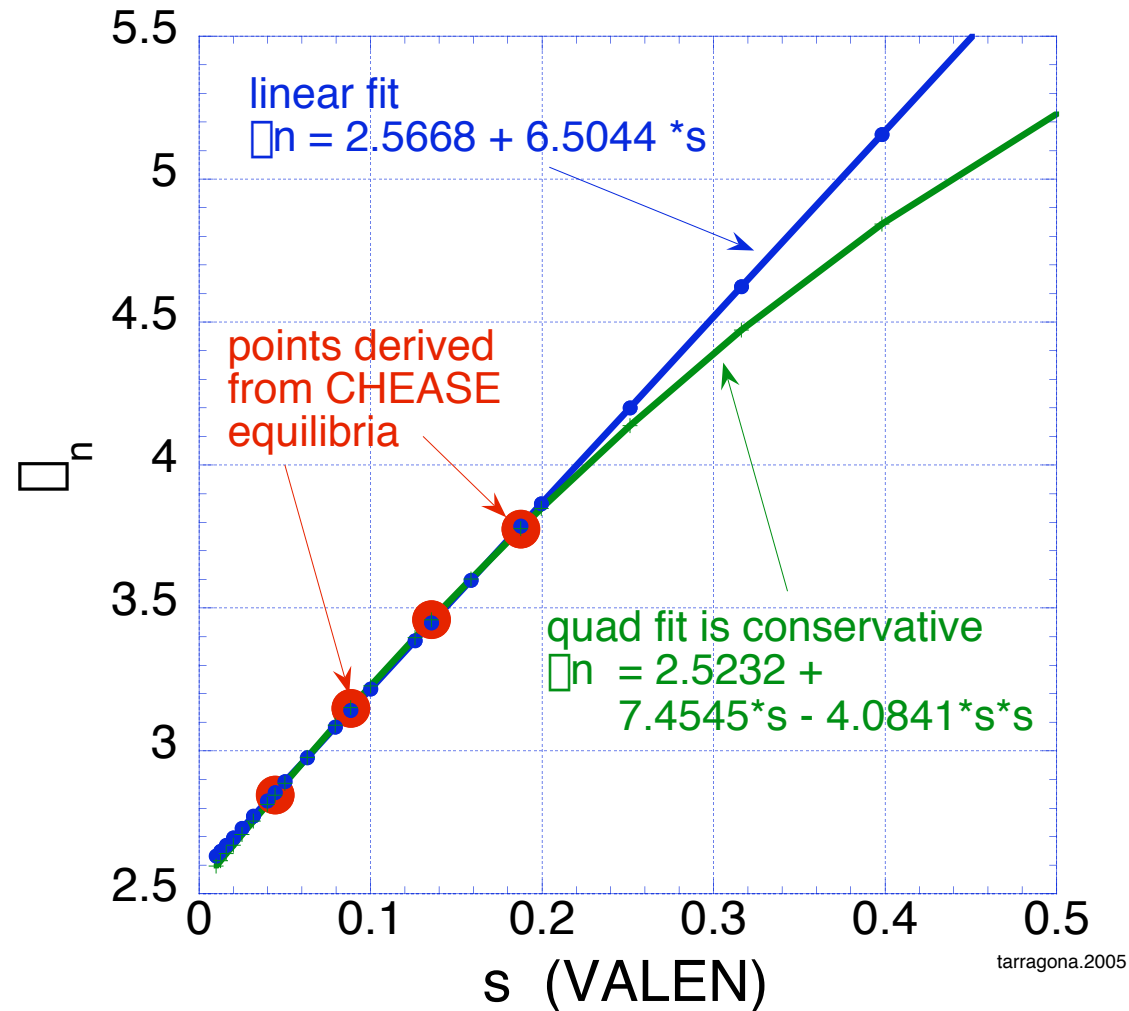
- VALEN RWM continuous coil benchmark model reaches  $\beta_n = 3.196$  or  $C_\beta = 69\%$  (2.52 / 3.50) [only the double wall vacuum vessel in this model].
- Presence of all blanket modules ( 9 ms each) extend the ideal  $\beta_n$  limit from 3.50 to 5.21
- ITER baseline design (no blankets, 6 ext coils with L/R =10. s & voltage control) requires both  $G_p$  &  $G_d$  (sensor flux and sensor voltage) gain, this model has about same performance as continuous coil benchmark model
- Extended ITER models with internal RWM coils performs significantly better than baseline ITER design:  $\beta_n = 3.94$  with all blanket modules and  $\beta_n = 4.83$  with blanket modules removed on mid plane radial ports

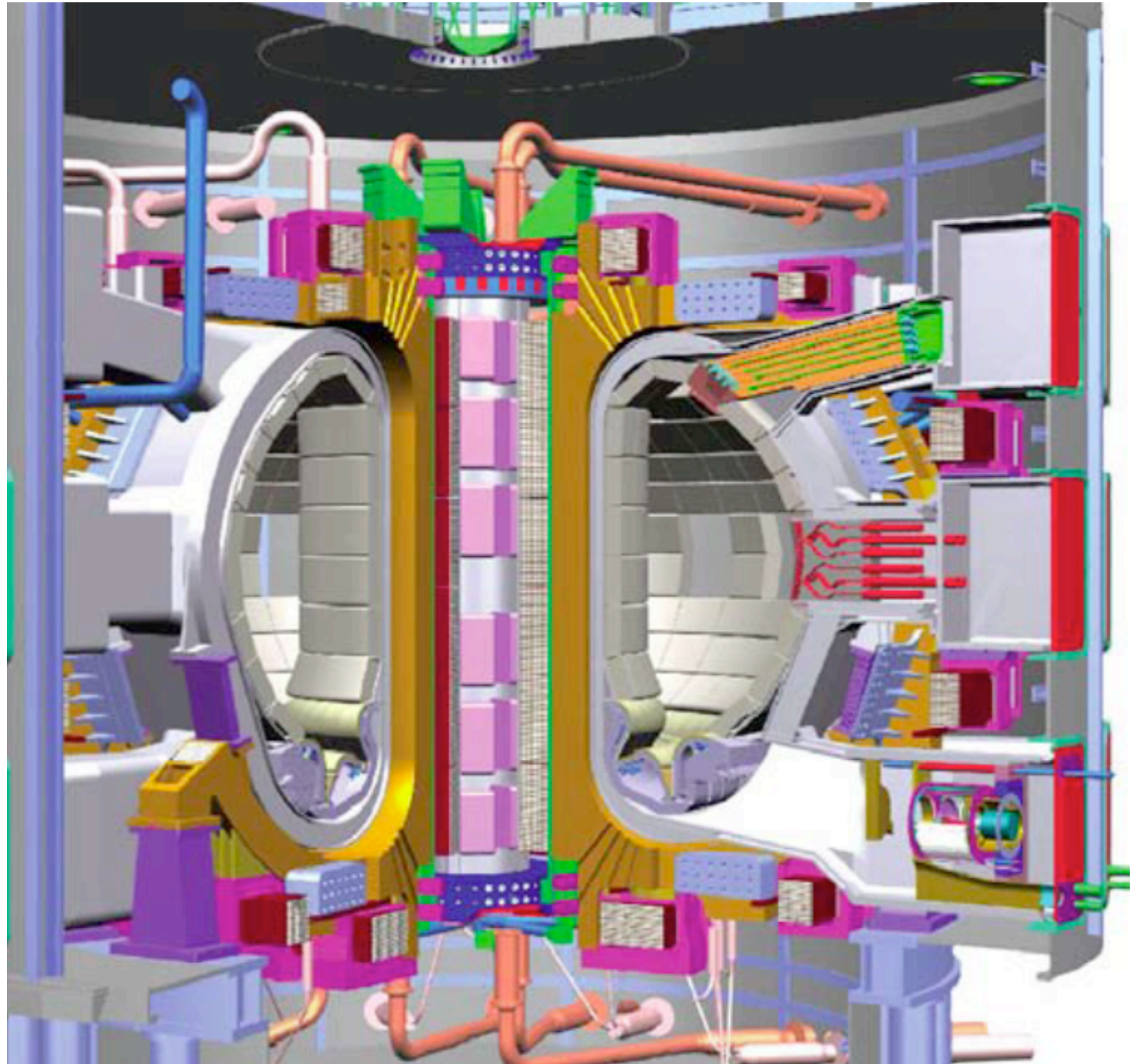
## Mapping from s to $\beta_n$

VALEN parameter  $s = -\beta W / (LI^2/2)$

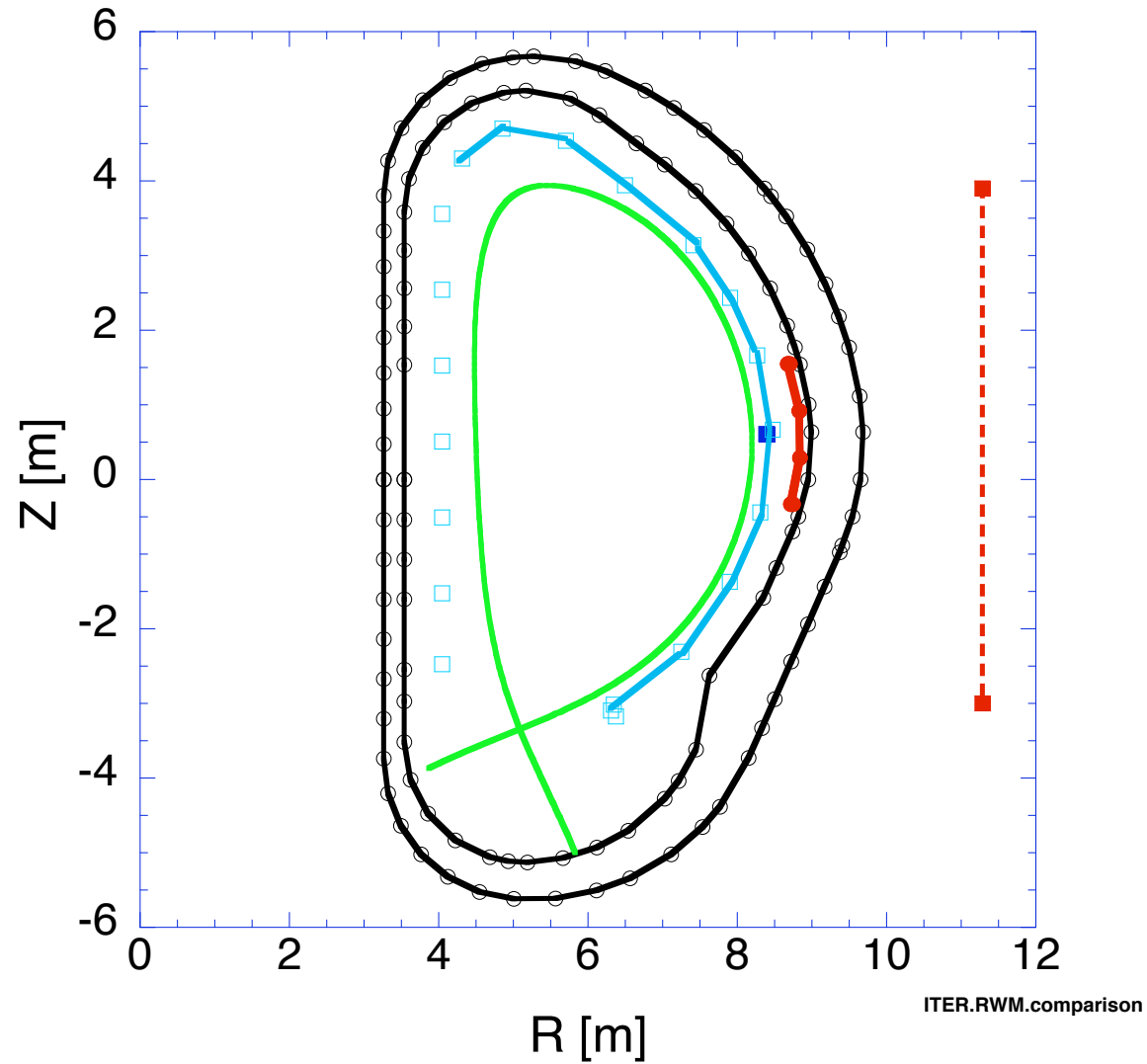
no wall  $\beta_n$  limit = 2.52 from conservative fit

Here  $LI^2/2$  is the energy of the current distribution that produces  $B_n$



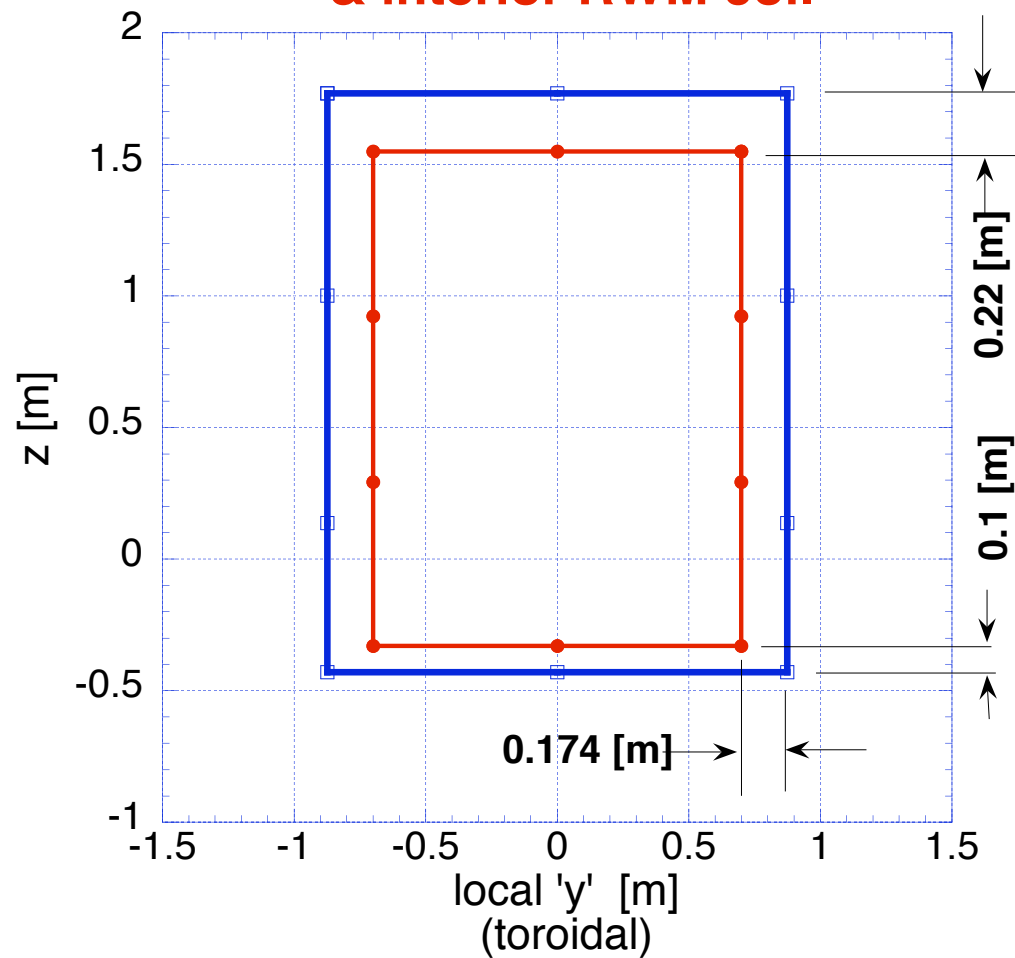


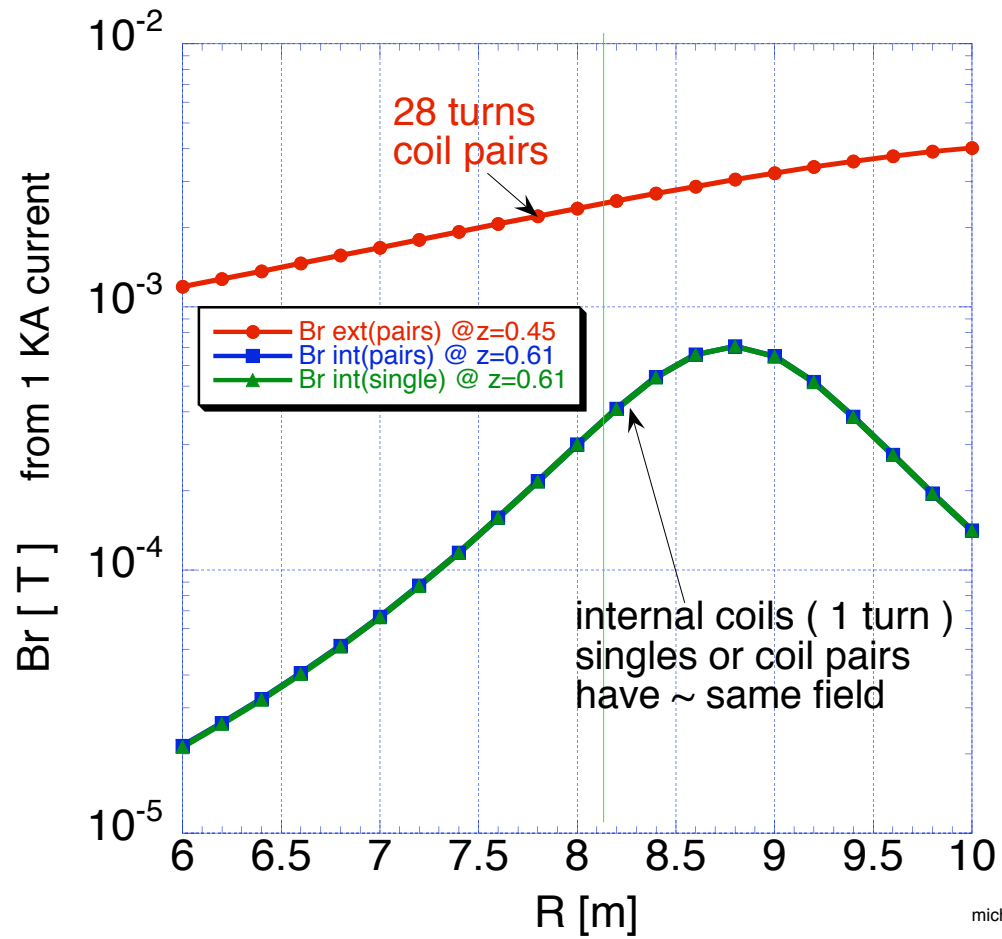
**ITER RWM benchmarking**  
**plasma, walls, control coils,**  
**blanket modules, & Bp sensors**



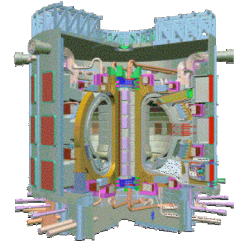
each internal RWM  
coil covers **9.05 degrees**  
(in toroidal direction)

**radial view of  
mid plane port  
& interior RWM coil**



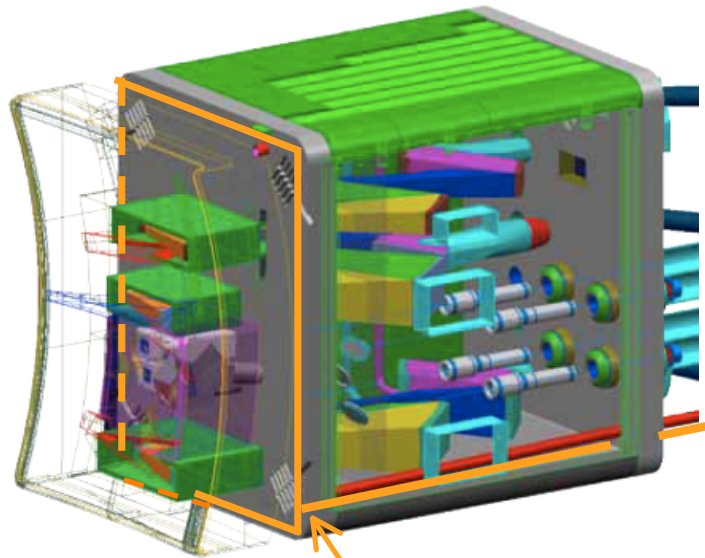


# Applying FIRE-Like RWM Feedback Coils to ITER Increases $\beta_N$ limit for $n = 1$ from $\beta_N = 2.5$ to $\sim 4$



G. Navratil, J. Bialek Columbia University

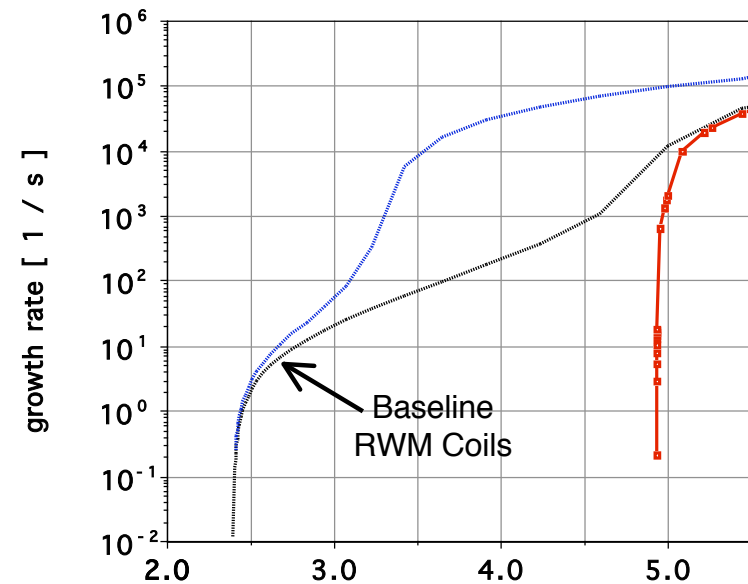
## RWM Coil Concept for ITER



- Baseline RWM coils located outside TF coils
- **FIRE-like RWM coils would be located inside the vacuum vessel behind shield module but inside the vacuum vessel on the removable port plugs.**
- Integration and Engineering feasibility of internal RWM coils is under study.

VALEN Analysis Columbia University

Data from "ITER.09.2003"



No-wall limit

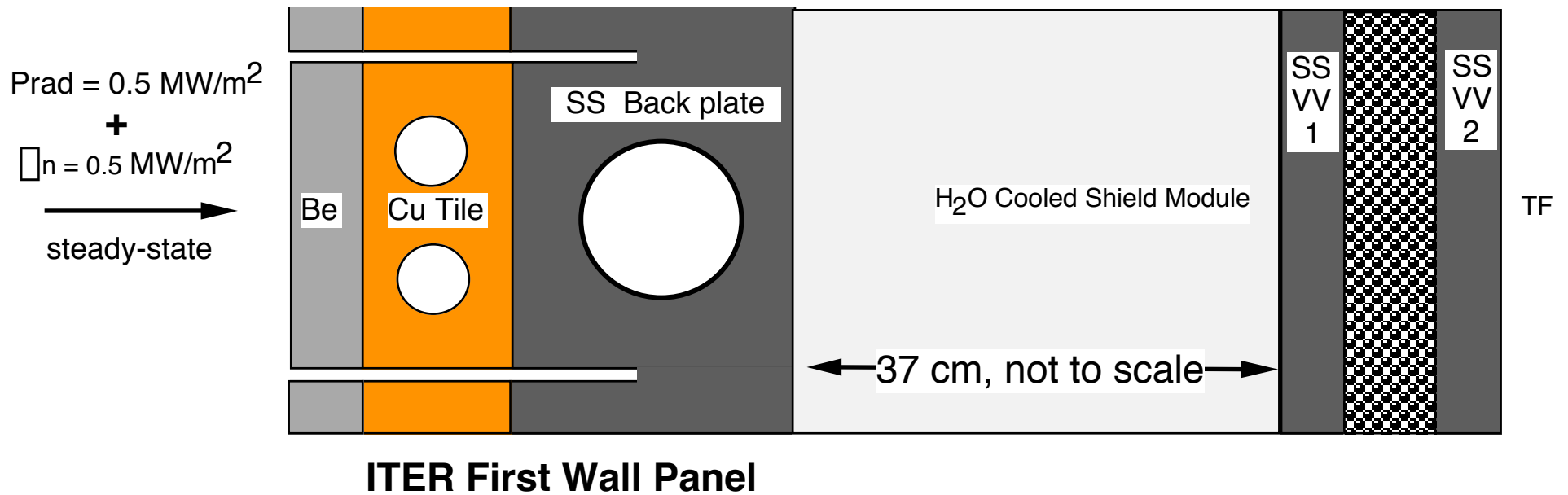
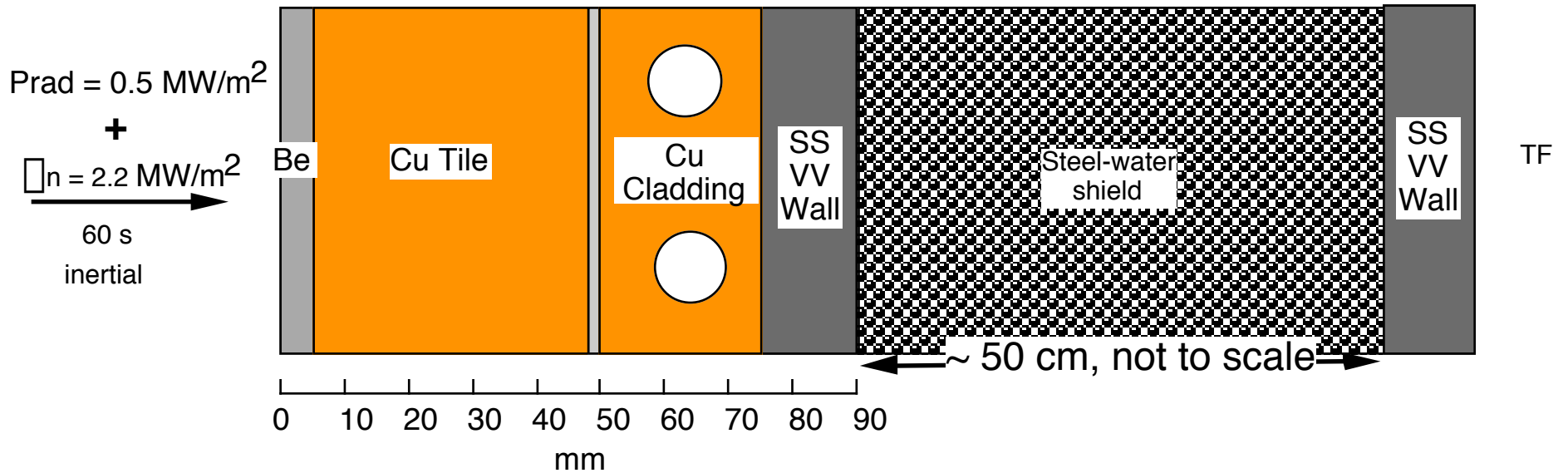
beta-n (new)

RWM Coils in every third port, no shield module

**FIRE-like RWM coils would have large stabilizing effect on  $n=1$**

# FIRE and ITER First Wall Design Concepts are Similar

**Outboard First Wall for FIRE**



**ITER First Wall Panel**