

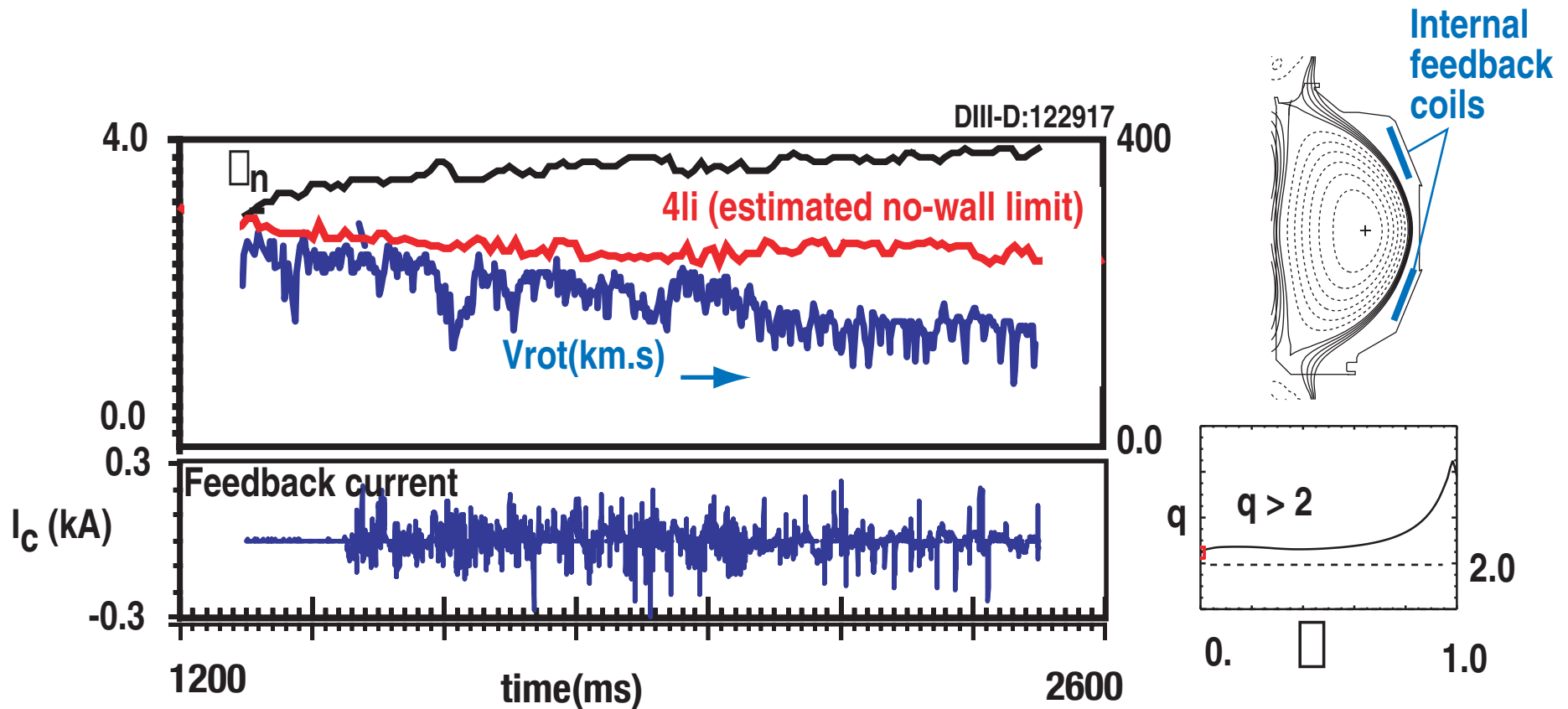
**Present understanding of RWM physics
and
possible approaches for RWM control in burning plasmas**

**Workshop (W60) on “Burning Plasma Physics and Simulation”
4-5 July 2005, University Campus, Tarragona, Spain
Under the Auspices of the IEA Large Tokamak Implementing Agreement**

Goal of RWM Control in Burning Plasmas

- Sustainment of AT plasmas well above no-wall limit -

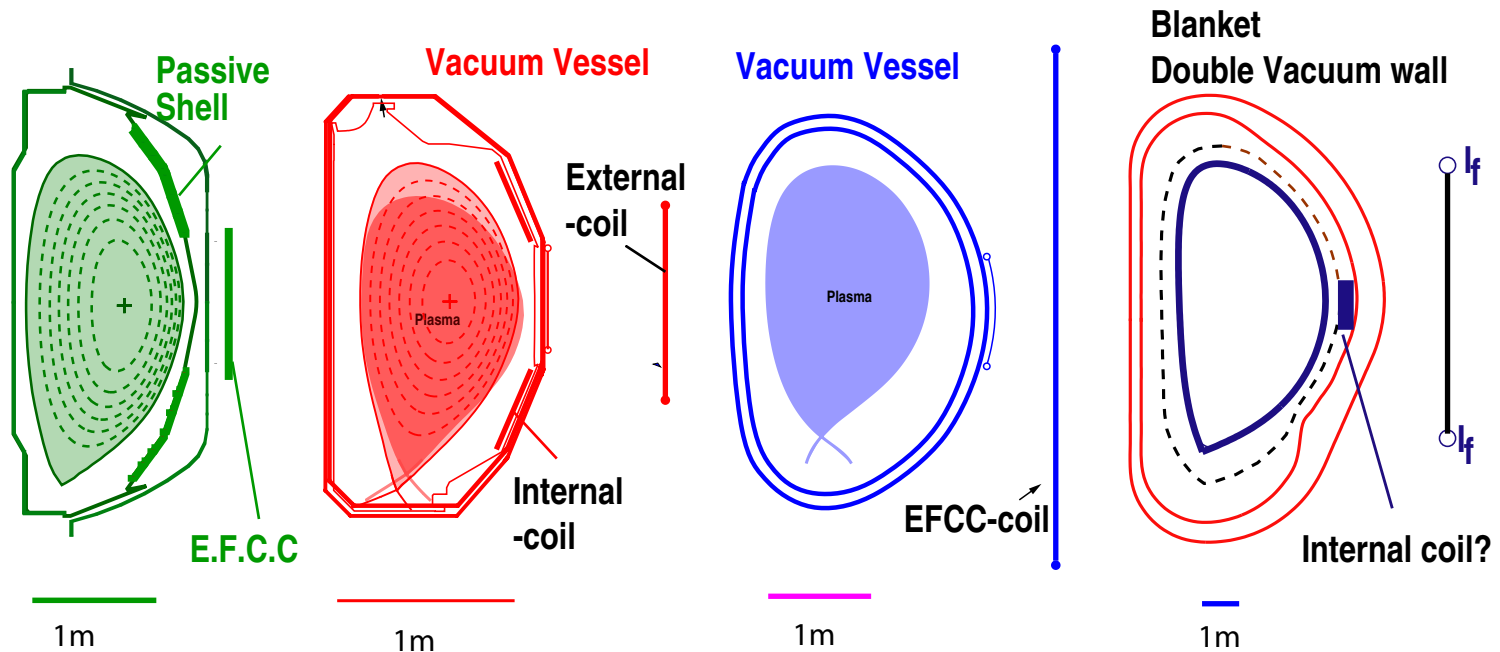
- Achievement of high β_n AT plasmas was assisted by combined stabilization of plasma rotation and magnetic feedback



OUTLINE

- **RWM physics understanding has been significantly advanced by collaborative efforts (DIII-D, JET, NSTX,.....)**
 - High betan AT plasma has been achieved
 - Experimental results and theoretical predictions are in qualitative agreement
 - Analysis using numerical codes (e.g., MARS, VALEN,) has advanced the understanding of RWM physics
 - Plasma rotation is marginal for RWM stabilization in ITER: present prediction
- **Advantages of Internal coils (DIII-D experiments)**
 - Low current required for dynamic error field correction
 - Fast time-response compared with external coils
 - Achievement of high betan
- **ITER**
 - Internal control coils are attractive
- **Open issues**

Non-axisymmetric Coils on Various Devices



NSTX

DIII-D

JET

ITER

non-axisymmetric coils

External(6)

External (6)
internal (6x2)

External (4)

External (9)
Internal coil (7)?

R/a

1.27

3.1

3.0

3.4

R(m)

1.10

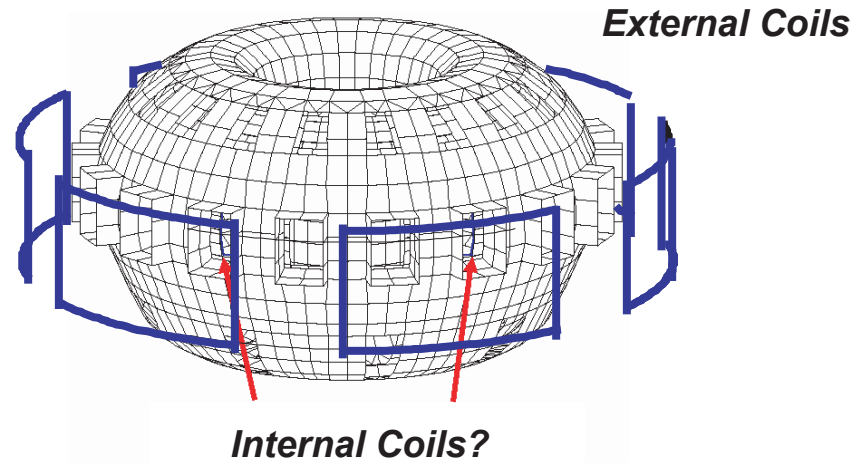
1.69

2.85

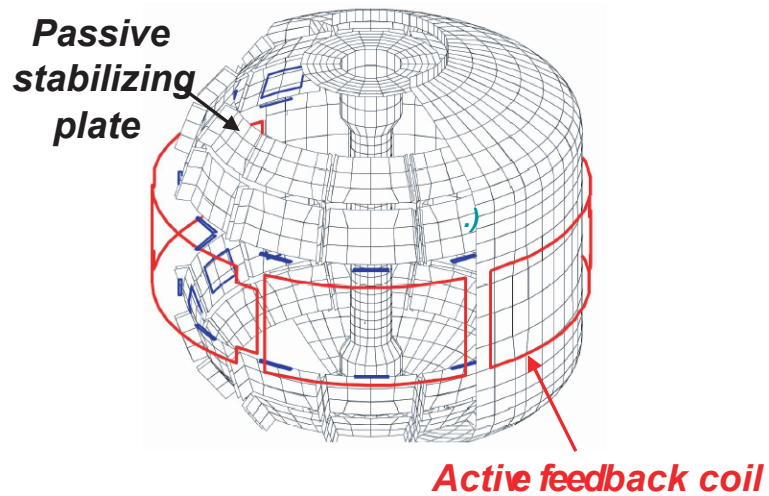
6.35

Non-axisymmetric Coils on Various Devices

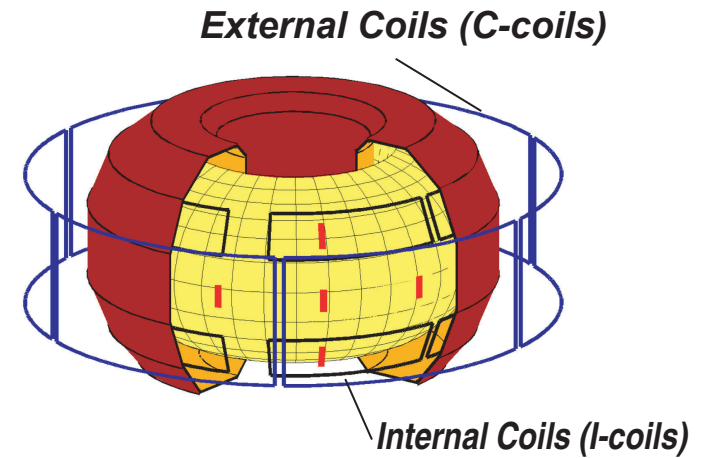
ITER



NSTX



DIII-D



Excellent Progress of Experiments and RWM Theory Has Led to Quantitative Understanding of RWM Physics

- 1996 - concept of rotational stabilization and feedback

$$\underbrace{(\gamma + in\Omega)^2 - \delta W_p}_{\text{Ideal Stability}} + \underbrace{\frac{\delta W_{pw} \gamma \tau_w}{\gamma \tau_w + 1}}_{\text{Resistive Wall}} + \underbrace{(\gamma + in\Omega) D}_{\text{Plasma Dissipation}} = 0$$

- 1998 Use of non-axisymmetric coils

- 2001 Discovery of Dynamic Error Field Correction (DEFC)

- 2002 Confirming Resonant error Field Amplification (RFA)

- 2003 - Joint Experiments with DIII-D, JET, NSTX

- MARS
- VALEN
- Analytical models
-

Dissipation
stabilizing force

$$j\text{Im}(\Delta W_C + \Delta W_T) = -\frac{1}{2} \int \vec{F}_{\text{diss}} \cdot \vec{\xi}_{\perp}^* d^3x$$

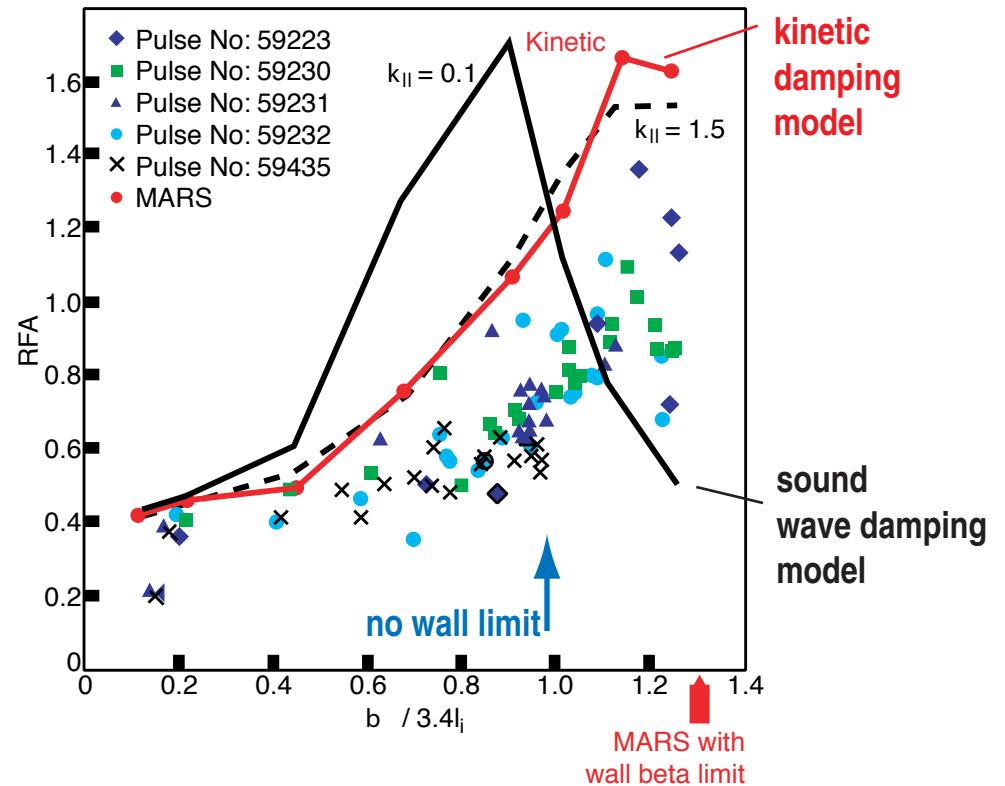
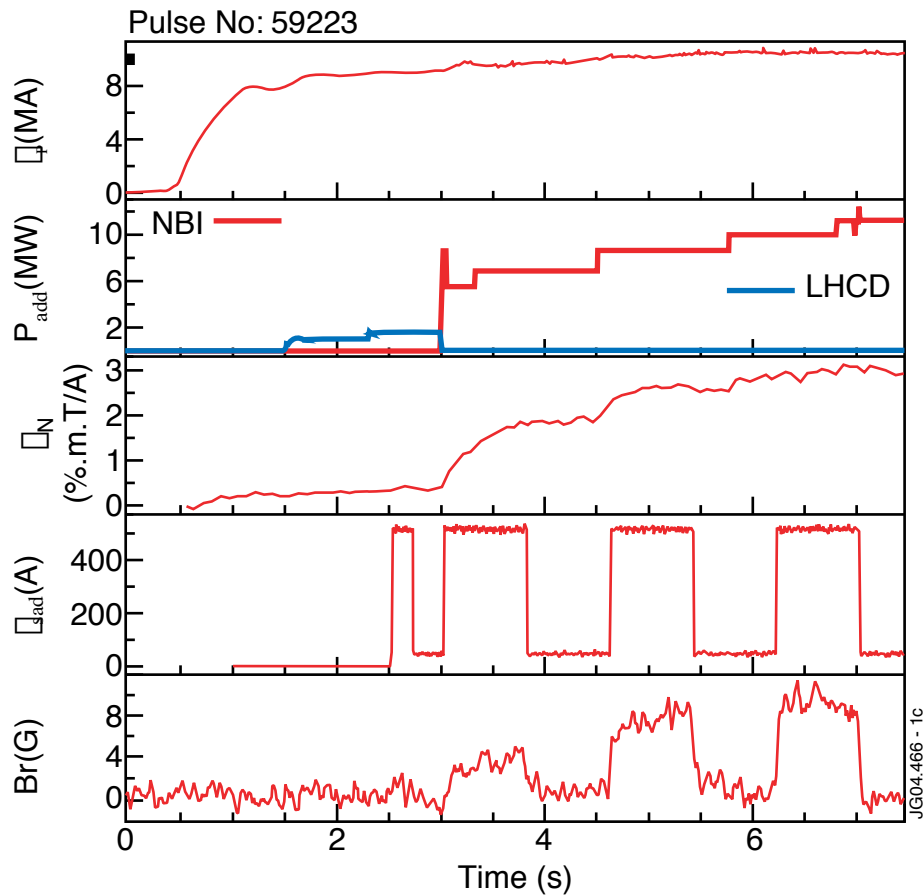
$$\Delta W_T = \frac{1}{2} \sum_{m'} \int d^3x \int_{\text{trapped}} d\Gamma \left(-\frac{\partial f}{\partial E} \right) \frac{\omega}{\omega + m' \omega_b} | \langle \exp(j\chi_{m'}) H \rangle |^2$$

$$\Delta W_C = \frac{1}{2} \sum_{m'} \int d^3x \int_{\text{circ}} d\Gamma \left(-\frac{\partial f}{\partial E} \right) \frac{\omega}{\omega - (nq - m') \omega_t} | \langle \exp(j\chi_{m'}) H \rangle |^2$$

Kinetic damping model

RFA Has Been Observed at $\beta_N \geq \beta_{N, \text{no-wall}}$ in JET

- RFA is common feature in the toroidal device
- MARS code provides qualitative agreement



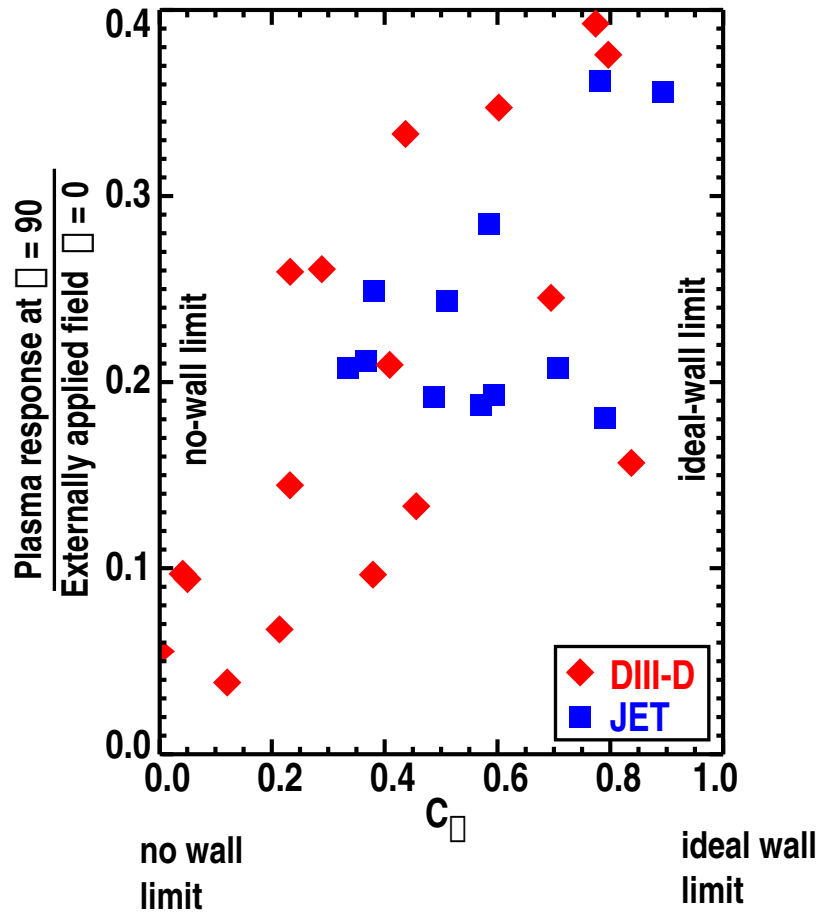
JET RFA with internal coils

ref: T. Hender et al., [IAEA 2004]

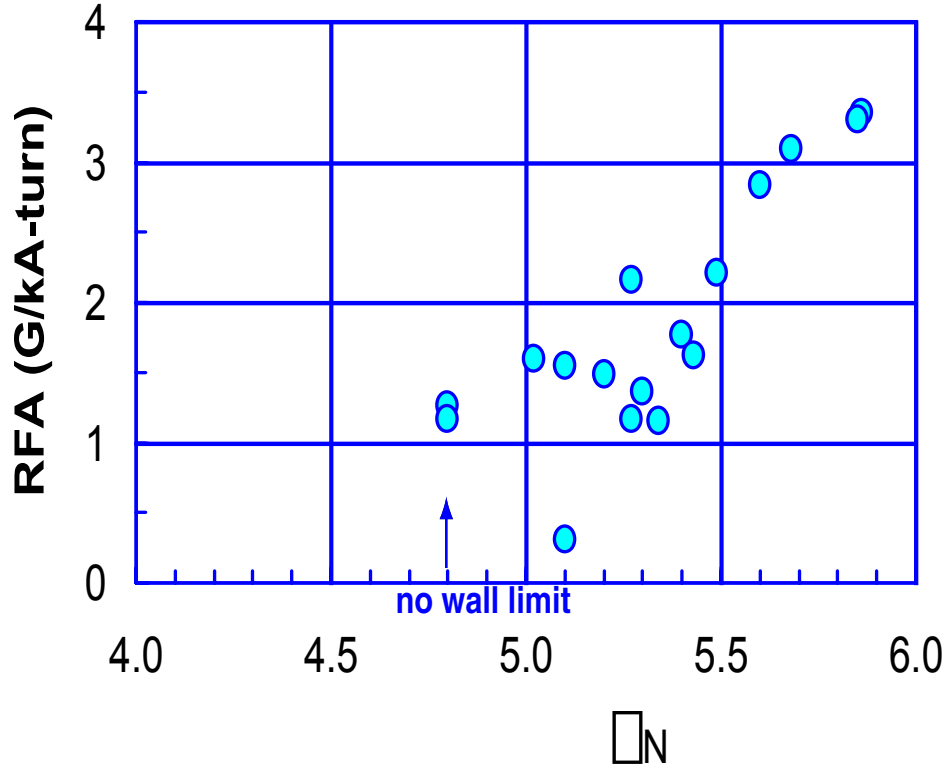
- Mode rigidity is the fundamental assumption of understanding in the rotational stabilization.
 - > Internal mode structure measurement should verify the hypothesis.
 - MSE technique is now available [R. Jayakumar RSI 75(2004)2995]

RFA Observations in JET, DIII-D and NSTX

Have Provided Consistent Dependence of RFA Magnitude on β_N

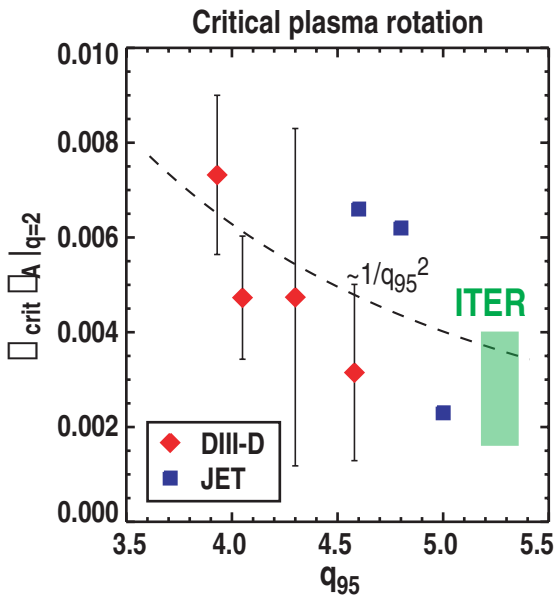
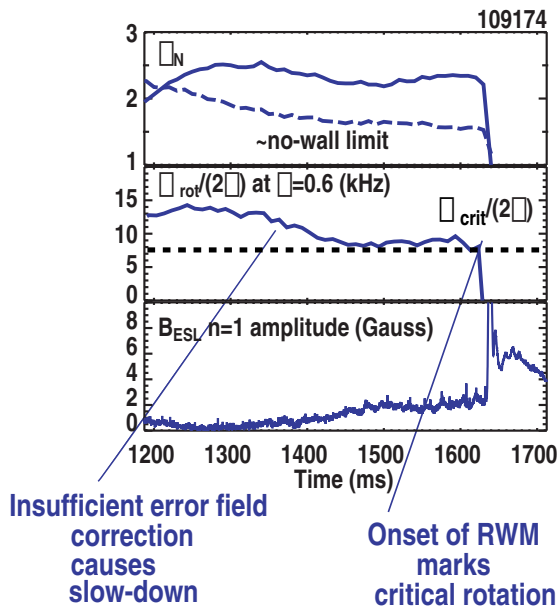


JET / DIII-D
with External coils
H. Reimerdes EPS[2005]

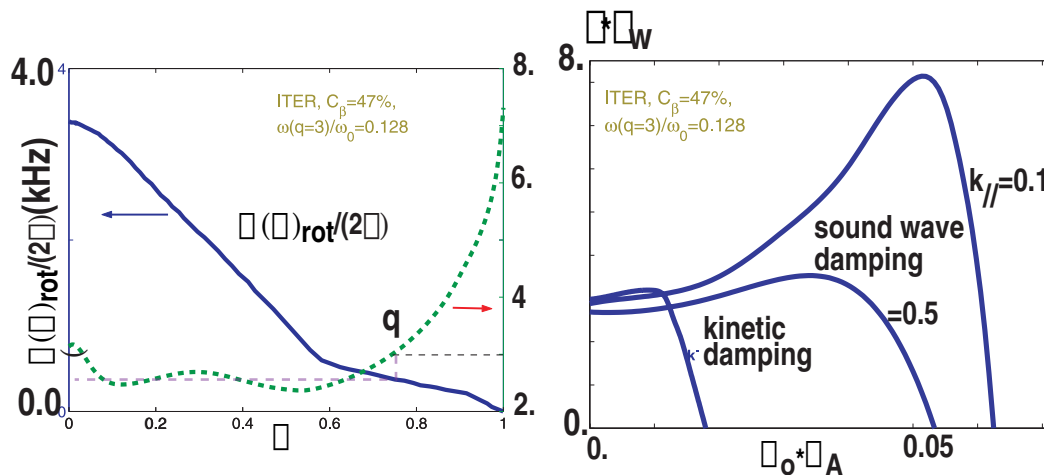


NSTX
S. Sabbagh IAEA(2004)

Results from DIII-D/JET Indicates that the Rotation in ITER will be Marginal for RWM Stability

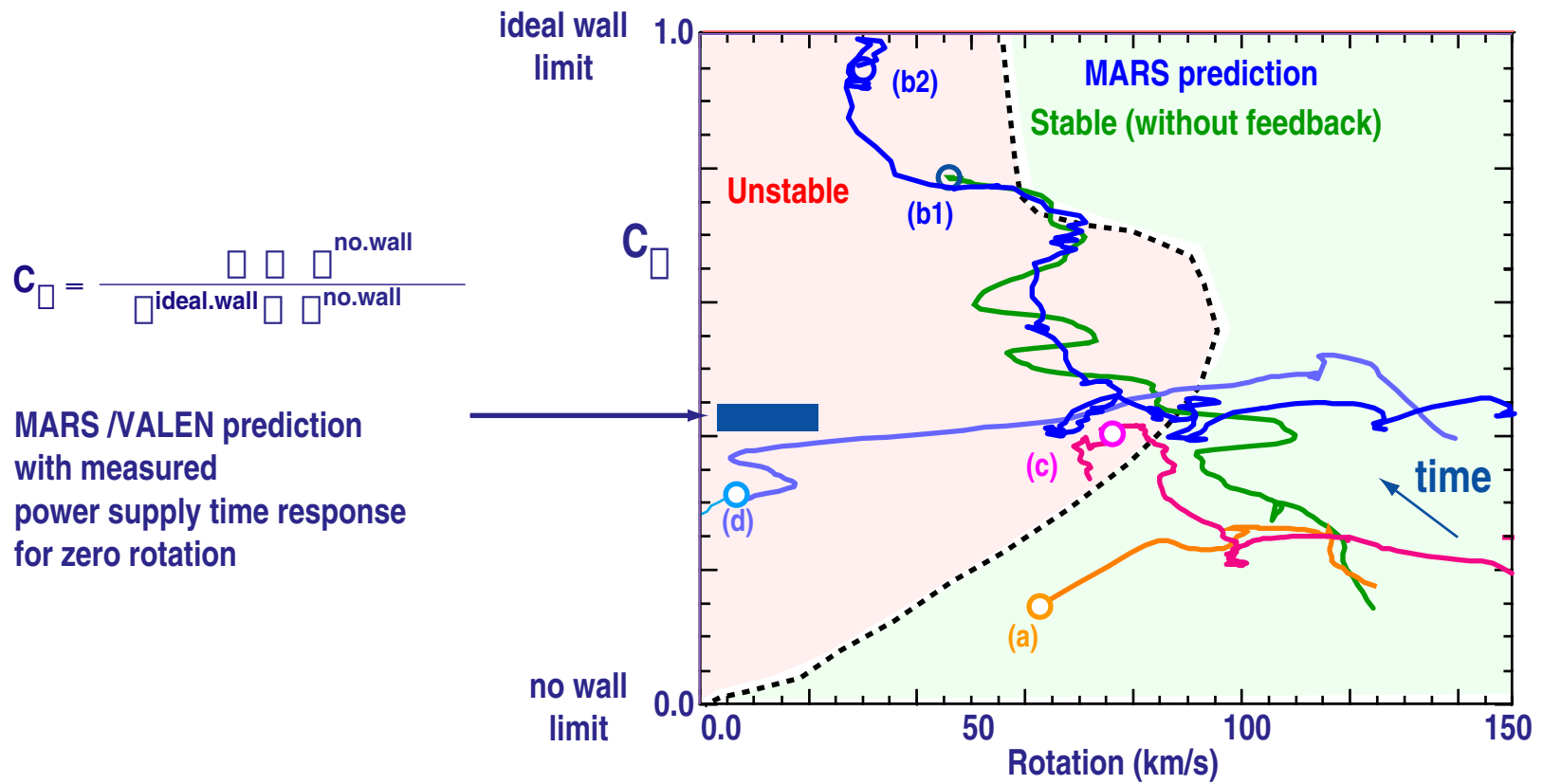


	DIII-D Exp.	ITER prediction	ITER predicted by MARS (kinetic)	ITER expected rotation
R(m)	1.69	6.35		
q_{min}	1.5	2.4		
ω_A (s)	0.40	0.75		
$\omega_{crit}^* \omega_A$	0.004 (q=2)	0.004	0.002 (q=3)	
$\omega_{crit}/(2\pi)$	1.6 (q=2)	1.0	0.45 kHz	
$\omega_{expected}/(2\pi)$				0.5 kHz



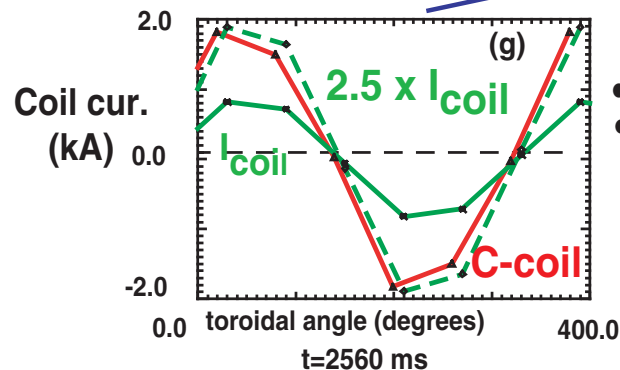
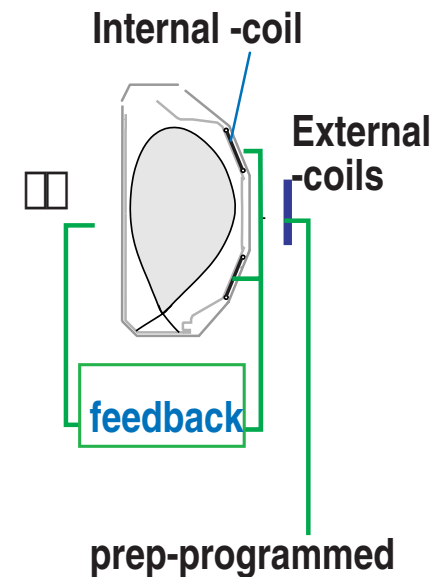
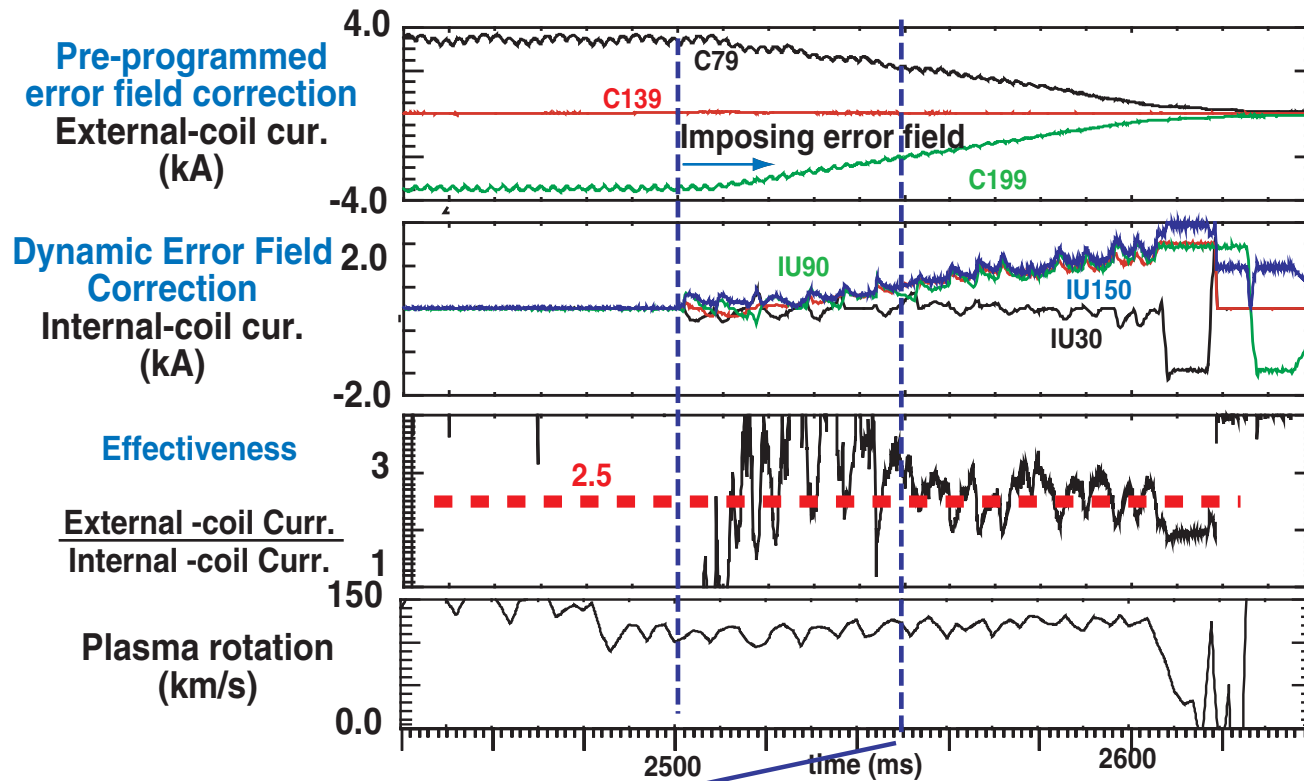
ITER prediction for scenario 4 [Y.Q.Liu IAEA 2004]

Combination of Rotational Stabilization and Feedback Has Increased Stable RWM Domain



Internal Coils Need only $\approx 1/3$ of External Coil Current for Dynamic Error Field Correction

- Error field imposed by External Coils was replaced by Internal Coils through feedback



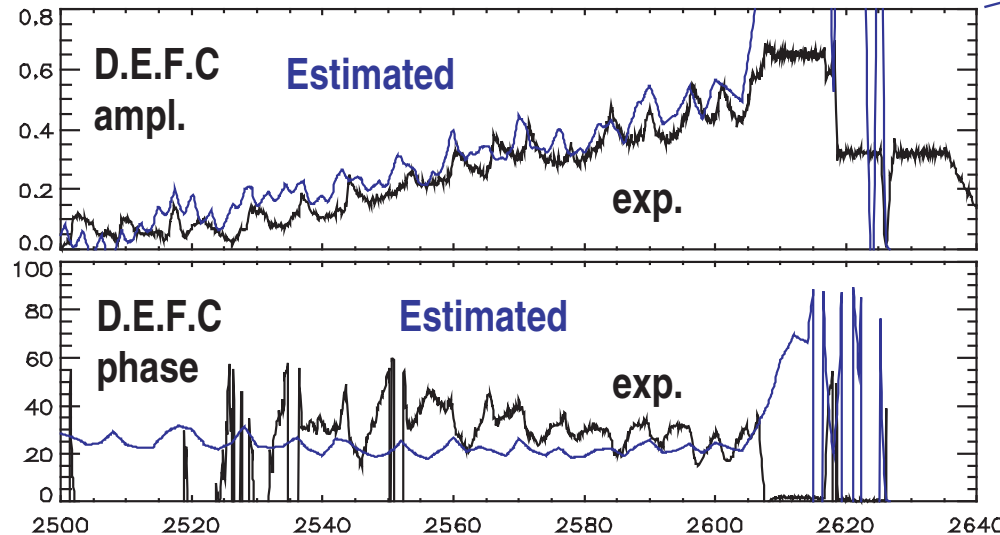
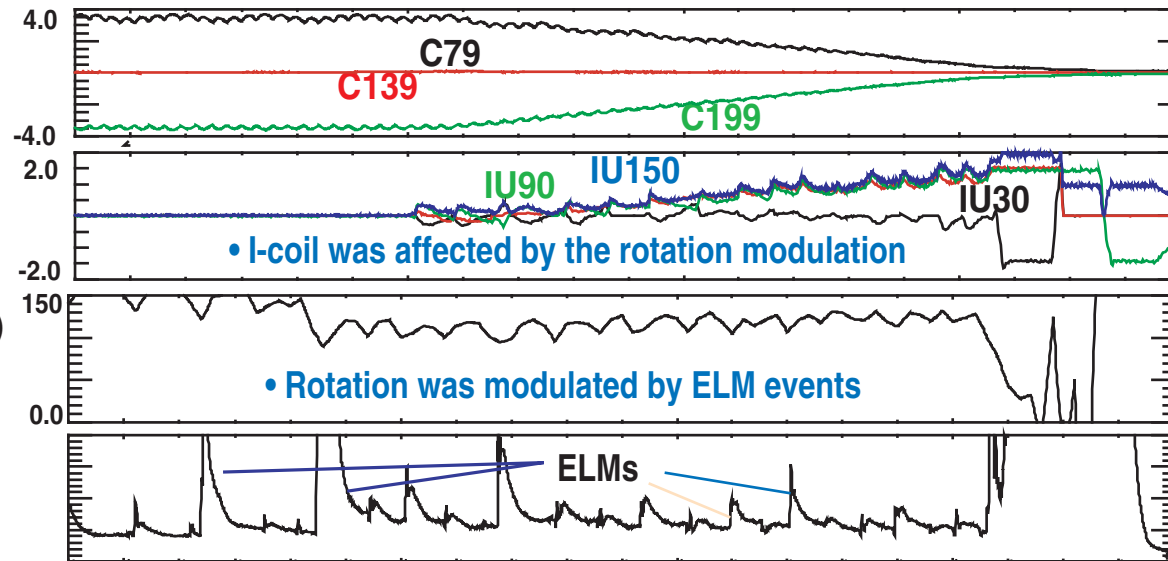
- Internal coils: $1/2 \cdot L \cdot I^2$
 - Internal coils: $L \cdot I$
- 1% of External -coil
□ 3% of External-coil

	L	R
Internal coils	10 □H	4 m□
External coils	170 □H	10 m□

ELM-Modulated rotation affects the coil current.

- ω_{rot} May be Needed as an input for Refining Dynamic Error Field Correction.

- Pre-programmed error field correction
External-coil cur. (kA)
- Dynamic error field correction
Internal -coil cur.(kA)
- Plasma rotation (km/s)



• Estimate by "Extended lumped parameter model" including ω_{rot} explains I-coil modulation

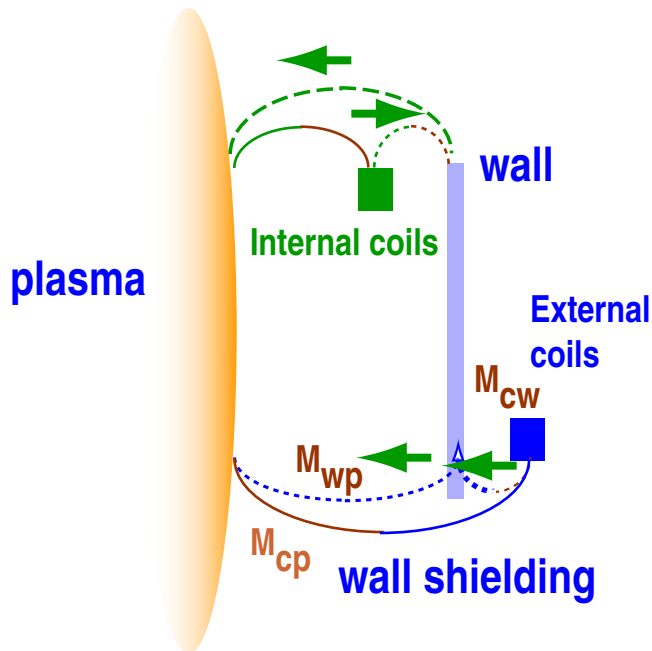
-> need of sensors of ω_{rot} for optimizing the process

Internal-coil is more effective in reducing ELM induced n=1 RWM

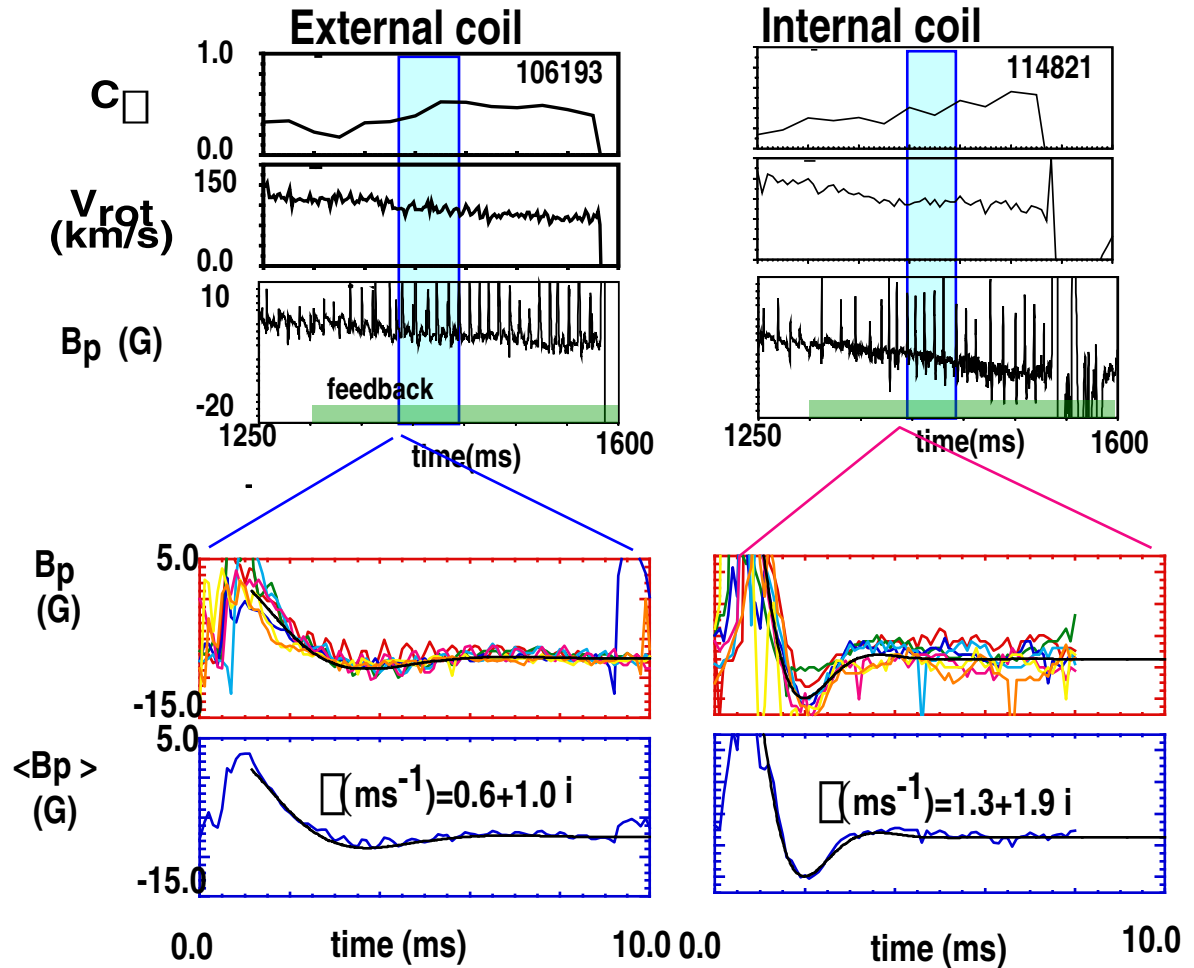
- n=1 component of ELM events excites n=1 RWM
- Internal-coil feedback reduces the n=1 RWM by a factor of 2 faster than with C-coil

Internal coil advantages

- Closer to Plasma
- Wall shielding can be compensated by higher feedback gain

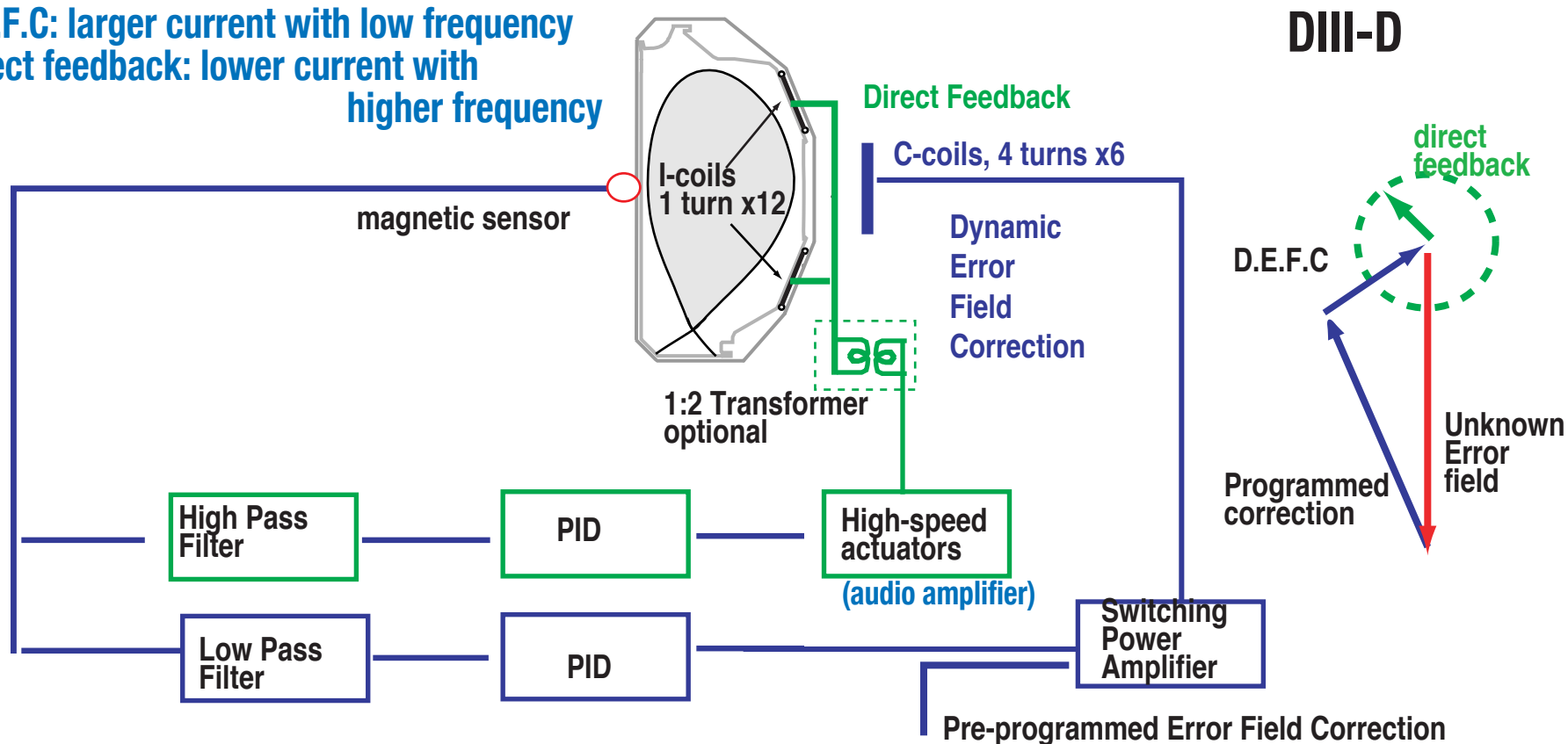


Feedback Performance



Independent Operation of Dynamic Error Field Correction and Direct Feedback is More Efficient and Effective

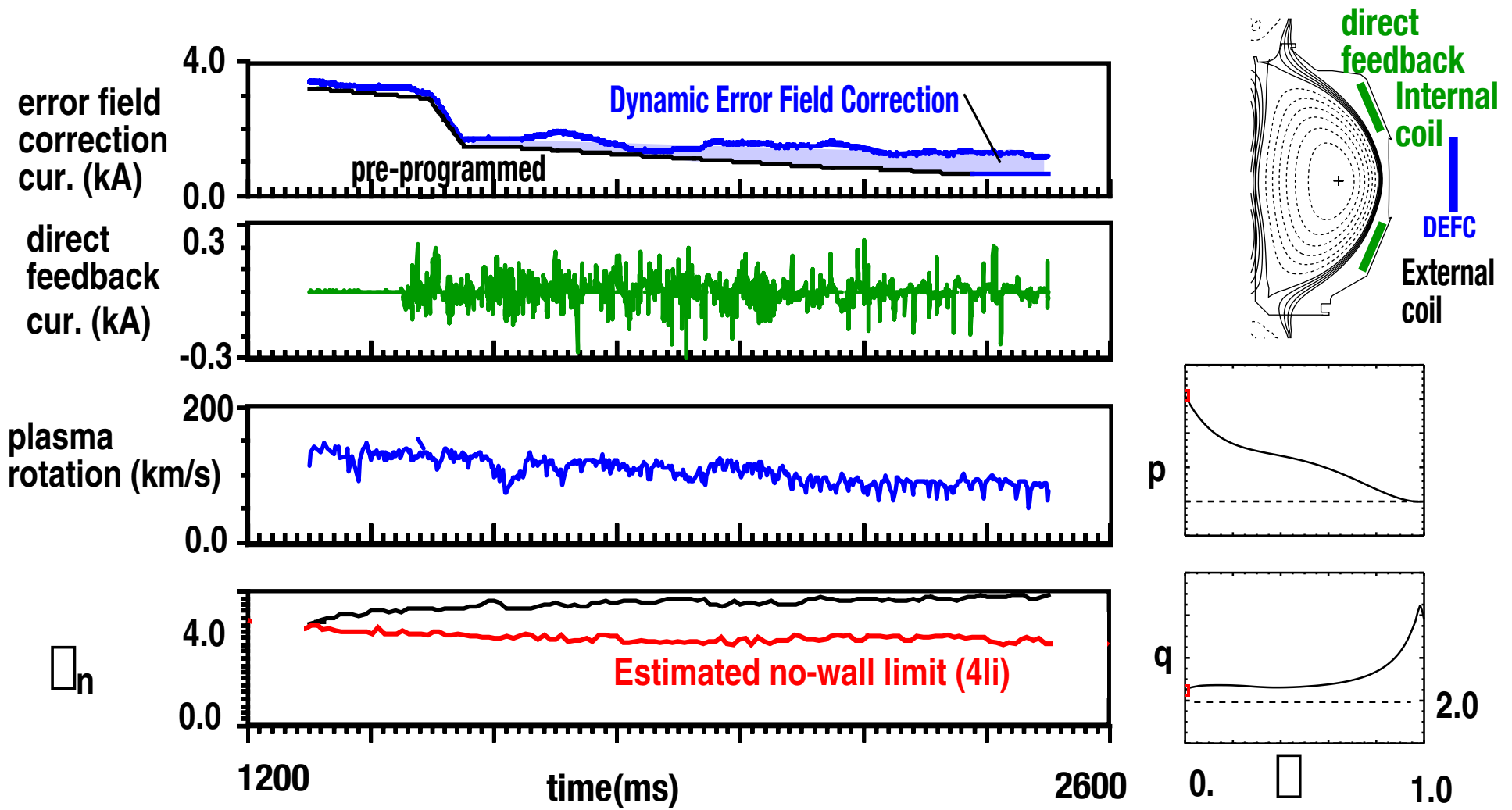
- D.E.F.C: larger current with low frequency
- Direct feedback: lower current with higher frequency



Coil	Inductance	Resistance incl. leads	Power Supply	volt and current	Freq. range
I-coil	10 μ H (quartet)*	4 m Ω	High-speed actuators	400 A x 140 V (quartet)	DC-50 kHz
C-coil	170 μ H (pair)*	10 m Ω	Switching Power Amplifier	3.5kA x 250 V (pair)	DC-1.5 kHz

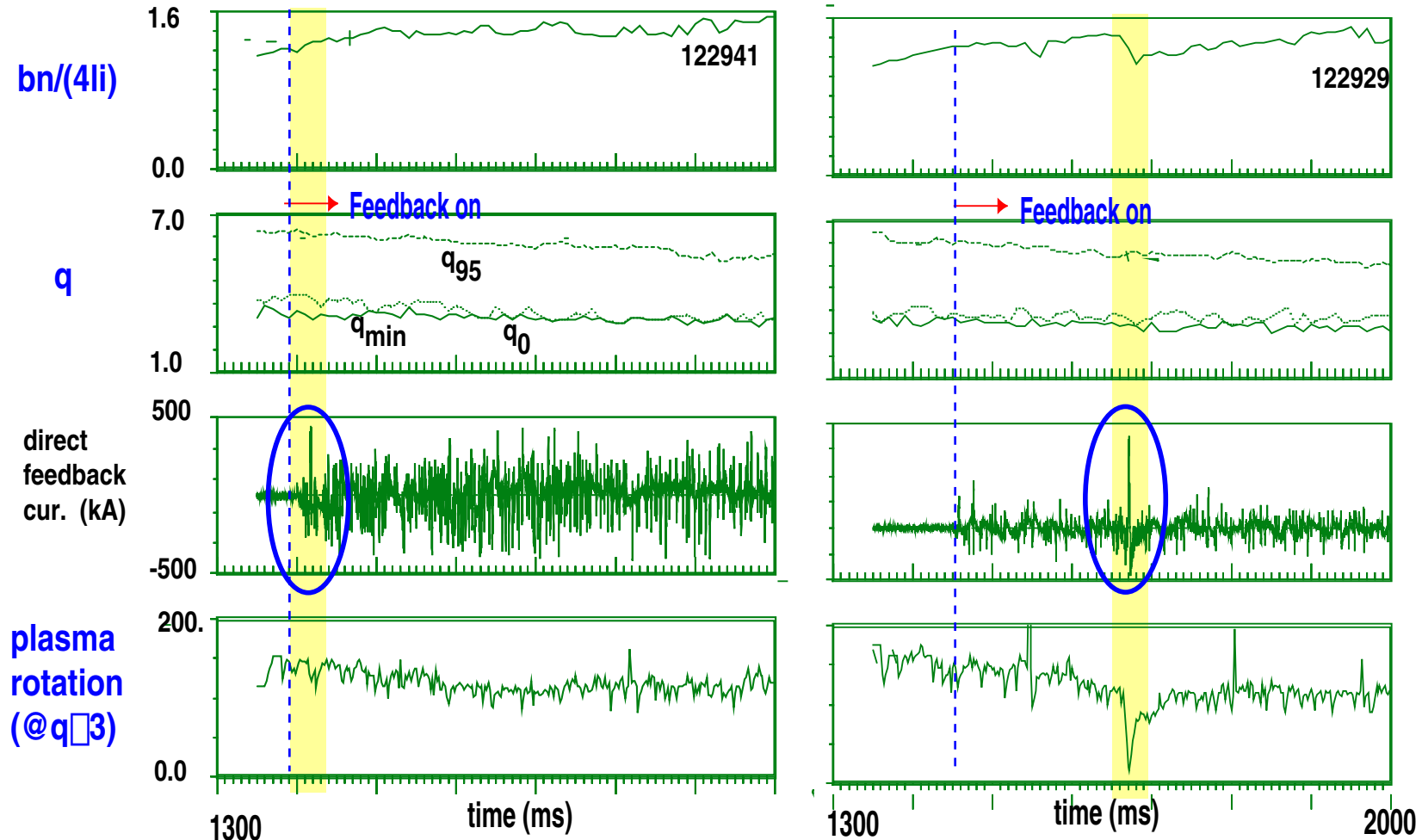
* including lead inductance 50 μ H

Combination of External and Internal Feedback Assists Achievement of High q_n AT Plasmas



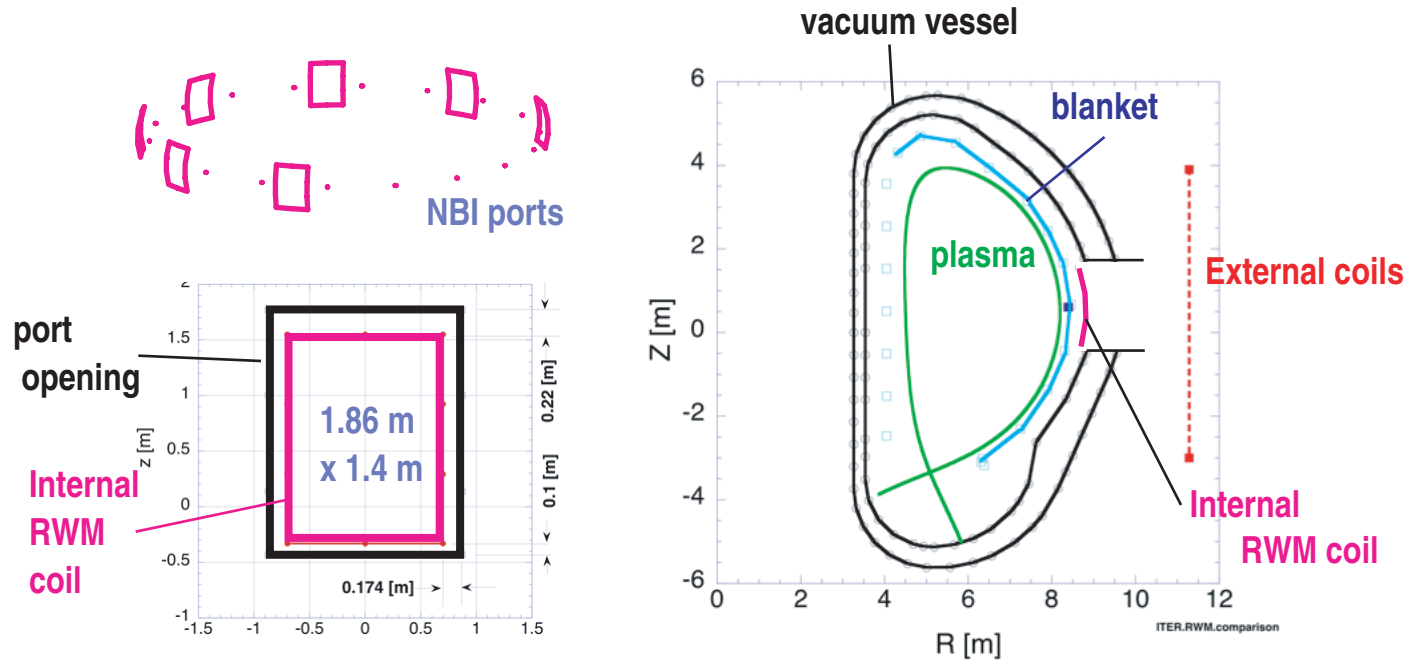
Unstable RWM is Excited in An Predictable Manner

- Occasionally RWM stabilization by combined rotation and feedback becomes marginal, requesting large feedback current.



Internal 7 coils for RWM control in ITER

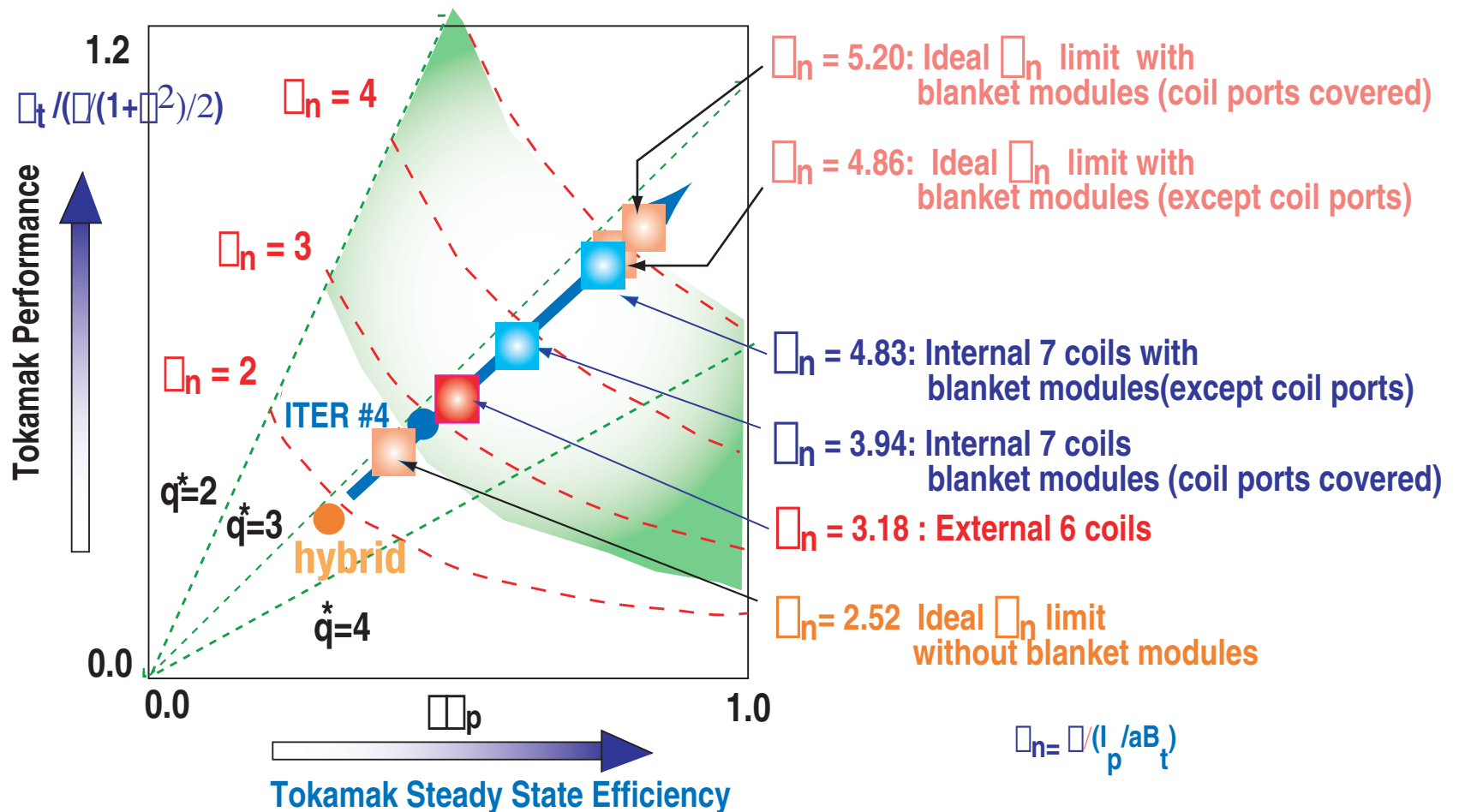
- RWM coils are located at every 40 degrees except NBI ports



- Blanket without opening: 9 ms L/R time assumed
- Thin shell model

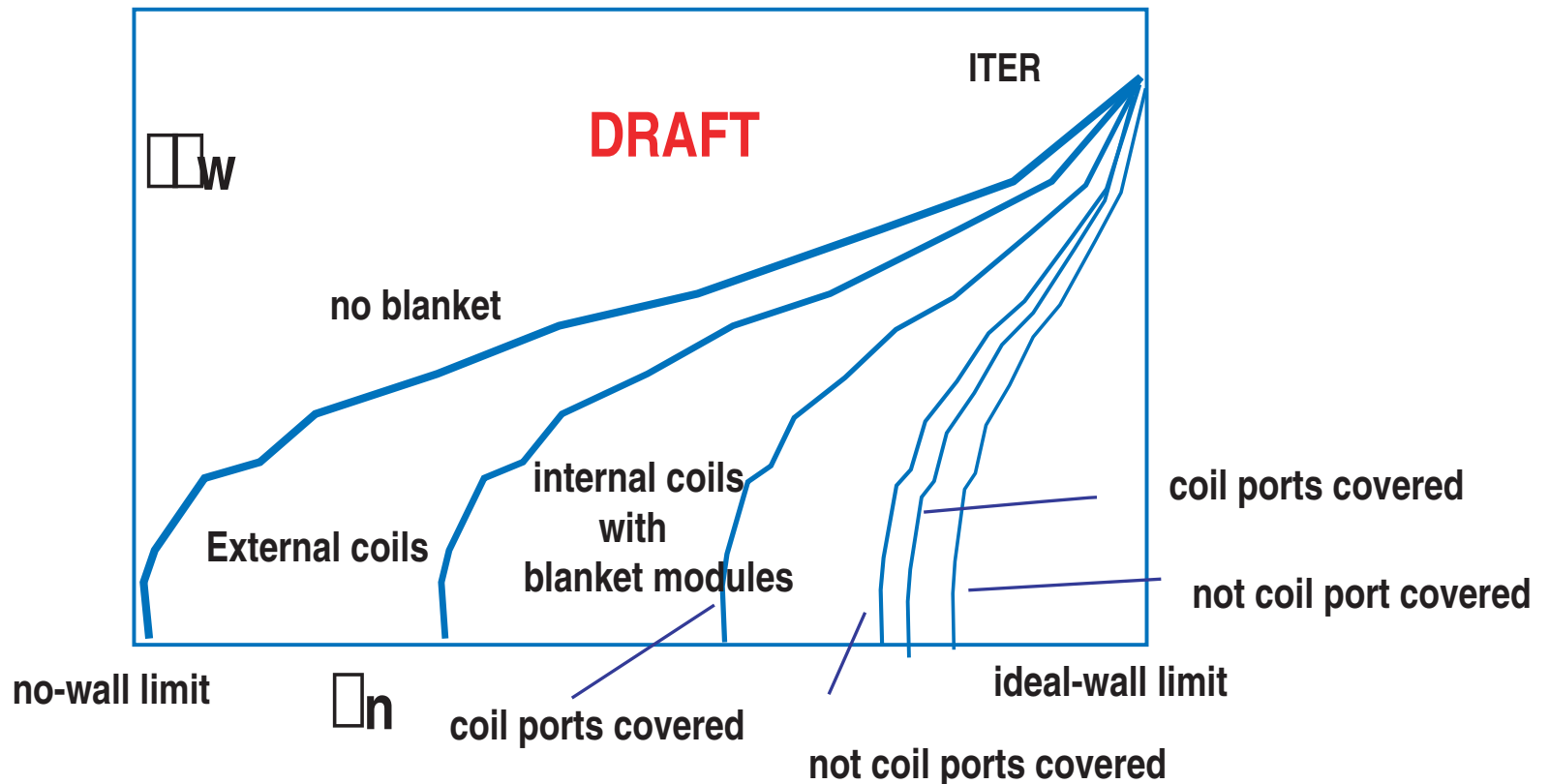
	T		L	R	ΔB_n (G/kA) pl.surface
Internal	1 turn	7 coils	3.6 μ H	0.18 m-ohm	27.0
External	28 turn	3 pairs	39.2 mH	3.92 m-ohm	5.4

• Internal Coils Outperform External Coils in ITER



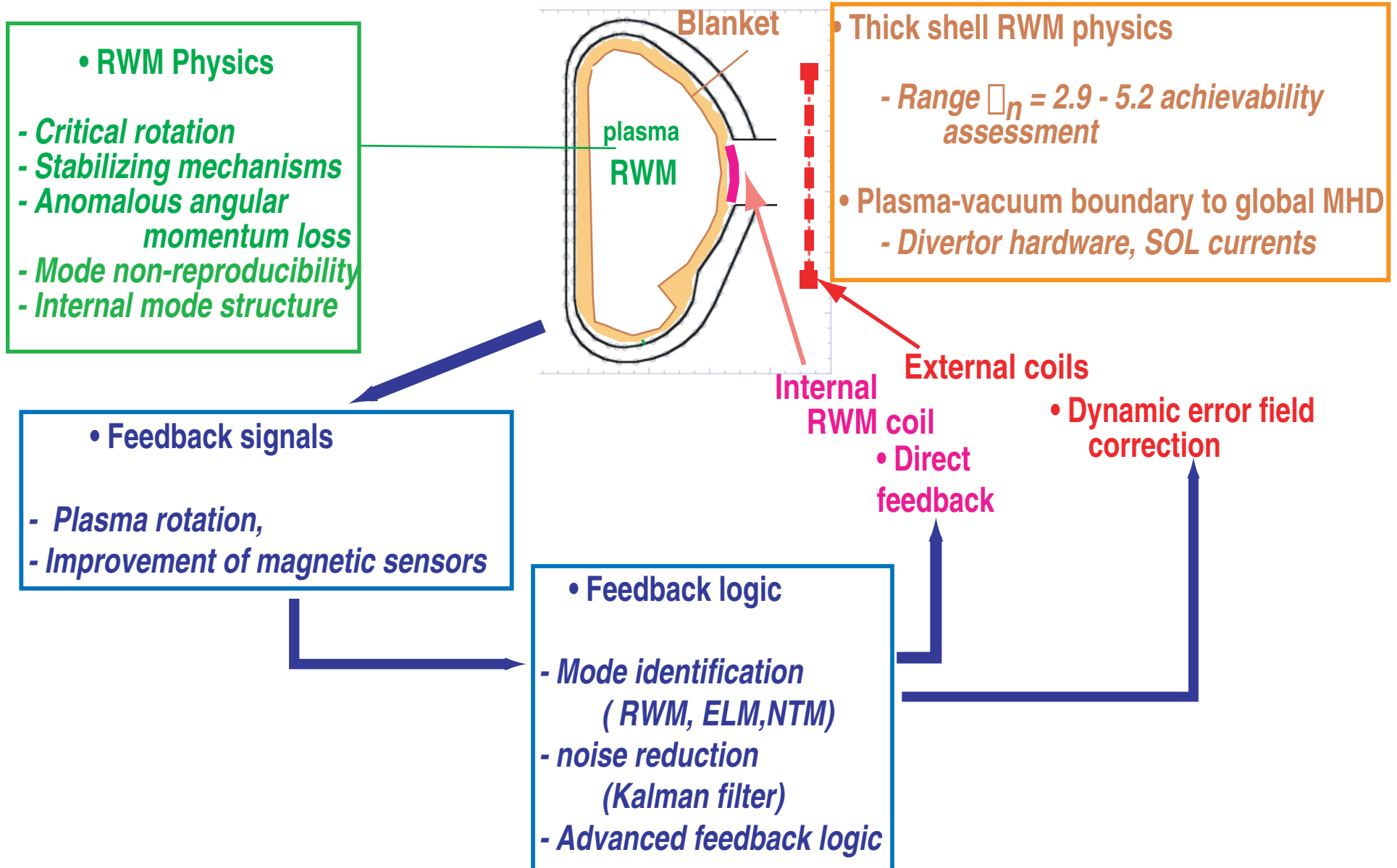
Wide Range β_n 2.5 -5.2 May be Sustainable with Internal Coils

- **Achievability:** depending on the effectiveness of blanket against external kinks



- **Important factors :**
 - Plasma-vacuum boundary physics
 - Thick shell RWM physics. ...
 - Joint experiments with various devices: essential to assess these issues

RWM Issues for Next Step



Plan for Addressing Open Issues

Subject

Contributions to Burning Plasmas

- RWM Physics

- RWM damping mechanisms
 - quantitative comparison with numerical codes
 - critical plasma rotation
 - Mode rigidity
 - internal structure measurement by MSE
 - RWM triggering mechanisms
 - RWM coupling to ELM and others
 - Thick shell RWM physics
 - Plasma-Vacuum boundary to global MHD
- > feedback necessity
- > control logic
- > control logic
- > achievable β_n limit
- > control logic

- Feedback

- Crucial test of feedback with
 - reduced NBI momentum input (DIID)
 - Optimization of Internal and external coil combination
 - Feedback optimization with internal coils
 - Non magnetic signal use for feedback
- > achievable β_n limit
- > overall optimization
- > Internal control coils
- > Improvement of dynamic error field correction