

Lawrence Livermore National Laboratory University of California Livermore, California 94551



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LLNL Ground Water Project

1997 Annual Report

Technical Editors:

J. Hoffman* M. Maley* B. Qualheim R. Bainer E. Folsom M. Dresen*

Contributing Authors:

J. Aarons	G. Howard
S. Bahowick	G. Kumamoto
R. Blake	W. McNab
Z. Demir*	C. Noyes*
L. Berg*	T. Pico
K. Folks	M. Ridley
R. Gelinas	S. Shukla
F. Hoffman	

*Weiss Associates, Emeryville, California



Environmental Protection Department Environmental Restoration Program and Division

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Table of Contents

Su	Immary
1.	Introduction1
2.	Regulatory Compliance1
	2.1. CERCLA Documents1
	2.2. Milestones and Activities
	2.3. Community Relations
3.	Ground Water Sampling4
4.	Ground Water Flow and Transport Modeling4
	4.1. Treatment Facility B Model5
	4.2. Site-Wide Model for HSUs 1B and 25
	4.3. Site-Wide Model for all HSUs5
	4.4. Zone 7 Project
5.	Annual Summary of Remedial Action Program
	5.1. Treatment Facility A7
	5.1.1. Performance Summary7
	5.1.2. Field Activities
	5.2. Treatment Facility B
	5.2.1. Performance Summary
	5.2.2. Field Activities
	5.3. Treatment Facility C9
	5.3.1. Performance Summary9
	5.3.2. Field Activities
	5.4. Treatment Facility D 10
	5.4.1. Performance Summary 10
	5.4.2. Field Activities 11
	5.4.3. Field Scale Pilot Tests 11
	5.5. Treatment Facility E 11
	5.5.1. Performance Summary 12
	5.5.2. Field Activities
	5.6. Treatment Facility G 12

5.6.1. Performance Summary 12
5.6.2. Field Activities
5.7. Treatment Facility 406 13
5.7.1. Performance Summary
5.7.2. Field Activities
5.8. Vapor Treatment Facility 51814
5.8.1. Performance Summary14
5.8.2. Field Activities
5.8.3. Soil Vapor Extraction Treatability14
5.9. Ground Water Treatment Facility 518 15
5.10. Treatment Facility 547515
5.10.1. Field Activities
5.10.2. Ground Water Treatability Test
6. Trends in Ground Water Analytical Results 16
References

List of Figures

- Figure 1. Locations of Livermore Site monitor wells, piezometers, extraction wells and treatment facilities, December 1997.
- Figure 2. Comparison of measured (top) and simulated (bottom) aqueous TCE concentrations in HSU 1B for 1996.
- Figure 3. Comparison of measured (top) and simulated (bottom) aqueous TCE concentrations in HSU 2 for 1996.
- Figure 4. Total VOC mass removed from the Livermore Site subsurface.
- Figure 5. Ground water elevation contour map based on water levels collected from 126 wells completed within HSU 1B showing estimated hydraulic capture areas, LLNL and vicinity, December 1997.
- Figure 6. Ground water elevation contour map based on water levels collected from 152 wells completed within HSU 2 showing estimated hydraulic capture areas, LLNL and vicinity, December 1997.
- Figure 7. Ground water elevation contour map based on water levels collected from 60 wells completed within HSU 3A showing estimated hydraulic capture areas, LLNL and vicinity, December 1997.
- Figure 8 Ground water elevation contour map based on water levels collected from 23 wells completed within HSU 4 showing estimated hydraulic capture areas, LLNL and vicinity, December 1997.

- Figure 9. Ground water elevation contour map based on water levels collected from 43 wells completed within HSU 5 showing estimated hydraulic capture areas, LLNL and vicinity, December 1997.
- Figure 10. Isoconcentration contour map of total VOCs for 128 wells completed within HSU 1B based on samples collected in the fourth quarter of 1997 (or the next most recent data).
- Figure 11. Isoconcentration contour map of total VOCs for 170 wells completed within HSU 2 based on samples collected in the fourth quarter of 1997 (or the next most recent data).
- Figure 12. Isoconcentration contour map of total VOCs for 71 wells completed within HSU 3A based on samples collected in the fourth quarter of 1997 (or the next most recent data).
- Figure 13. Isoconcentration contour map of total VOCs for 37 wells completed within HSU 4 based on samples collected in the fourth quarter of 1997 (or the next most recent data).
- Figure 14 Isoconcentration contour map of total VOCs for 45 wells completed within HSU 5 based on samples collected in the fourth quarter of 1997 (or the next most recent data).
- Figure 15. 1997 TFA extraction wells, pipelines and discharge location.
- Figure 16. 1997 TFB extraction wells, pipelines and discharge location.
- Figure 17. 1997 TFC extraction wells, pipelines and discharge location.
- Figure 18. 1997 TFC Southeast extraction wells, pipelines and discharge location.
- Figure 19. 1997 TFD extraction wells, pipelines and discharge location.
- Figure 20. 1997 TFD East extraction wells, pipelines and discharge location.
- Figure 21. 1997 TFD West extraction wells, pipelines and discharge location.
- Figure 22. 1997 TFE East extraction wells, pipelines and discharge location.
- Figure 23. 1997 TFG-1 extraction wells, pipelines and discharge location.
- Figure 24. 1997 TF406 extraction wells, pipelines and discharge location.

List of Tables

- Table 1.
 1997 Livermore Site Livermore Site Remedial Action Implementation Plan milestones.
- Table 2Summary of 1997 Livermore Site VOC remediation.
- Table 3. Summary of cumulative Livermore Site VOC remediation.

Appendices

Appendix A—Well Construction and Closure Data	. A-1
Appendix B—Hydraulic Test Results	B-1
Appendix C—1998 Ground Water Sampling Schedule	C-1
Appendix D—1997 Drainage Retention Basin Annual Monitoring Program Summary	. D-1

Summary

The major Livermore Site Ground Water Project (GWP) restoration activities conducted in 1997 are:

- 1. The Lawrence Livermore National Laboratory (LLNL) Livermore Site GWP produced two major Comprehensive Environmental Response, Compensation, and Liability Act documents in 1997 according to the Remedial Action Implementation Plan schedule (RAIP): The Five-Year Review, issued August 1, 1997 and finalized in December 1997; and Draft Remedial Design Report No. 4 (RD4) issued August 21, 1997. Two Explanations of Significant Differences (ESDs) were issued in April 1997 describing modifications to the remediation systems at Treatment Facilities A and B (TFA and TFB), and a change in metals discharge requirements. Twelve additional documents or letter reports were submitted to the regulatory agencies in 1997, consisting of 10 Remedial Project Managers Meeting Summaries, the GWP 1997 Annual Report, and an updated Quality Assurance Project Plan. All six Department of Energy (DOE)/LLNL/RAIP milestones 1997 were met ahead of schedule.
- 2. The Community Work Group met twice in 1997 to discuss topics including the DOE budget, progress on Livermore Site cleanup, the two ESDs, the Priority List/Consensus Statement, the Five-Year Review, and RD4.
- 3. In 1997, the GWP submitted 890 ground water samples for analyses, collected during 820 individual sampling events from 352 wells and piezometers.
- 4. The three-dimensional ground water flow and contaminant transport model developed in 1996 was expanded in 1997, and a summary of the preliminary results for the TFB area was completed in 1997. We began to change our primary modeling computer code to FEFLOW from CFEST. In 1998, FEFLOW will be used to expand a site-wide model for all hydrostratigraphic units.
- 5. LLNL began a project for the Alameda Flood Control and Water Conservation District Zone 7, to assess future ground water use in the basin surrounding LLNL by using the existing Livermore Site ground water models. A report to Zone 7 is being prepared for submittal in early 1998.
- 6. The 1997 extraction wells, extraction rates, and estimated volatile organic compound (VOC) mass removed at TFA, TFB, Treatment Facility C (TFC), Treatment Facility D (TFD), Treatment Facility E (TFE), Treatment Facility G (TFG), Treatment Facility 406 (TF406), and Vapor Treatment Facility 518 (VTF518) areas are summarized in Table Summ-1.
- 7. Construction activities in 1997 included:
 - Replacement of the ground water treatment system at TFA to a more cost-effective, large-capacity air-stripping system.
 - Construction of portable treatment unit stations at TFC Southeast, TFD West, TFD East, and Ground Water Treatment Facility 518 (TF518).

- 8. Sixteen wells installed in 1997 are listed in Table Summ-2.
- 9. Hydraulic tests conducted in 1997 are presented in Table Summ-3.
- 10. During 1997, DOE/LLNL operated TFA, TFB, TFC, TFD, TFE, TFG, TF406, and VTF518. By the end of 1997, a total of about 569 million gal of ground water and almost 6.2 million cubic ft of vapor have been processed, removing more than 334 kg of VOCs.

Treatment facility area	Extraction wells	Extraction rate	Estimated total VOC mass removed (kg)
TFA	W-109, W-262, W-408, W-415, W-457, W-518, W-520, W-522, W-601, W-602, W-603, W-609, W-614, W-712, W-903, W-904, W-1004, W-1009	270-340 gpm	18.4
TFB	W-357, W-610, W-620, W-621, W-655, W-704	40-45 gpm	6.8
TFC	W-701, W-1015, W-1102, W-1103, W-1104, W-1116, W-1213	45-55 gpm	9.4
TFD	W-351, W-906, W-907, W-1208, W-1215, W-1216, W-1301, W-1303, W-1306, W-1307	60-100 gpm	55.0
TFE	W-566, W-1109	15-20 gpm	15.9
TFG	W-1111	8 gpm	0.6
TF406	GSW-445, W-1114	4-20 gpm	0.9
VTF518	SVI-518-201, SVI-518-303	20-50 scfm	40.6
TF5475	W-1302	1-2 gpm	0.1
1997 Total			147.7

Table Summ-1. 1997 extraction wells, extraction rates and estimated VOC mass removed.

Notes:

kg = Kilograms.

gpm = Gallons per minute.

scfm = Standard cubic feet per minute.

Treatment facility area	Well(s)
TFD	W-1303, W-1304, W-1306, W-1307, W-1308, W-1311, W-1401, W-1402, W-1403, W-1404, W-1405, W-1406, W-1407
TF406	W-1309, W-1310
TF5475	W-1302

Table Summ-2. Wells installed in 1997.

Note:

TF5475 = Ground Water Treatment Facility 5475.

Treatment facility area	Well(s)
TFA	W-1002, W-1003, W-1005, W-1006, W-1107, W-1214, W-1217, W-1227
TFB	W-1226
TFC	W-1224
TFD	W- 314, W-1218, W-1220, W-1301, W-1303, W-1304, W-1306, W-1307, W-1308, W-1311, W-1401, W-1402
TFE	W-1008, W-1219
TFF/TF406	W-1309, W-1310
TF518	W-211
T-5475	W-1225

Table Summ-3. Summary of 1997 hydraulic tests.

Notes:

TF518 = Ground Water Treatment Facility 518.

TFF = Treatment Facility F.

1. Introduction

This report summarizes the 1997 Lawrence Livermore National Laboratory (LLNL) Livermore Site Ground Water Project (GWP) activities in six sections: Regulatory Compliance; Ground Water Sampling; Flow and Transport Modeling; Annual Summary of Remedial Action Program, including discussions of treatment facility activities; and Trends in Ground Water Analytical Results. The 1997 GWP quarterly self-monitoring reports (Lamarre and Littlejohn, 1997a; 1997b; Bainer and Littlejohn, 1997a; 1998) were issued separately.

Figure 1 shows the locations of monitor wells, piezometers, extraction wells, and treatment facilities at the Livermore Site and vicinity as well as other areas referenced in this report. Wells and boreholes drilled in 1997 are shown in larger type.

Appendices A through D present Well Construction and Closure Data, Hydraulic Test Results, the 1998 Ground Water Sampling Schedule, and the 1997 Drainage Retention Basin Annual Monitoring Program Summary. Ground water volatile organic compound (VOC) analyses, water level elevations, and the Treatment Facility F/Treatment Facility 406 (TFF/TF406) area ground water VOC and fuel hydrocarbon (FHC) analyses are available on request.

2. Regulatory Compliance

In 1997, the U.S. Department of Energy (DOE)/LLNL submitted documents required by the Comprehensive Environmental Response, Compensation, and Liability Act (CERCLA) and the Livermore Site Federal Facility Agreement (FFA). In addition, DOE/LLNL continued environmental restoration and community activities as discussed below.

2.1. CERCLA Documents

During 1997, DOE/LLNL issued two CERCLA documents for the Livermore Site according to the amended schedule in the Remedial Action Implementation Plan (RAIP) (Dresen et al., 1993). The Five-Year Review (Berg et al., 1997a) was submitted to the regulatory agencies on August 1, 1997, and was subsequently finalized and approved by the U.S. Environmental Protection Agency (EPA) in December 1997. Draft Remedial Design Report No. 4 (RD4) (Berg et al., 1997b) was submitted on August 21, 1997.

In addition, DOE/LLNL prepared a status report presenting the hydrogeology, wellfield design, and treatability studies for the Treatment Facility 5475 (TF5475). The status report was issued one day ahead of scheduled on February 24, 1997 (Lamarre and Littlejohn, 1997c).

Two Explanations of Significant Differences (ESDs) were also prepared and approved by the regulatory agencies. The first ESD describes a change from ultraviolet light/hydrogen peroxide (UV/H_2O_2) and air stripping remediation to air stripping only at Treatment Facilities A and B (TFA and TFB) (Berg et al., 1997c). The second ESD was for a change in metals discharge

requirements based on wet and dry season beneficial use (Berg et al., 1997d). Both ESDs were issued in April 1997.

A Draft Action Memorandum (Bainer and Berg, 1997) for an emergency removal action was prepared in response to the discovery of undocumented buried capacitors during excavation for the National Ignition Facility (NIF) in the northeast part of the Livermore Site. Appropriate public notification and information activities were conducted in support of this removal action. The Draft Action Memorandum was submitted on October 31, 1997 for a 30-day community review and comment period, and DOE/LLNL are currently responding to community comments. The final Action Memorandum will be issued in February 1998. A Closeout Report for the emergency removal action was submitted in December 1997 (Bainer and Littlejohn, 1997b).

As required by the FFA, DOE/LLNL issued the 1996 Ground Water Project Annual Report (Hoffman et al., 1997). DOE/LLNL also issued ten Remedial Project Managers' (RPMs') meeting summaries; the March and June (Lamarre and Littlejohn, 1997a; 1997b, respectively), and the September and December summaries (Bainer and Littlejohn, 1997a; 1998, respectively) included quarterly self-monitoring data. LLNL also prepared an updated Quality Assurance Project Plan (Dibley, 1997) for regulatory review and comment.

2.2. Milestones and Activities

Table 1 presents the 1997 RAIP milestones (Table 5 in Dresen et al., 1993) for the Livermore Site. All six milestones were completed ahead of schedule.

Livermore Site Environmental Restoration activities in 1997 also included the following:

- Implemented Engineered Plume Collapse (EPC) to accelerate mass removal and site cleanup. EPC incorporates hydrostratigraphic unit analysis, smart pump and treat, source isolation, Portable Treatment Unit (PTU) technology, and treatment of VOCs in fine-grained sediments.
- Gave presentations to the regulatory agencies on the hydrostratigraphy of the TF5475 area and catalytic reductive dehalogenation bench-scale studies.
- Designed a treatability test for treating ground water using granular activated carbon (GAC).
- Re-evaluated the sampling frequency of the guard wells listed in the Compliance Monitoring Plan and proposed a reduced sampling plan that is cost-effective and remains protective of human health and the environment (Lamarre and Littlejohn, 1997d). The regulatory agencies are still reviewing this proposal.
- Provided support for an infiltration study in the southwest part of the site funded through the Environmental Management Science Program. See Section 5.1 for further discussion.
- Negotiated a revised Livermore Site Consensus Statement/Priority List and the RAIP milestone schedule on July 17, 1997 (Lamarre and Littlejohn, 1997e).
- Prepared and submitted to the regulatory agencies Standard Operating Procedures (SOPs) for ground water sampling that included procedures for low-volume sampling (Bainer

and Littlejohn, 1997c), and incorporated EPA comments. The final low-volume sampling SOPs will be issued in 1998.

- Implemented a more efficient format to report data in the quarterly self-monitoring reports beginning with the second quarter report (Lamarre and Littlejohn, 1997b).
- Began operation of a high-efficiency air stripper at TFA on June 18, 1997. See Section 5.1 for further discussion.
- Changed the quarterly, semiannual and annual self-monitoring sampling schedule, with regulatory concurrence, to collect samples at the beginning of the reporting period to ensure the data are collected and analyzed in time to include in the quarterly reports (Bainer and Littlejohn, 1997d). In addition, DOE/LLNL changed the annual self-monitoring sampling for all treatment facilities to January of each year to help ensure that there is enough water to collect a receiving water sample.
- Began *in situ* pilot testing of catalytic reductive dehalogenation in the TF5475 area on August 8, 1997. See Section 5.10.2 for further discussion.
- Requested and was granted an increase in the TFA discharge rate from 350 gallons per minute (gpm) to 500 gpm (Bainer and Littlejohn, 1997e; Rochette, 1997).
- Started a treatability test on a Solar-powered Water Activated-carbon Treatment (SWAT) unit on August 13, 1997. See Section 5.4.3 for further discussion.
- Performed a removal action for buried drums and capacitors discovered during excavation for the NIF (Bainer and Berg, 1997).
- Performed geophysical surveys to determine the potential of finding more undocumented buried waste in the NIF construction area. Exploratory boreholes will be drilled in early 1998.
- Met with the Alameda County Flood Control and Conservation District, Zone 7 (Zone 7) to discuss a cooperative effort to model the water needs for Livermore Valley's increasing population and agriculture needs. See Section 4.4 for further discussion.
- Oversaw identification, stabilization, and excavation of mammoth bones at the NIF construction site.
- Started construction of ground water Treatment Facility 518 (TF518), which is scheduled to start operation by January 30, 1998.

2.3. Community Relations

In August 1997, DOE/LLNL held a celebration of five years of successful environmental restoration at the Livermore Site since the signing of the Record of Decision (U.S. DOE, 1992). The celebration was attended by elected officials, DOE, regulatory agencies, LLNL, and community representatives.

The Community Work Group (CWG) met twice in 1997 to discuss the DOE budget, progress of Livermore Site cleanup, the two ESDs, the Priority List/Consensus Statement, the Five-Year

Review, and RD4. There was ongoing correspondence and communication with CWG members throughout the year.

Other Livermore Site community relations activities in 1997 included communications and meetings with local, regional and national interest groups; other community organizations; public presentations including those to local Realtors, national and northern California peace leaders, and international student and business groups; producing and distributing the *Environmental Community Letter*; maintaining the Information Repositories and the Administrative Record; conducting tours of site environmental activities; and responding to public and news media inquiries. DOE/LLNL met three times with members of Tri-Valley Citizens Against a Radioactive Environment and their technical advisor as part of the activities funded by an EPA Technical Assistance Grant.

3. Ground Water Sampling

In 1997, the GWP submitted 890 ground water samples for analysis. These samples were collected during 820 individual sampling events from 352 sampling locations, consisting of 275 monitor wells, 55 source investigation piezometers, 13 TFF/TF406 wells and nine Zone 7 or domestic wells. The samples were analyzed for VOCs, FHCs, polychlorinated biphenyls, metals, radionuclides, or combinations of these analyses depending on the compounds of concern.

Livermore Site ground water sampling frequency recommendations are updated quarterly using a cost-effective sampling algorithm that evaluates trends in contaminant levels in each well over an 18-month period. The sampling frequency is determined by the treatment facility Task Leaders based on algorithm results and other data. The main features of the algorithm that help to determine the sampling frequencies are based on the following criteria:

- Wells exhibiting little change [<10 parts per billion (ppb) per year] are sampled annually or biennially.
- Wells exhibiting moderate change (≥ 10 ppb but <30 ppb per year) are sampled semiannually.
- Wells showing large change (\geq 30 ppb) are sampled quarterly.
- Wells with less than 18 months of analytical history are sampled quarterly for the first 18 months, then the algorithm logic, and input from the Task Leaders for each treatment facility area, determine the sampling frequency.

Wells located at the leading edge of VOC plumes are sampled quarterly. The sampling schedule for 1998 is presented in Appendix C.

4. Ground Water Flow and Transport Modeling

Ground water flow and contaminant transport models are used at the Livermore Site to improve our ability to forecast, monitor, and interpret the progress of the ground water remediation program. Modeling results are also used to support ongoing subsurface characterization. Ground water flow and transport modeling is part of our overall support of the design and performance evaluation of Livermore Site remediation systems. In 1997, we further developed our three-dimensional (3-D) ground water model for the Livermore Site. The 3-D model builds vertical resolution into the two-dimensional (2-D) model previously developed for the Livermore Site (Tompson, et al., 1995).

4.1. Treatment Facility B Model

In 1997, a 3-D ground water flow and contaminant transport model was developed that focused on the transport of dissolved trichloroethylene (TCE) in hydrostratigraphic units (HSUs) 1B and 2 in the TFB area. A technical note containing a description of the 3-D model calibration and a summary of the preliminary results was completed in August 1997 (Demir et al., 1997). This 3-D model was developed using the CFEST (Coupled Flow, Energy and Solute Transport) computer code (Gupta, 1987). The modeling was an extension of the TFA area model performed in 1996 (Vogele et al., 1996).

As described in Demir et al. (1997), the 3-D flow model was calibrated to measured ground water elevation data collected from the Livermore Site monitor wells. The contaminant transport portion of the model was calibrated to TCE ground water concentrations observed in the TFB area from 1988 through 1995. These simulations were comprised of a series of remedial pumping time steps that were constructed to reflect changes in extraction well flow rates. Results from the preliminary simulations were within plausible uncertainty limits of the model (Figs. 2 and 3).

The TFB model indicates that the current TFB extraction wells mitigate the offsite migration of the VOC plume. Results of the model analysis show that high pumping rates at TFA induce part of the TFB area plume to migrate towards TFA. Further model analysis indicates that this interference is controllable by adding extraction locations between TFA and TFB. The first of these new locations is planned for installation in early 1998.

4.2. Site-Wide Model for HSUs 1B and 2

The conceptual model used for the TFA and TFB areas was further expanded to simulate the migration of perchloroethylene (PCE), TCE and total VOC plumes in HSU-1B and HSU-2 for the entire Livermore Site. The results of these simulations will be presented in an interim report in early 1998. The site-wide simulations indicated the need for better characterization of the individual VOC plumes with respect to their historical behavior and the definition of the source areas.

4.3. Site-Wide Model for all HSUs

The development of a 3-D model for all Livermore Site HSUs will require detailed hydrogeological and contaminant data for the entire Livermore Site and adjacent areas. In 1997, work began on developing these site-wide data sets. To improve the accuracy of simulations and to better simulate the contaminant migration in the source areas, all available data regarding the subsurface hydraulic properties are being analyzed. The results of this work, together with the

detailed HSU definitions, will be used to expand the current 3-D model analysis to include all HSUs beneath the Livermore Site.

An evaluation of the migration history of individual plumes was also begun in 1997. As a result of this work, plumes for 11 individual VOC constituents and total VOCs were generated for each quarter from 1987 to 1997 and displayed through a web-based graphical interface for analysis. This approach is being expanded to inorganic constituents which can serve as additional indicators to further understand ground water movement beneath the site and expedite cleanup.

In 1997, we began to change our primary modeling computer code from CFEST to FEFLOW. FEFLOW is similar to CFEST in that it is a finite element ground water flow and contaminant transport model. However, FEFLOW has superior graphical user interfaces and improved features for handling more complex hydrogeologic boundary conditions and parameters compared to CFEST. We are converting our previous models into FEFLOW and will be performing the site-wide model for all HSUs using FEFLOW.

4.4. Zone 7 Project

In 1997, Zone 7 approached LLNL about using the existing LLNL ground water models to provide assistance to Zone 7 on issues regarding future ground water use in the basin surrounding LLNL. The objective of this investigation is to determine the subsurface volume of ground water and the volume of potential subsurface storage in the basin to answer short- and long-term water resources management questions. For this preliminary investigation, the volume of ground water flow in the basin was estimated using the existing 2-D CFEST flow model (Tompson et. al., 1995). The model was also used to test the influence of different rates of extraction and reinjection within the basin. A volumetric calculation was performed to determine the volume of potential ground water storage in the basin, and a potential drawdown or buildup of ground water in the area of interest. A report to Zone 7 is being prepared and should be ready by early 1998.

5. Annual Summary of Remedial Action Program

This section summarizes activities performed during 1997 to support the Remedial Action Program at the Livermore Site, and includes treatment system design, new construction, modifications to existing systems, treatment facility performance, treatability tests, well installation, well abandonment, and hydraulic tests performed during 1997. The volume of ground water and soil vapor treated at the facilities and the estimated VOC mass removed from the subsurface during 1997 and historically is presented in Tables 2 and 3, respectively. A graph of VOC mass removal at the Livermore Site since 1989 is presented in Figure 4. Figures 5 through 9 show the hydraulic capture areas, based on December 1997 ground water elevation data, in the vicinity of the ground water extraction wells for HSUs 1B, 2, 3A, 4, and 5, respectively. Figures 10 through 14 show fourth quarter total VOC isoconcentrations in the same five HSUs. Figures 15 through 24 show treatment facility extraction wells, pipelines, discharge locations, and self-monitoring program sampling stations.

5.1. Treatment Facility A

TFA is located in the southwestern quadrant of the Livermore Site near Vasco Road and East Avenue (Fig. 1). In 1997, TFA treated ground water from 18 extraction wells, including six HSU 1B wells (W-262, W-408, W-520, W-601, W-602, and W-1004), eleven HSU 2 wells (W-109, W-415, W-457, W-518, W-520, W-603, W-609, W-614, W-903, W-904 and W-1009), and one HSU 3A well (W-712). TFA was operated at flow rates ranging from 270 to 340 gpm.

In June 1997, a new ground water treatment system was installed at TFA. From 1989 to mid 1997, TFA processed VOCs in ground water using a UV/H_2O_2 method that breaks down VOCs into carbon dioxide and chloride ions. The water was further processed with an air stripper to remove any remaining VOCs. In June, the UV/H_2O_2 system was replaced with a more cost-effective, large-capacity air-stripping system. The effluent air from the air stripper is passed through GAC to remove VOCs. The treated effluent air from the air stripper is discharged to the atmosphere. This new system is permitted to treat up to 500 gpm of ground water.

Treated ground water from TFA is discharged to the Recharge Basin, located about 2,000 ft southeast of TFA on DOE property administered by Sandia National Laboratories (Figs. 1 and 15). On several occasions in 1997, while attempting to maximize ground water treatment and capture with the UV/H_2O_2 system, TFA exceeded its waste discharge requirement (WDR) limit of 5 ppb total VOCs in ground water effluent. These discharges were reported to the Regional Water Quality Control Board, and at no time did VOCs in TFA discharge exceed a Maximum Contaminant Level. Since startup of the new system, TFA has not exceeded the 5 ppb total VOC WDR limit.

From 1989 through 1994, TFA treated ground water extracted from well W-415. The TFA North and TFA Arroyo Pipelines connected nine additional extraction wells to TFA in September 1994. The TFA South Pipeline connected eight additional extraction wells to TFA in July 1995 (Fig. 15).

In 1997, in conjunction with LLNL's Geosciences and Environmental Technology Division, a vadose zone study area was constructed in the southwest corner of the TFA area for conducting infiltration studies. In late October and early November, about 6,300 gallons of water containing noble gas isotopes were introduced into the vadose zone at a rate of about 0.4 gallons per minute. The infiltration was imaged using electrical resistance tomography (ERT), which showed that the water reached the water table (\approx 70 ft below ground surface [bgs]) within a day of being released. Changes in moisture content in the vadose zone were detected barometrically, and also electrically by monitoring resistance changes in gypsum blocks deployed to specific depths beneath the site. Preliminary results indicate that the dissolved noble gas tracers coming out of solution at the water table are rapidly dissipating in the vadose zone. Additional tracer and ERT experiments are planned for spring of 1998.

5.1.1. Performance Summary

During 1997, TFA treated more than 128 million gal of ground water containing an estimated 18.4 kg of VOCs (Table 2). Since system startup in 1989, TFA has treated nearly 391 million gal of ground water and removed about 94.3 kg of VOC mass from the subsurface (Table 3).

The TFA VOC plumes in HSUs 1B, 2, and 3A continue to be hydraulically controlled based on the capture zone analysis shown on the ground water elevation contour maps (Figs. 5, 6, and 7) and the total VOC isoconcentration maps (Figs. 10, 11, and 12) for each HSU.

5.1.2. Field Activities

Sixteen boreholes were drilled in the TFA area in 1997 for the infiltration study. Three boreholes (SEA-INF-001, SEA-INF-002, and SEA-INF-003) were completed in the unsaturated zone using FLUTe liners. The FLUTe (formerly called SEAMIST) system is an impermeable, everted membrane that carries soil vapor sampling instrumentation down an unlined borehole (Keller and Lowry, 1991). Four boreholes (SIB-INF-004, SIB-INF-005, SIB-INF-006 and SIB-INF-007) were completed as unsaturated zone monitoring wells. Eight boreholes (SIB-INF-008, SIB-INF-009, SIB-INF-010, SIB-INF-011, SIB-INF-013, SIB-INF-014, SIB-INF-015, and SIB-INF-016) were completed as unsaturated zone instrumentation boreholes. One borehole (SIB-INF-012) was completed to 16 ft and was used as the infiltration well for the test.

In 1997, eight one-hour drawdown tests were conducted in the TFA area on wells W-1002, W-1003, W-1005, W-1006, W-1107, W-1214, W-1217, and W-1227. Results are presented in Appendix B. No other hydraulic tests were conducted in the TFA area during 1997.

5.2. Treatment Facility B

TFB is located north of Mesquite Way in the west-central portion of the Livermore Site (Fig. 1). In 1997, TFB treated ground water from six extraction wells, including three HSU 1B wells (W-610, W-620, and W-704), and three HSU 2 wells (W-357, W-621, and W-655). TFB was operated at flow rates ranging from 40 to 45 gpm in 1997.

TFB processes VOCs in ground water using a UV/H_2O_2 and air stripping system similar to TFA. The effluent air from the air stripper is treated using GAC prior to discharge to the atmosphere. Ground water is treated for hexavalent chromium by adding hydrogen peroxide and carbon dioxide.

Treated ground water from TFB is discharged into the north-flowing drainage ditch running parallel to Vasco Road that empties into Arroyo Las Positas to the north. TFB was in compliance with all permits throughout 1997.

From 1990 through 1995, TFB treated ground water extracted from wells W-357 and W-704. The TFB North Pipeline and TFB West Pipeline connected four additional extraction wells to TFB in September 1995 (Figs 1 and 16).

5.2.1. Performance Summary

During 1997, TFB treated about 16.9 million gal of ground water containing an estimated 6.8 kg of VOCs (Table 2). Since system startup in 1990, TFB has treated nearly 65.3 million gal of ground water and removed about 25.5 kg of VOC mass from the subsurface (Table 3).

The TFB VOC plumes in HSUs 1B and 2 continue to be hydraulically controlled based on the capture zone analysis shown on the ground water elevation contour maps (Figs. 5 and 6) and the total VOC isoconcentration maps (Figs. 10 and 11) for each HSU.

5.2.2. Field Activities

No boreholes or wells were drilled or installed in the TFB area during 1997.

In 1997, a one-hour drawdown test was conducted in the TFB area on well W-1226. Results are presented in Appendix B. No other hydraulic tests were conducted in the TFB area during 1997.

5.3. Treatment Facility C

Treatment Facility C (TFC) is located north of Westgate Drive and west of Avenue A in the northwest quadrant of the Livermore Site (Fig. 1). In 1997, TFC treated ground water from six HSU 1B extraction wells (W-701, W-1015, W-1102, W-1103, W-1104, and W-1116).

The PTU location TFC Southeast (TFC-SE) was activated on January 21, 1997, 10 days ahead of its RAIP milestone date. TFC-SE is located near the intersection of Avenue A and Sixth Street in the northwest quadrant of the Livermore Site (Fig. 1). TFC-SE treats ground water from HSU 1B well W-1213. The combined TFC facilities were operated at flow rates ranging from 45 to 55 gpm in 1997.

TFC and TFC-SE process VOCs in ground water using air stripping. The effluent air from the air stripper is treated using GAC prior to discharge to the atmosphere. Ground water is treated for hexavalent chromium using an ion-exchange unit. As with TFB, under the revised discharge permit (Bessette Rochette, 1996), TFC and TFC-SE require treatment for hexavalent chromium.

Treated ground water from TFC is discharged into the drainage ditch that flows northward and empties into Arroyo Las Positas (Fig. 17). Treated ground water from TFC-SE is discharged into a storm sewer that empties into Arroyo Las Positas to the north (Fig. 18). TFC was in compliance with all permits throughout 1997.

From 1993 through 1996, TFC treated ground water extracted from well W-701. The TFC North Pipeline connected five additional extraction wells to TFC in September 1996 (Fig. 17).

5.3.1. Performance Summary

During 1997, the combined TFC facilities treated more than 22.7 million gal of ground water containing an estimated 9.4 kg of VOCs (Table 2). Since 1993, the combined TFC facilities have treated nearly 35.6 million gal of ground water and removed about 15.4 kg of VOC mass from the subsurface (Table 3).

In the TFC area, VOCs are confined to HSU 1B. The VOC plumes in the TFC area continue to be hydraulically controlled based on the capture zone analysis shown on the ground water elevation contour map (Fig. 5) and the total VOC isoconcentration map (Fig. 10) for HSU 1B.

5.3.2. Field Activities

No boreholes or wells were drilled or installed in the TFC area during 1997.

In 1997, a one-hour drawdown test was conducted in the TFC area on well W-1224. Results are presented in Appendix B. No other hydraulic tests were conducted in the TFC area during 1997.

5.4. Treatment Facility D

Treatment Facility D (TFD) is located north of the Drainage Retention Basin (DRB) in the east-central portion of the Livermore Site (Fig. 1). In 1997, TFD treated ground water from four extraction wells, including one HSU 2 well (W-906) one HSU 3A well (W-1208) and two HSU 4 wells (W-351 and W-907).

Two additional extraction locations, TFD West (TFD-W) and TFD East (TFD-E), were activated in 1997 using PTUs. TFD-W is located south of the North Inner Loop Road in the central portion of the Livermore Site (Fig. 1). TFD-W treats ground water from two HSU 2 extraction wells (W-1215 and W-1216). TFD-E is located east of the DRB in the east-central portion of the Livermore Site (Fig. 1). TFD-E treats ground water from four extraction wells, including two HSU 2 wells (W-1303 and W-1306), one HSU 3A well (W-1301), and one HSU 4 well (W-1307). The combined TFD facilities were operated at flow rates ranging from 60 to 100 gpm in 1997.

TFD, TFD-W, and TFD-E process ground water for treatment of VOCs using air stripping. The effluent air from the air stripper is treated using GAC prior to discharge to the atmosphere. Treated ground water from TFD and TFD-E is discharged into the underground pipeline downstream of the DRB weir, and flows northward to Arroyo Las Positas (Figs. 19 and 20). Treated ground water from TFD-W is discharged into a nearby storm sewer that also empties into Arroyo Las Positas (Fig. 21). All TFD facilities were in compliance with all permits throughout 1997.

TFD began operation in September 1994 and treated ground water extracted from wells W-351, W-906, and W-907. In January 1997, well W-1208 was connected to TFD. PTU location TFD-W was activated on April 22, 1997, three days ahead of its RAIP milestone date. PTU location TFD-E was activated on September 16, 1997, 14 days ahead of its RAIP milestone date.

5.4.1. Performance Summary

During 1997, the combined TFD facilities treated more than 48.1 million gal of ground water containing an estimated 55.0 kg of VOCs (Table 2). Since 1994, the combined TFD facilities have treated nearly 60.5 million gal of ground water and removed about 73.4 kg of VOC mass from the subsurface (Table 3).

The TFD area extraction wells hydraulically control VOCs in HSUs 2, 3A, and 4 associated with the East Traffic Circle Landfill and Helipad source areas based on the capture zone analysis shown on the ground water elevation contour maps (Figs. 6, 7, and 8) and the total VOC isoconcentration maps (Figs. 11, 12, and 13) for each HSU.

5.4.2. Field Activities

Thirteen wells were installed in the TFD area during 1997. Extraction wells W-1303 and W-1306 were installed in HSUs 2 and 3A, and W-1307 was installed in HSU-4. These three wells were connected to the TFD-E PTU in 1997. Monitor wells W-1304 and W-1402 were completed in HSU 3A in the TFD-E area. Monitor wells W-1311 and W-1401 were completed in HSU 2 in the TFD-W area.

Extraction well W-1308 was installed in HSU 2 and is planned to be connected to the TFD-Southeast (TFD-SE) PTU location in March 1998 (Fig. 1). Monitor wells W-1404, W-1405, and W-1407 were completed in HSU 2, and wells W-1403 and W-1406 were completed in HSU 4 in the TFD-SE area. Well construction details are provided in Table A-1.

Well W-352 was sealed and abandoned to accommodate expansion of Building 451 (Fig. 1). The well was properly sealed in December 1997 by pressure grouting. Well closure data are presented in Table A-2 of Appendix A.

The TFD-South PTU is scheduled to begin operation in June 1998 (Fig. 1). TFD-South will treat water pumped from wells W-1218 and W-1220.

In 1997, seven one-hour drawdown tests were conducted in the TFD area on wells W-1304, W-1306, W-1307, W-1308, W-1311, W-1401, and W-1402. Seven long-term (72-hour) hydraulic tests were performed in the TFD area to evaluate the effectiveness of proposed extraction wells. Tests were performed on wells W-1301, W-1303, and W-1306 in the TFD-E PTU location, W-1308 and W-314 in the TFD-SE PTU location, and W-1218 and W-1220 in the TFD-South PTU location. The results of these tests indicated that the location and flow rates for all seven of these wells were suitable for use as extraction wells. Results are presented in Appendix B.

5.4.3. Field Scale Pilot Tests

A treatability test of the SWAT unit was conducted from August 13 through November 5, 1997 on well W-361, south of the DRB (Fig. 1). A solar powered pump was used to extract ground water, which was then passed through a series of three 30-lb GAC canisters for treatment. The treated ground water was discharged into the DRB. During the treatability tests in 1997, the SWAT unit treated about 107,000 gal of ground water containing an estimated 1.0 kg of VOCs.

In addition, a PTU was operated at well W-352 from January to August 1997 as part of a pilot test to demonstrate expedited site cleanup. Well W-352 is located north of the South Inner Loop road near Southgate Drive (Fig. 1). Well W-352 was pumped at a rate of about 30 gpm, and about 8 million gal of ground water containing an estimated 7.7 kg of VOCs was treated.

5.5. Treatment Facility E

Multiple PTUs will be located in the Treatment Facility E (TFE) area in the southeastern quadrant of the Livermore Site. In 1997, one PTU, TFE East (TFE-E), was operating in the area. TFE-E is located west of Avenue H near Third Street in the east-central portion of the Livermore Site (Fig. 1). TFE-E, activated in November 1996, treats ground water from two extraction

wells, W-1109 (HSU 2) and W-566 (HSU 5). TFE-E was operated at flow rates ranging from 15 to 20 gpm in 1997.

TFE-E processes ground water for treatment of VOCs using an air stripper, and the effluent air is treated using GAC to remove VOCs prior to discharge to the atmosphere. Treated ground water from TFE-E is discharged into a drainage ditch flowing north into the DRB (Fig. 22). TFE-E was in compliance with all permits throughout 1997.

5.5.1. Performance Summary

During 1997, TFE-E treated about 9.5 million gal of ground water containing an estimated 15.9 kg of VOCs (Table 2). Since system startup in 1996, TFE-E has treated nearly 9.9 million gal of ground water and removed about 17.1 kg of VOC mass from the subsurface (Table 3).

The TFE-E extraction wells provide hydraulic control of VOC source areas in HSUs 2 and 5 in the TFE area based on the capture zone analysis shown on the ground water elevation contour maps (Figs. 6 and 9) and the total VOC isoconcentration maps (Figs. 11 and 14) for each HSU.

5.5.2. Field Activities

No boreholes or wells were drilled or installed in the TFE area during 1997.

In 1997, two one-hour drawdown tests were conducted in the TFE area on wells W-1008 and W-1219. Results are presented in Appendix B. No other hydraulic tests were conducted in the TFE area during 1997.

5.6. Treatment Facility G

Multiple PTUs will be located in the Treatment Facility G Area in the south-central portion of the Livermore Site. In 1997, one PTU, Treatment Facility G-1 (TFG-1), was operating in the TFG area. TFG-1 is located near Avenue B, about 300 ft north of East Avenue in the south-central part of the Livermore Site (Fig. 1). TFG-1, activated in April 1996, treats ground water from extraction well W-1111 (HSU 2) and was operated at a flow rate of about 8 gpm in 1997.

TFG-1 processes ground water for VOC treatment using an air stripper, and the effluent air is treated using GAC to remove VOCs prior to discharge to the atmosphere. Ground water is treated for hexavalent chromium using an ion-exchange unit. As with TFB and TFC, under the revised discharge permit (Bessette Rochette, 1996), TFG-1 requires treatment for hexavalent chromium.

Treated ground water from TFG-1 is discharged to a storm drain located about 50 ft north of TFG-1 (Fig. 23), which empties into Arroyo Seco. TFG-1 was in compliance with all permits throughout 1997.

5.6.1. Performance Summary

During 1997, TFG-1 treated about 3.3 million gal of ground water containing an estimated 0.6 kg of VOCs (Table 2). Since system startup in 1996, TFG-1 has treated nearly

4.3 million gal of ground water and removed about 0.8 kg of VOC mass from the subsurface (Table 3).

TFG-1 extraction well W-1111 provides hydraulic control of the VOC source areas in the TFG area based on the capture zone analysis shown on the ground water elevation contour map (Fig. 6) and the total VOC isoconcentration map (Fig. 11) for HSU 2.

5.6.2. Field Activities

No boreholes or wells were drilled or installed in the TFG area during 1997. No hydraulic tests were conducted on TFG wells during 1997.

5.7. Treatment Facility 406

TF406 is located east of Southgate Drive near East Avenue in the south-central part of the Livermore Site (Fig. 1). In 1997, TF406 treated ground water from two extraction wells, GSW-445 (HSU 4) and W-1114 (HSU 5). TF406 was operated at flow rates ranging from 4 to 20 gpm in 1997.

TF406 processes ground water for VOC treatment using an air stripper, and the effluent air is treated using GAC to remove VOCs prior to discharge to the atmosphere. All treated ground water is discharged to a storm drain that flows to Arroyo Las Positas (Fig. 24). TF406 was in compliance with all permits throughout 1997.

TF406, activated in August 1996, processes ground water from extraction wells GSW-445 and W-1114. In April 1997, well W-1114 was damaged beyond repair during the drilling of new borehole B-1305. Borehole B-1305 was intended as an additional extraction well for TF406. Both wells were subsequently destroyed. Two new extraction wells (W-1309 and W-1310) were installed in 1997 to replace well W-1114 and borehole B-1305. TF406 is scheduled to begin processing ground water from wells W-1309 and W-1310 in February 1998. Cumulative flow from the three wells is projected to be about 30 to 35 gpm. The TF406 extraction wells will provide hydraulic control of VOC plumes in HSUs 4 and 5.

Passive bioremediation continued to be implemented in this area during 1997. Active ground water extraction and treatment for residual dissolved FHCs using TFF was permanently discontinued in 1996 (Hoffman et al., 1997).

5.7.1. Performance Summary

During 1997, TF406 processed about 2.3 million gal of ground water from wells W-1114 and GSW-445 containing an estimated 0.9 kg of VOCs (Table 2). Since system startup in 1996, TF406 has treated nearly 2.7 million gal of ground water and removed about 1.1 kg of VOC mass from the subsurface (Table 3).

5.7.2. Field Activities

Two wells were installed in the TF406 area during 1997. HSU 4 extraction well W-1309 was installed adjacent to the TF406 PTU and will augment extraction from well GSW-445. HSU 5 extraction well W-1310 was installed next to well W-1309 and replaces well W-1114.

Both W-1114 and B-1305 were pressure grouted and properly sealed. Well construction details are provided in Table A-1 and well closure data are presented in Table A-2.

Two one-hour drawdown tests were performed on extraction wells W-1309 and W-1310. Results are presented in Appendix B. No other hydraulic tests were conducted in the TF406 area during 1997.

5.8. Vapor Treatment Facility 518

VTF518 is located in the southeastern quadrant of the Livermore Site, north of East Avenue and near Avenue H (Fig. 1). Soil vapor is extracted at VTF518 from the vadose zone using a vapor extraction system. VOCs are removed from the vapor at VTF518 using GAC canisters. The treated effluent air from the air stripper is discharged to the atmosphere. VTF518 was in compliance with the Bay Area Air Quality Management District permit throughout 1997.

VTF518 was activated in September 1995 by treating soil vapor from extraction well SVI-518-201. An additional vapor extraction well, SVI-518-303 was added in March 1997. The VTF518 facility was operated at flow rates ranging from 20 to 50 standard cubic feet per minute in 1997.

5.8.1. Performance Summary

During 1997, VTF518 processed about 4,330,000 cubic feet (ft^3) of soil vapor, removing an estimated 40.6 kg of VOCs (Table 2). Since VTF518 began operating in September 1995, about 106.9 kg of VOC mass has been removed from approximately 6,187,000 ft³ of soil vapor (Table 3).

5.8.2. Field Activities

Two FLUTe instrumented/sampling wells, SEA-518-301 and SEA-518-304, continue to be used to monitor vadose zone remediation in the VTF518 area. The FLUTe system is used to collect vapor, pressure, soil temperature, soil moisture, and soil vapor concentration data from various discrete depths. VOC vapor concentrations at SEA-518-301, the FLUTe system borehole nearest VTF518 vapor extraction well SVI-518-201, have declined from an average of 111 parts per million by volume (ppmv) in September 1995 to an average of 34 ppmv in December 1997.

5.8.3. Soil Vapor Extraction Treatability

A treatability test was conducted at VTF518 to evaluate the impact of extracting simultaneously from vapor extraction well SVI-518-201 and proposed vapor extraction well SVI-518-303. The test indicated that higher influent concentrations resulted when pumping from both wells. Accordingly, soil vapor is now being extracted from both wells.

5.9. Ground Water Treatment Facility 518

TF518 is located in the southeastern quadrant of the Livermore Site, north of East Avenue and near Avenue H, adjacent to VTF518 (Fig. 1). TF518 was constructed in 1997 and is scheduled to begin operating by its RAIP milestone date of January 30, 1998.

TF518 will process ground water for VOC treatment using an air stripper, and the effluent air will be treated using GAC to remove VOCs prior to discharge to the atmosphere. All treated ground water will be discharged to a storm drain located about 250 ft north of TF518 that ultimately empties into Arroyo Las Positas.

TF518 will process ground water from HSU 5 extraction well W-112 and HSU 6 extraction well W-211. Well W-112 will provide hydraulic control of VOC source areas in HSU 5. Well W-211 will serve as an HSU 6 extraction well since TCE concentrations in well W-211 exceeded 5 ppb on one sampling event (5.9 ppb, September 1997). Cumulative flow from the two wells is projected to be about 25 gpm.

No ground water wells were drilled or completed in the TF518 area in 1997.

A 72-hr drawdown test was conducted on proposed TF518 extraction well W-211 to evaluate VOC concentrations in HSU 6 and the integrity of the well's annular seal. While not definitive, the test results suggest that TCE at well W-211 may be the result of a leaky annular seal. Results of this test are provided in Appendix B.

5.10. Treatment Facility 5475

The TF5475 area is located in the southeastern quadrant of the Livermore Site (Fig. 1). The operation of TF5475 will start by September 30, 1998.

5.10.1. Field Activities

One dual-screened well, W-1302, was installed in the TF5475 area during 1997. Well W-1302 is a test well designed to use the down-hole in-situ treatment technology catalytic reductive dehalogenation (CRD). Well W-1302 is intended to be the first TF5475 extraction well scheduled to begin full operation in September 1998. Well construction details are provided in Table A-1 of Appendix A.

In 1997, a one-hour drawdown test was conducted in the T5475 area on well W-1225. A series of step-drawdown tests were also conducted on well W-1302. Results are presented in Appendix B. No other hydraulic tests were conducted in the TF5475 area during 1997.

5.10.2. Ground Water Treatability Test

In 1997, pilot testing began at well W-1302 for the down-hole in-situ CRD technology for the treatment of VOCs in ground water. This technology is based upon the reaction of dissolved hydrogen with VOCs on a palladium-alumina catalyst to form ethane and chloride. Hydrogen is provided by electrolysis of water under an applied voltage potential or compressed hydrogen gas. The treatment takes place during one pass through the treatment unit because of the high reaction rates of CRD, allowing the treatment unit to be placed in the well casing. Because well W-1302

is a dual-screened well, the unit extracts from one screened interval and injects treated water into the other. In August 1997, a program of short- and long-term testing was initiated to assess the following issues:

- Scale-up of the treatment technology from bench-top experiments to the higher flow rates encountered in field implementation.
- Optimization of operating parameters (e.g., flow rate vs. applied voltage).
- Evaluation of long-term performance.

Results from these initial tests indicate that the VOC removal efficiency is generally greater than 95%. The high total VOC influent concentrations (about 4,000 to 5,000 ppb) at well W-1302 resulted in high mass removal rates per unit volume of ground water treated. Some tests have shown that the electrolyzer is converting a portion of the chloroform found in the ground water into a maximum of 1.9 ppb chloroethane, 19 ppb chloromethane, and 21 ppb methylene chloride. This may exclude the use of the electrolyzer in the presence of chloroform. Scaling issues are still being evaluated. The unit is designed for a treatment capacity of approximately 3 gpm; however, the local hydrogeologic conditions at well W-1302 constrain the actual rates used during the test to between 1 to 2 gpm.

During the pilot tests, about 5,289 gal of ground water was treated, and an estimated 0.08 kg of VOCs were removed (Table 2).

6. Trends in Ground Water Analytical Results

Notable results of VOC analyses of ground water received from January 1997 through December 1997 are discussed below. Figures 10 through 14 show isoconcentration contours for total VOCs underlying the Livermore Site and vicinity within HSU 1B, HSU 2, HSU 3A, HSU4, and HSU 5, respectively.

- 1. The TCE concentration in well W-011 has decreased. Well W-011 is located in the eastern portion of the Sandia National Laboratory Site about 500 ft south of East Avenue, and is screened from 136 to 141 ft bgs in HSU 5. In April 1983, <5 ppb of TCE was reported in the initial analysis. Since that time, the TCE increased to a high of 160 ppb in October of 1991, but has decreased to 9.6 ppb as of July 1997.
- 2. The PCE concentration in well W-602 has gradually decreased. Well W-602 is located in the southwest corner of the Livermore Site, near the intersection of East Avenue and Vasco Road, and is screened from 90 to 100 ft bgs in HSU 1B. In November 1989, 430 ppb PCE was reported in the initial analysis. Since that time, the PCE has gradually decreased to 19 ppb as of May 1997.
- 3. The TCE concentration in well W-903 has decreased. Well W-903 is located approximately 300 ft west of the Livermore Site near the corner of Vasco Road and East Avenue, and is screened from 132 to 140 ft in HSU 2. In February 1995, 130 ppb TCE was reported in the initial analysis. Since that time, the TCE concentration has gradually decreased to 41 ppb as of May 1997.

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Figures

1997 Annual Report

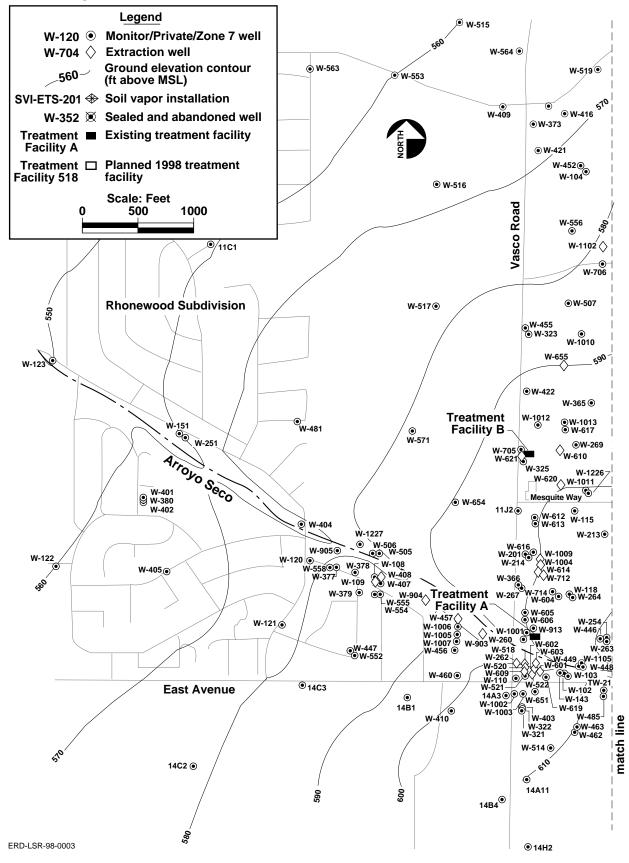


Figure 1. Locations of Livermore Site monitor wells, extraction wells and treatment facilities, December 1997.

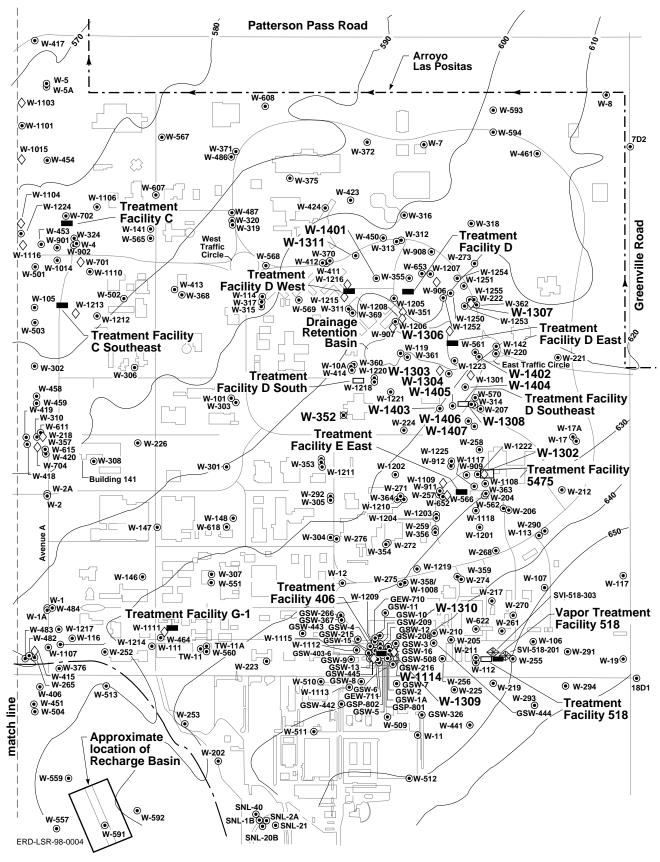


Figure 1 (continued).

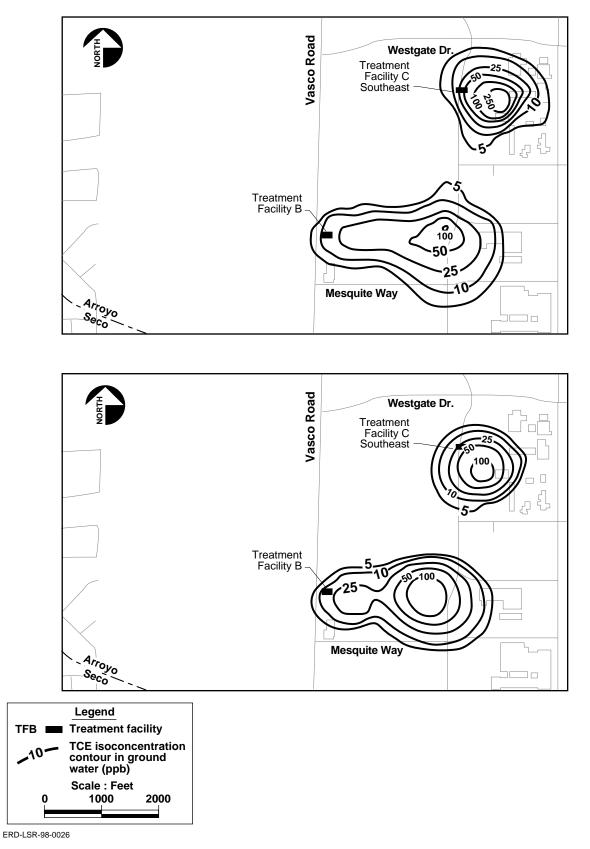


Figure 2. Comparison of measured (top) and simulated (bottom) aqueous TCE concentrations in HSU 1B for 1996.

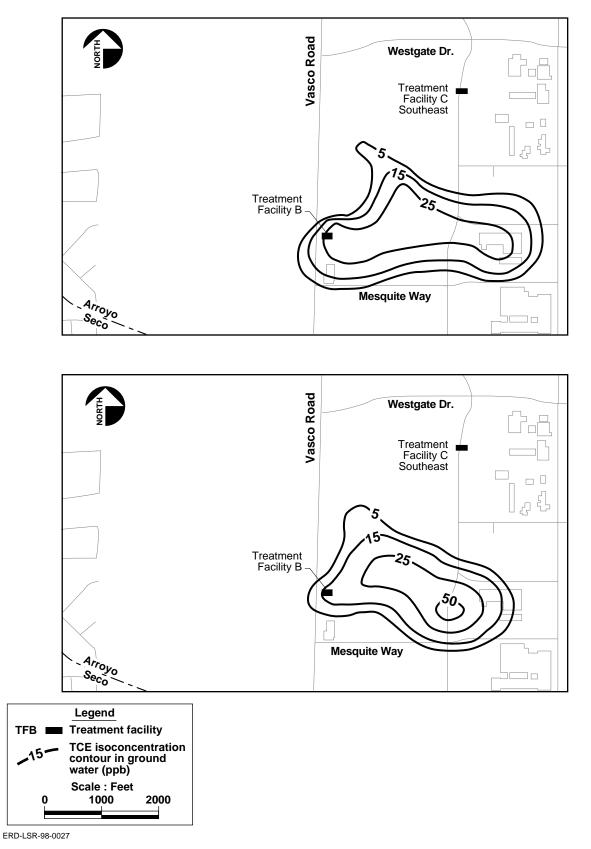


Figure 3. Comparison of measured (top) and simulated (bottom) aqueous TCE concentrations in HSU 2 for 1996.

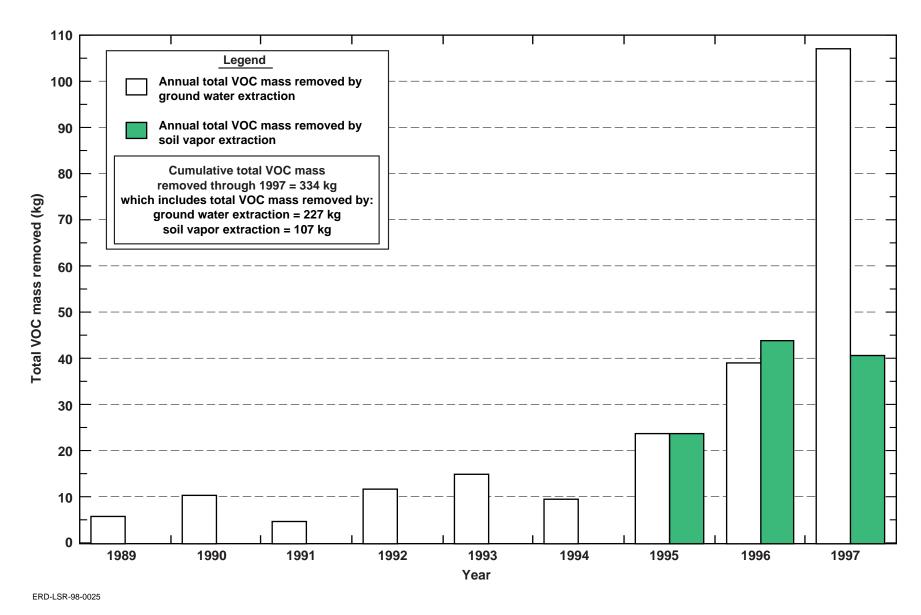


Figure 4. Total VOC mass removed from the Livermore Site subsurface.

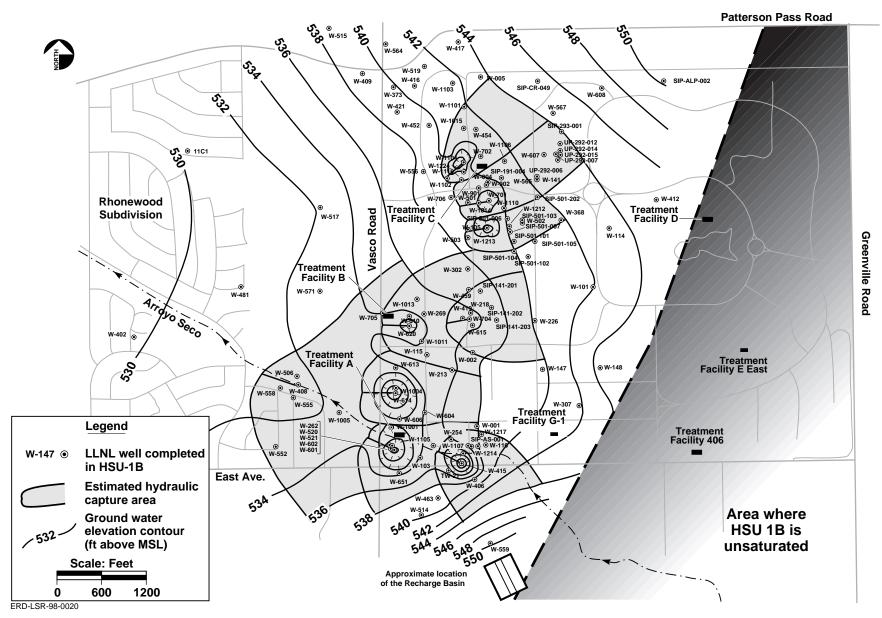


Figure 5. Ground water elevation contour map based on water levels collected from 126 wells completed within HSU 1B showing estimated hydraulic capture areas, LLNL and vicinity, December 1997.

1997 Annual Report

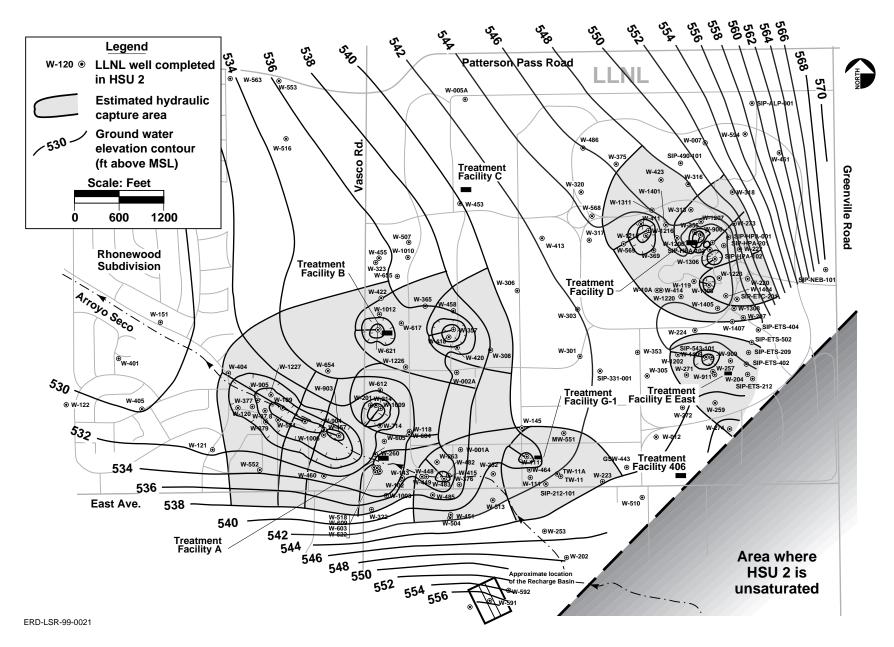
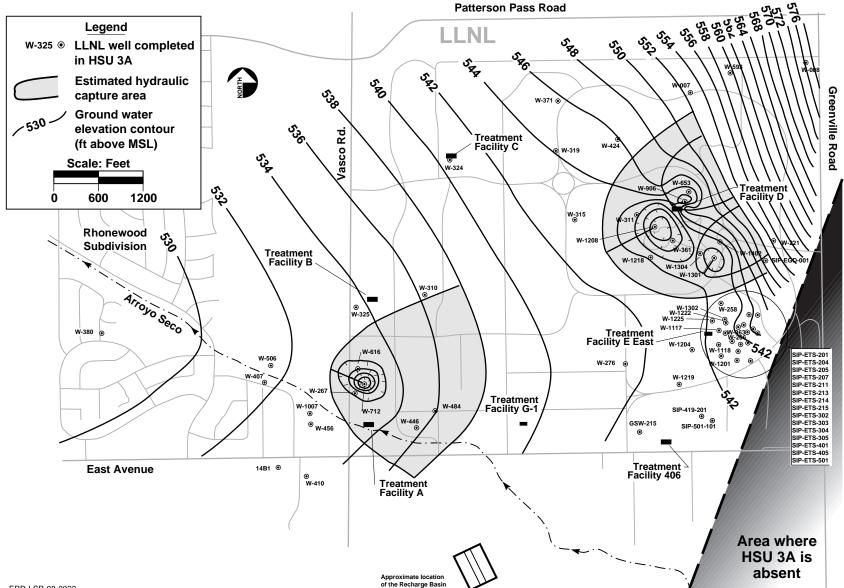


Figure 6. Ground water elevation contour map based on water levels collected from 152 wells completed within HSU 2 showing estimated hydraulic capture areas, LLNL and vicinity, December 1997.



ERD-LSR-98-0022

Figure 7. Ground water elevation contour map based on water levels collected from 60 wells completed within HSU 3A showing estimated hydraulic capture areas, LLNL and vicinity, December 1997.

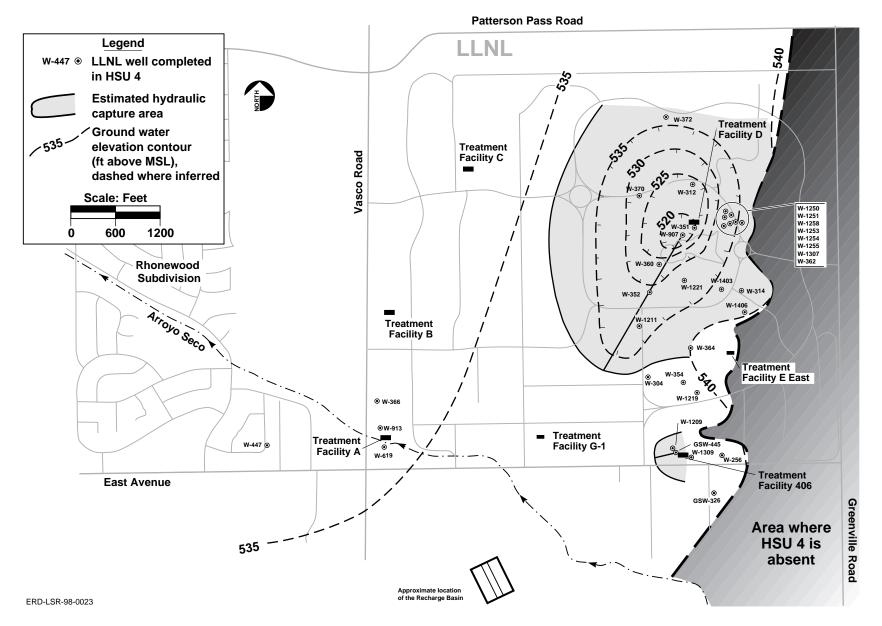
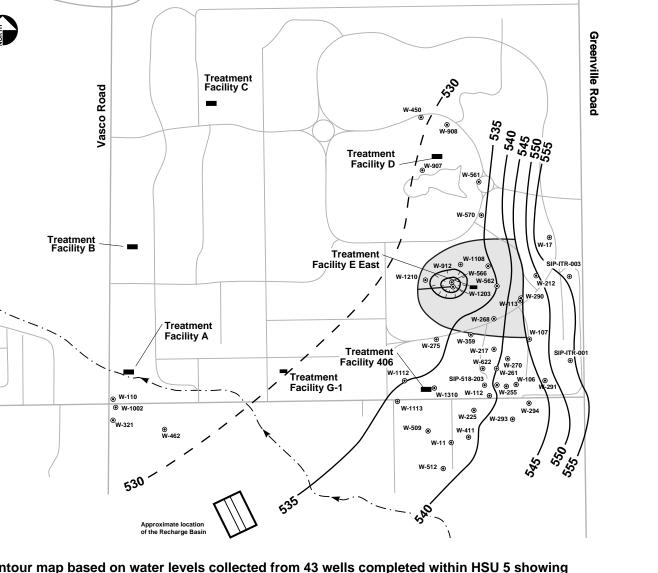


Figure 8. Ground water elevation contour map based on water levels collected from 23 wells completed within HSU 4 showing estimated hydraulic capture areas, LLNL and vicinity, December 1997.



Patterson Pass Road

LLNL

ERD-LSR-98-0024

Legend

W-462 ● LLNL well completed in HSU 5

capture area Ground water

- 530

0

Estimated hydraulic

elevation contour

dashed where inferred

1200

Arroyo Seco

Rhonewood Subdivision

East Avenue

(ft above MSL),

Scale: Feet

600

Figure 9. Ground water elevation contour map based on water levels collected from 43 wells completed within HSU 5 showing estimated hydraulic capture areas, LLNL and vicinity, December 1997.

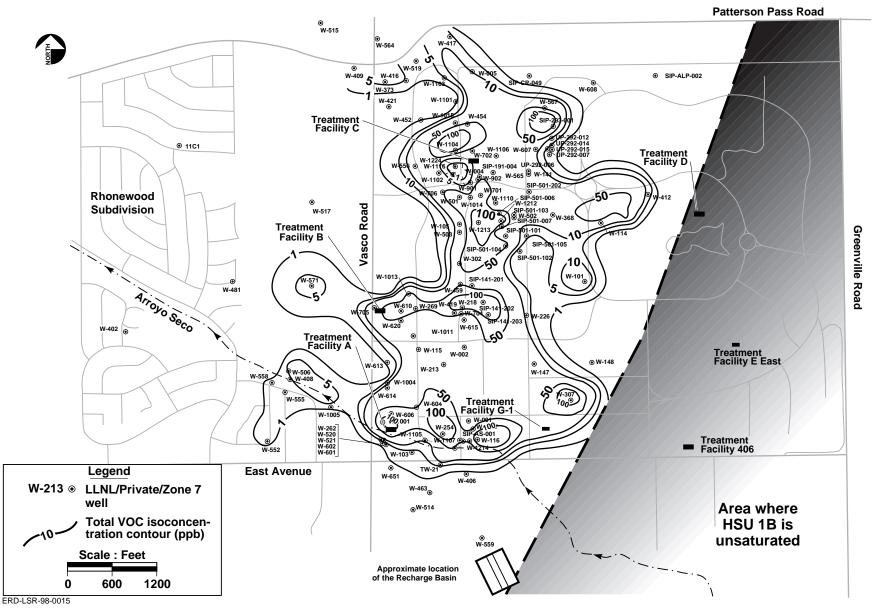
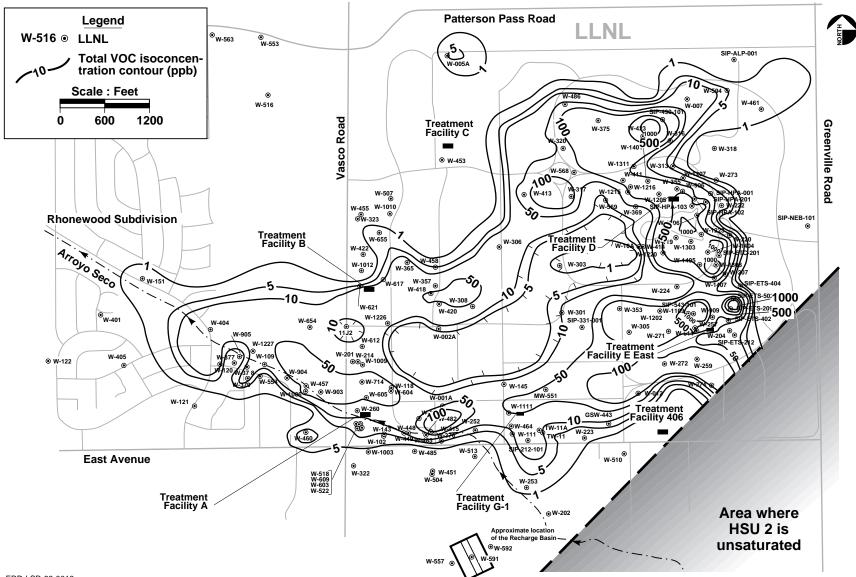
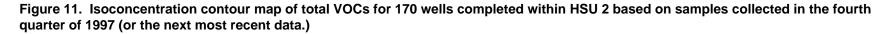


Figure 10. Isoconcentration contour map of total VOCs for 128 wells completed within HSU 1B based on samples collected in the fourth quarter of 1997 (or the next most recent data.)





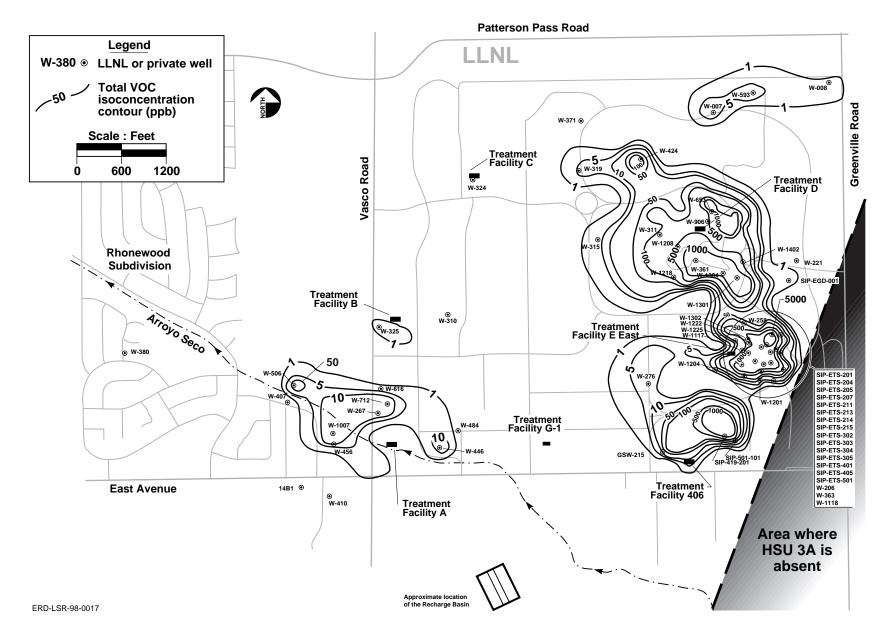


Figure 12. Isoconcentration contour map of total VOCs for 71 wells completed within HSU 3A based on samples collected in the fourth quarter of 1997 (or the next most recent data.)

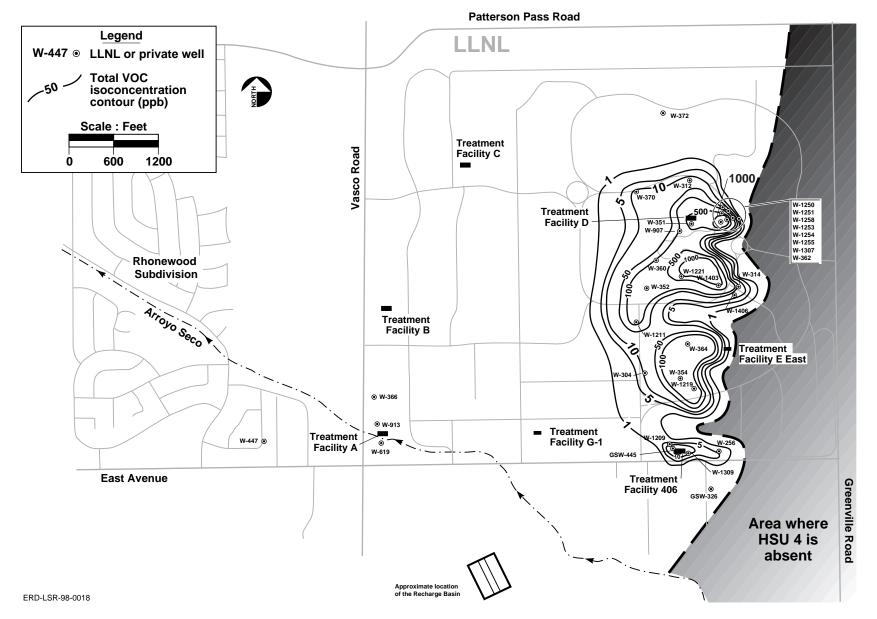
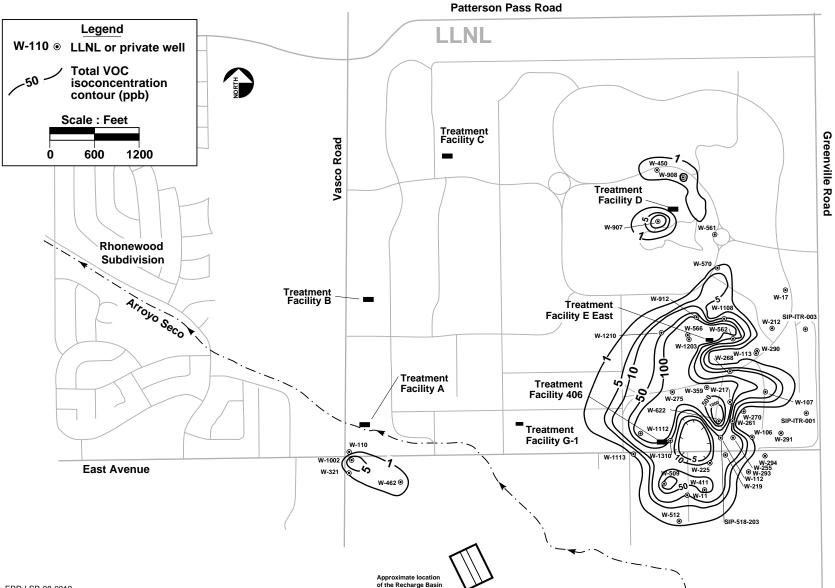


Figure 13. Isoconcentration contour map of total VOCs for 37 wells completed within HSU 4 based on samples collected in the fourth quarter of 1997 (or the next most recent data.)



ERD-LSR-98-0019

Figure 14. Isoconcentration contour map of total VOCs for 45 wells completed within HSU 5 based on samples collected in the fourth quarter of 1997 (or the next most recent data.)

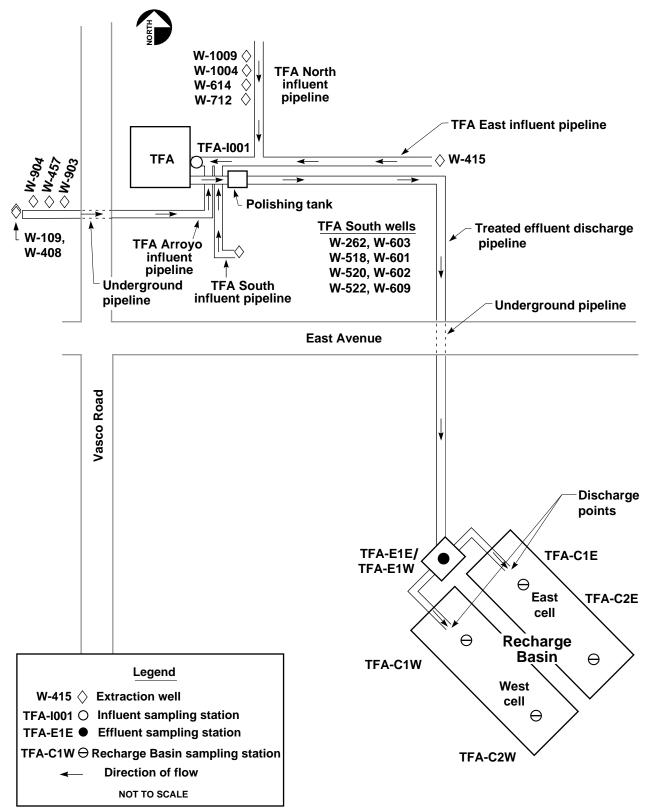
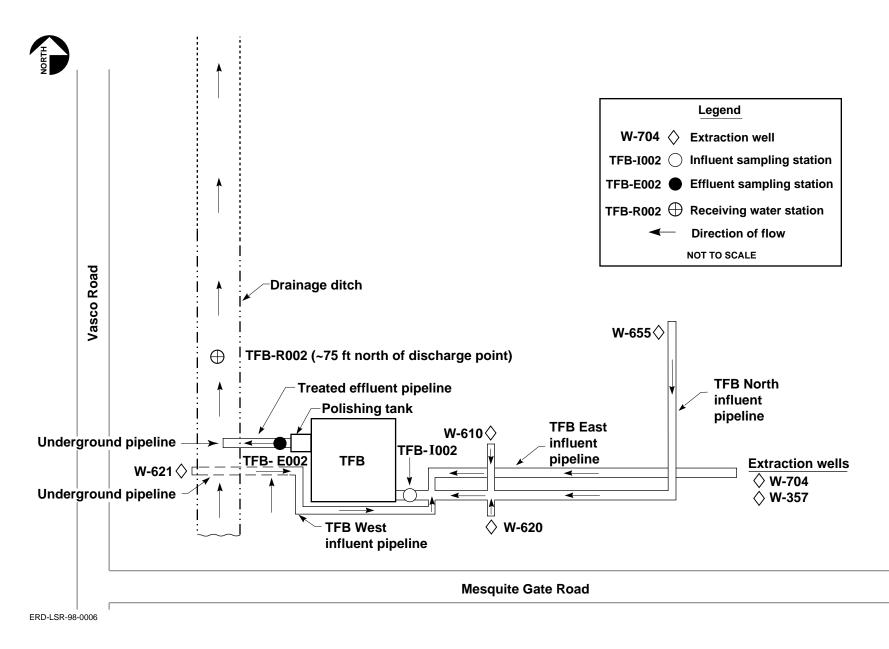
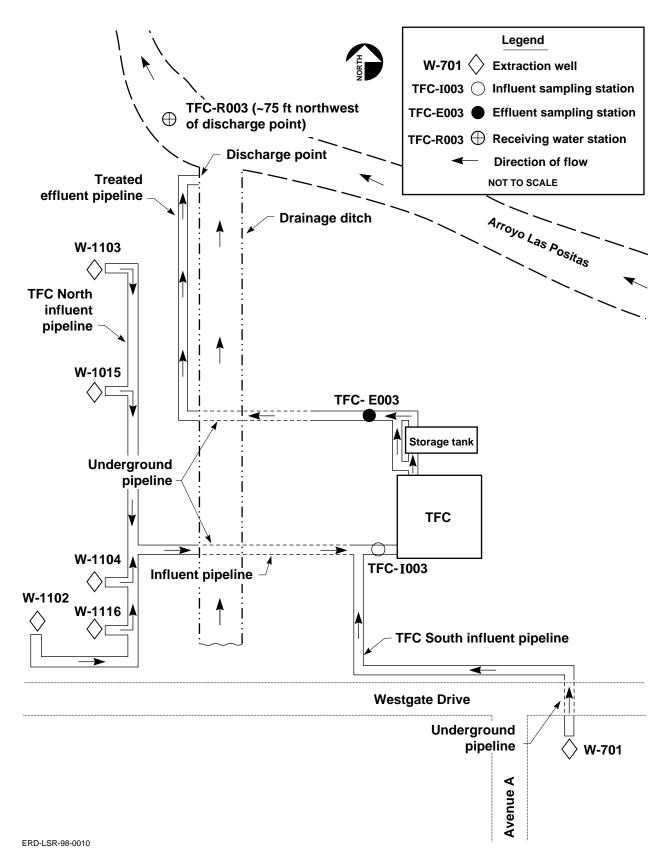


Figure 15. 1997 TFA extraction wells, pipelines and discharge location.









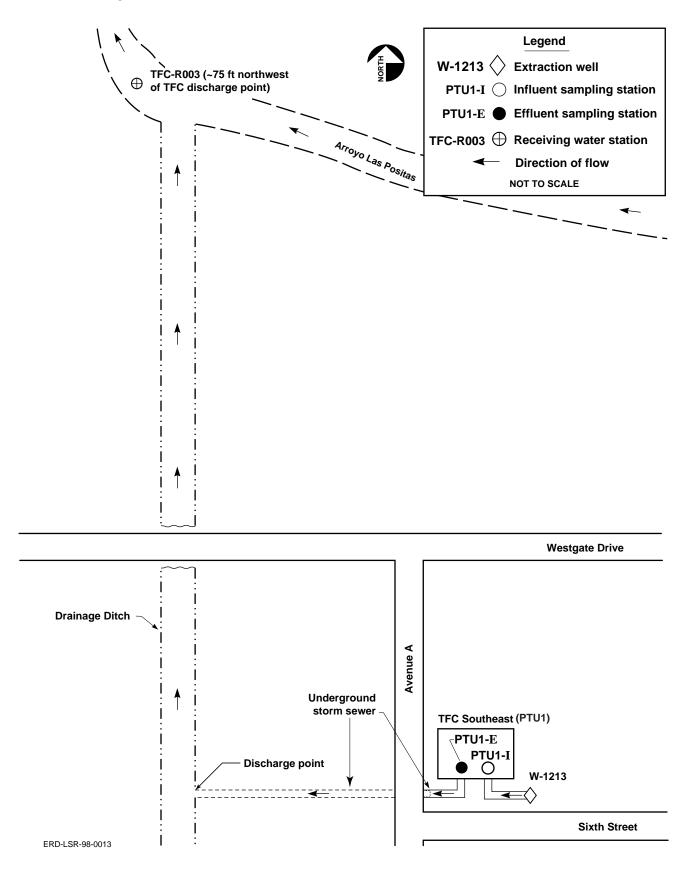
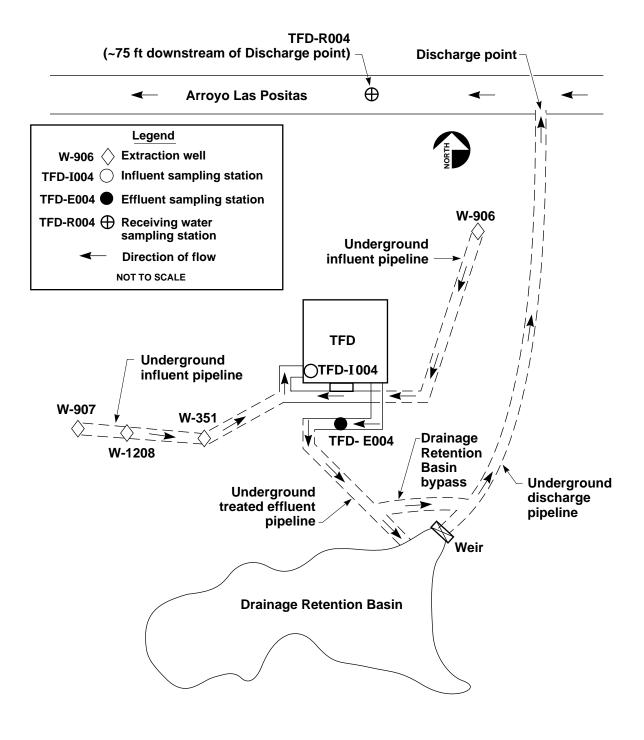


Figure 18. 1997 TFC Southeast extraction wells, pipelines and discharge location.





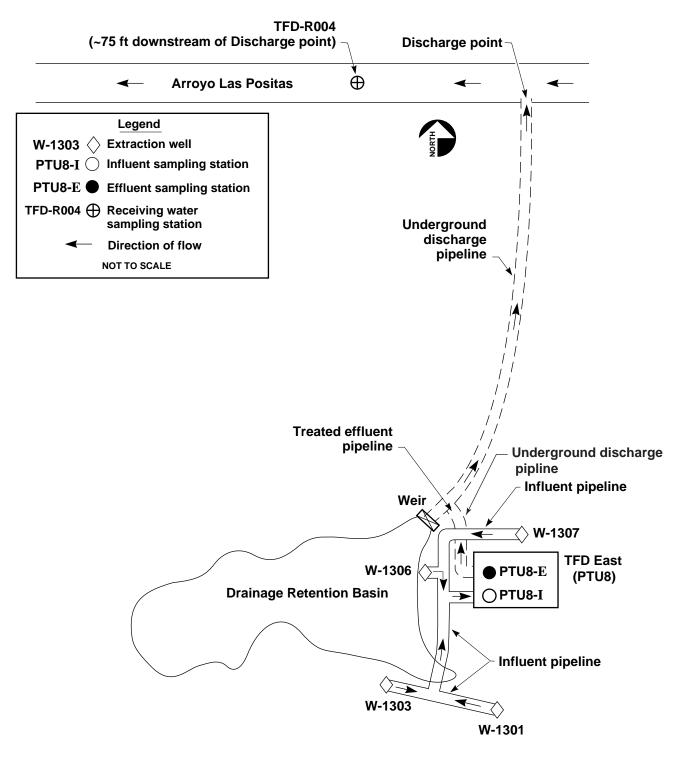


Figure 20. 1997 TFD East extraction wells, pipelines and discharge location.

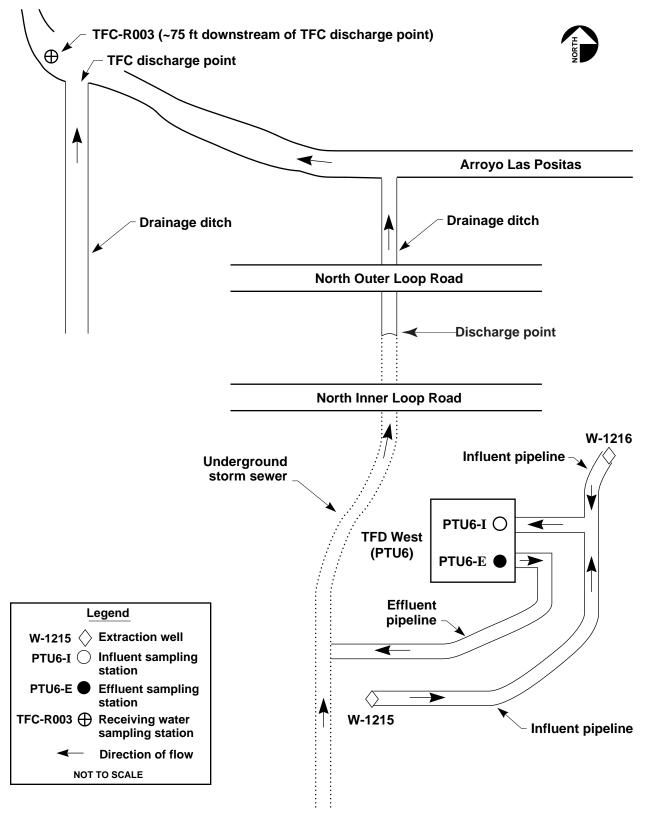


Figure 21. 1997 TFD West extraction wells, pipelines and discharge location.

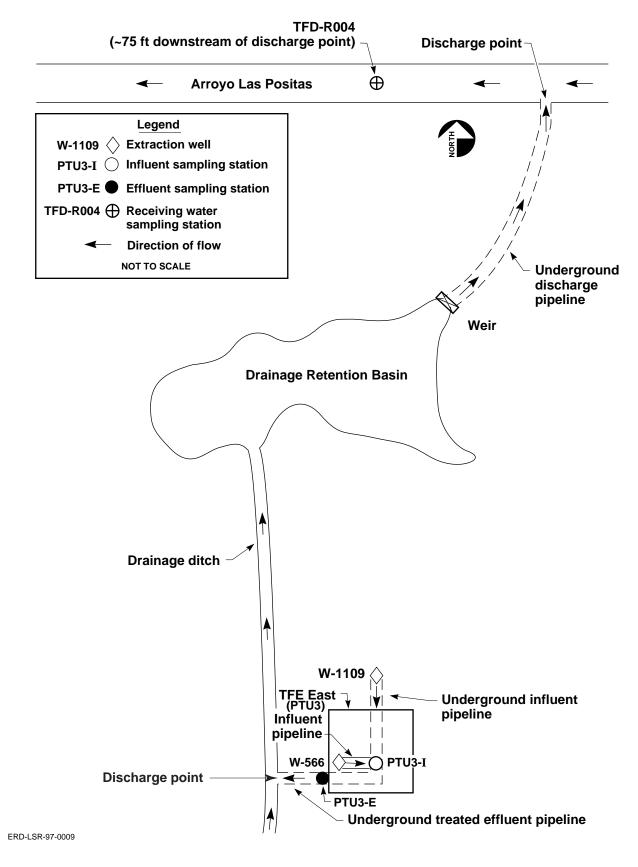


Figure 22. 1997 TFE East extraction wells, pipelines and discharge location.

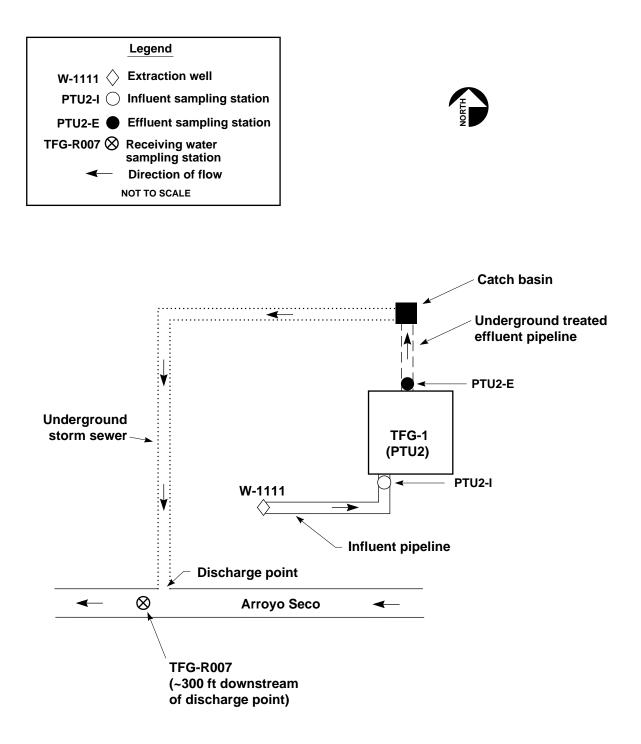


Figure 23. 1997 TFG-1 extraction well, pipelines and discharge location.

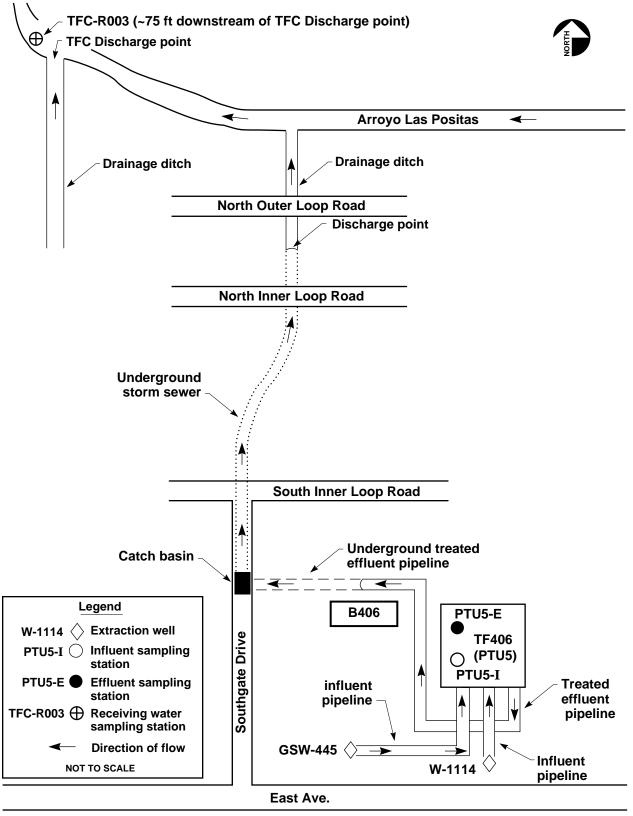


Figure 24. 1997 TF406 extraction wells, pipelines and discharge location.

Tables

Milestone	Milestone date	Completion date
Begin operation of TFC southeast PTU	01/31/97	01/21/97
Begin operation of TFD West PTU	04/25/97	04/22/97
Five-Year Review	08/05/97	08/01/97
Submit Draft RD4 to the regulatory agencies and the community	08/25/97	08/21/97
Begin operation of TFD East PTU	10/03/97	09/16/97
Receive regulatory comments on Draft RD4	11/04/97	11/03/97

 Table 1. 1997 Livermore Site Remedial Action Implementation Plan milestones.

Table 2. Summary of 1997 Livermore Site VOC remediation.

Treatment facility	Volume of ground water treated (Mgal)	Volume of soil vapor treated (Kft ³)	Estimated total VOC mass removed (kg) ^a
TFA	128.1	-	18.4
TFB	16.9	-	6.8
TFC	22.7	-	9.4
TFD	48.1	-	55.0
TFE	9.5	-	15.9
TFG	3.3	-	0.6
TF406	2.3	-	0.9
VTF518	-	4,330	40.6
TF5475	5.3 Kgal	-	0.1
Total	230.9	4,330	147.7

Notes:

kg = Kilograms.

Kft³ = Thousands of cubic feet.

Kgal = Thousands of gallons.

Mgal = Millions of gallons.

^a Masses are calculated using monthly flow volumes and total VOC concentrations.

Treatment facility	Volume of ground water treated (Mgal)	Volume of soil vapor treated (Kft ³)	Estimated total VOC mass removed (kg) ^a
TFA	391.0	((((()	94.3
ІГА	391.0	—	94.3
TFB	65.3	-	25.5
TFC	35.6	-	15.4
TFD	60.5	-	73.4
TFE	9.9	-	17.1
TFG	4.3	-	0.8
TF406	2.7	_	1.1
VTF518	_	6,187	106.9
TF5475	5.3 Kgal	-	0.1
Total	569.3	6,187	334.6

Table 3. Summary of cumulative Livermore Site VOC remediation.

Notes:

kg = Kilograms.

Kft³ = Thousands of cubic feet.

Mgal = Millions of gallons.

^a Masses are calculated using monthly flow volumes and total VOC concentrations.

Appendix A

Well Construction and Closure Data

Well number	Date completed	Borehole depth (ft)	Casing depth (ft)	Perforated interval (ft)	HSU ^a monitored	Well development flow rate (gpm) ^b
Monitor Wells						
W-1	21-Oct-80	122.5	116.0	95-100	1B/2	NA
W-1A	12-Apr-84	180.0	156.0	145-156	2	NA
W-2	29-Aug-80	102.5	101.0	86-101	1 B	NA
W-2A	02-Apr-84	185.0	164.0	150-164	2	NA
W-4	28-Jul-80	92.0	90.0	75-90	1 B	NA
W-5	24-Oct-80	93.5	90.0	56-71 81-86	1 B	NA
W-5A	09-Apr-84	115.0	105.0	95-105	2	NA
W-7	03-Oct-80	110.5	100.5	76-81 88-98	2/3A	NA
W-8	14-May-81	110.0	105.0	72-77 92-102	3A/3B	NA
W-10A	08-Sep-80	110.7	110.0	85-95 100-105	2	NA
W-11	03-Jun-81	252.0	191.0	136-141 177-187	5	NA
W-12	14-Aug-80	115.75	115.0	99-114	2	NA
W-17	08-Oct-80	114.0	114.0	94-109	5	NA
W-17A	20-May-81	181.4	160.0	127-132 147-157	7	NA
W-19	19-Sep-80	164.75	161.0	147-157	7	NA
W-101	25-Jan-85	77.0	72.0	62-72	1 B	1
W-102	12-Feb-85	396.5	171.5	151.5-171.5	2	40
W-103	14-Feb-85	96.0	89.5	79.5-89.5	1 B	5
W-104	21-Feb-85	61.5	56.5	38.75-56.5	1 B	2.5
W-105	26-Feb-85	69.0	62.0	42-62	1 B	0.7
W-106	06-Mar-85	144.0	134.5	127.5-134.5	5	0.1-0.2
W-107	13-Mar-85	128.0	122.0	115-122	5	1-3
W-108	21-Mar-85	113.5	69.0	57-69	1A	10
W-110	26-Apr-85	371.0	365.0	340-365	5	6
W-111	02-May-85	122.0	117.0	97-117	2	1.5
W-112	10-May-85	129.0	123.5	111-123.5	5	4
W-113	16-May-85	124.0	115.0	100-115	5	0.9

Table A-1. Well construction data, Lawrence Livermore National Laboratory and vicinity, Livermore, California.

Well number	Date completed	Borehole depth (ft)	Casing depth (ft)	Perforated interval (ft)	HSU ^a monitored	Well development flow rate (gpm) ^b
W-114	23-May-85	70.5	63.0	51-63	1 B	0.5
W-115	03-Jun-85	106.0	95.0	88-95	1 B	1.1
W-116	14-Jun-85	181.0	91.0	86-91	1 B	0.3
W-117	27-Jun-85	202.0	148.0	138-148	7	0.2
W-118	19-Jul-85	206.5	110.0	99-110	2	8
W-119	02-Aug-85	139.0	102.5	87.5-102.5	2	3.3
W-120	19-Aug-85	195.0	153.0	147-153	2	1
W-121	23-Aug-85	194.0	171.0	159-171	2	3.75
W-122	17-Aug-85	189.0	132.0	125-132	2	15
W-123	01-Oct-85	174.0	47.7	37.3-47.7	1A	5
W-141	23-Mar-85	61.5	60.0	45-60	1 B	0.8
W-142	29-Mar-85	74.2	72.0	62-72	2	0.8
W-143	12-Apr-85	130.0	126.0	121-126	2	0.8
W-146	16-Jul-85	225.0	125.0	115-125	2	5
W-147	26-Jul-85	137.0	87.0	77-87	1 B	0.5
W-148	08-Aug-85	152.0	98.0	83-98	1 B	0.5
W-151	30-Sep-85	237.0	157.5	148.5-157.5	2	1.5
W-201	17-Oct-85	211.0	161.0	151-161	2	14
W-202	07-Nov-85	191.0	109.0	99-109	2	0.5
W-203	15-Nov-85	87.0	41.0	31-41	1A	3
W-204	22-Nov-85	110.0	110.0	100-110	2	5+
W-205	09-Dec-85	180.0	117.0	107-117	3 B	<0.1
W-206	19-Dec-85	188.0	118.0	106-118	3A	<0.5
W-207	24-Jan-86	150.0	85.0	69-85	2	<0.5
W-210	11-Mar-86	176.0	113.0	108-113	3B	<0.5
W-211	19-Mar-86	215.5	193.0	183-193	7	1
W-212	28-Mar-86	183.0	136.0	124-136	5	1
W-213	04-Apr-86	174.0	100.0	94-100	1 B	2
W-214	11-Apr-86	146.0	141.5	134-141.5	2	20+
W-217	20-May-86	200.0	112.5	98.5-112.5	5	<0.5
W-218	30-May-86	201.0	71.0	64.5-71	1 B	6
W-219	13-Jun-86	214.0	148.0	141-148	5	2
W-220	25-Jun-86	196.0	92.5	82.5-92.5	2	<0.5
W-221	07-Jul-86	178.0	95.0	82-95	3A	2
W-222	17-Jul-86	197.0	83.0	63-83	2	5

Well number	Date completed	Borehole depth (ft)	Casing depth (ft)	Perforated interval (ft)	HSU ^a monitored	Well development flow rate (gpm) ^b
W-223	15-Aug-86	202.0	153.0	146-153	2	5.2
W-224	26-Aug-86	199.0	88.0	78-88	2	3
W-225	09-Sep-86	238.0	166.0	152-166	5	2.5
W-226	25-Sep-86	173.0	86.0	71-86	1 B	<0.25
W-251	03-Oct-85	50.0	47.5	35.5-47.5	1 A	2
W-252	18-Oct-85	197.0	126.0	108-126	2	3
W-253	30-Oct-85	180.0	128.0	112.5-128	2	1
W-254	21-Nov-85	277.0	91.5	84.5-91.5	1 B	5
W-255	05-Dec-85	187.0	124.0	115-124	5	1
W-256	19-Dec-85	187.0	137.0	132-137	4	<0.5
W-257	15-Jan-86	197.0	96.5	82.5-96.5	2	<0.5
W-258	31-Jan-86	157.0	121.5	116.5-121.5	3 A	0.5
W-259	07-Feb-86	200.0	99.0	93.5-99	2	<0.5
W-260	27-Feb-86	215.0	151.0	141-151	2	3.5
W-261	12-Mar-86	225.0	118.5	109-118.5	5	<0.5
W-263	07-Apr-86	146.0	130.0	123-130	2	2
W-264	14-Apr-86	170.0	151.0	141-151	2	20+
W-265	25-Apr-86	216.0	211.0	205-211	3A	3
W-267	27-May-86	196.0	179.0	172.5-179	3A	1
W-268	04-Jun-86	213.0	150.5	138-150.5	5	1
W-269	16-Jun-86	185.0	92.0	79-92	1 B	2
W-270	26-Jun-86	185.0	127.0	113-127	5	<0.5
W-271	07-Jul-86	201.0	112.0	105-112	2	2.1
W-272	18-Jul-86	226.0	110.0	95-110	2	1
W-273	11-Aug-86	203.0	84.0	64-84	2	3
W-274	21-Aug-86	217.0	95.0	90-95	2	<0.5
W-275	05-Sep-86	262.0	184.0	179-184	5	4
W-276	17-Sep-86	267.0	170.0	153.5-169.5	3A/3B	12
W-277	03-Oct-86	254.0	169.0	163-169	3 B	1.1
W-290	08-Jul-86	181.0	126.0	119.5-126	5	<0.5
W-291	24-Jul-86	194.0	137.0	127-137	5	<0.5
W-292	14-Aug-86	250.0	184.5	176-184.5	3 B	9
W-293	27-Aug-86	229.0	155.0	145-155	5	<1
W-294	15-Sep-86	251.0	139.0	122-139	5	1
W-301	07-Oct-86	203.0	141.0	136-141	2	5.5

Well number	Date completed	Borehole depth (ft)	Casing depth (ft)	Perforated interval (ft)	HSU ^a monitored	Well development flow rate (gpm) ^b
W-302	22-Oct-86	191.0	83.5	78-83.5	1 B	2
W-303	28-Oct-86	197.0	128.0	124-128	2	15
W-304	12-Nov-86	207.0	200.0	195-200	4	1
W-305	18-Nov-86	146.0	138.0	128-138	2	20
W-306	04-Dec-86	207.0	110.0	98-110	2	8.5
W-307	15-Dec-86	214.0	102.0	93-102	1 B	1
W-308	13-Jan-87	194.0	113.0	107-113	2	2
W-309	20-Jan-87	73.0	NA	NA	NA	NA
W-310	04-Feb-87	202.0	184.5	176.5-184.5	3 A	10
W-311	20-Feb-87	226.5	147.5	134.5-147.5	3 A	5
W-312	05-Mar-87	224.5	168.0	160-168	4	25
W-313	12-Mar-87	99.0	85.0	80-85	2	5.5
W-314	20-Mar-87	228.0	142.0	129-142	4	9.5
W-315	03-Apr-87	215.0	156.0	141-156	3A	15
W-316	15-Apr-87	196.0	71.0	66-72	2	3
W-317	20-Apr-87	100.0	95.0	88-95	2	7
W-318	28-Apr-87	200.0	81.0	74-81	2	0.5
W-319	05-May-87	198.0	125.0	119-125	3 A	25
W-320	11-May-87	106.0	99.0	94-99	2	3
W-321	29-May-87	356.0	321.5	305-321.5	5	60
W-322	01-Jul-87	565.5	152.0	142-152	2	4
W-323	04-Aug-87	200.0	127.0	122-127	2	7
W-324	17-Aug-87	219.0	189.0	184-189	3A	15
W-325	28-Aug-87	312.0	170.0	158-170	3 A	4
W-353	12-Nov-86	205.0	101.0	95.5-101	2	1
W-354	24-Nov-86	185.0	179.0	163-179	4/5	8
W-355	05-Dec-86	202.0	107.0	102-107	2	2
W-356	18-Dec-86	237.0	137.0	133-137	3 B	6
W-359	10-Feb-87	195.0	150.5	138-150.5	5	10
W-360	24-Feb-87	260.0	204.5	181.5-204.5	4	30
W-361	05-Mar-87	257.0	135.0	125-135	3A	4
W-362	13-Mar-87	151.0	145.0	131-145	4	12
W-363	24-Mar-87	195.0	129.0	117-129	3A	<0.5
W-364	31-Mar-87	195.0	165.0	155-165	3B/4	5
W-365	09-Apr-87	187.0	125.0	120-125	2	8.5
W-366	20-Apr-87	273.0	251.0	240-251	4	13

Well number	Date completed	Borehole depth (ft)	Casing depth (ft)	Perforated interval (ft)	HSU ^a monitored	Well development flow rate (gpm) ^b
W-368	06-May-87	206.0	78.0	70-78	1 B	3
W-369	14-May-87	204.0	113.0	107-113	2	2
W-370	29-May-87	286.0	208.0	196.5-208	4	5
W-371	12-Jun-87	233.0	162.0	155-162	3 A	1.5
W-372	25-Jun-87	218.0	152.5	147.5-152.5	4	1
W-373	06-Jul-87	178.0	99.0	89-99	1 B	7
W-375	29-Jul-87	223.0	71.0	65-71	2	0.75
W-376	27-Aug-87	249.0	172.0	162-172	2	2
W-377	04-Sep-87	159.0	144.0	141.5-144	2	2.5
W-378	09-Sep-87	155.0	150.0	146-150	2	5
W-379	14-Sep-87	155.0	150.0	146-150	2	5
W-380	01-Oct-87	195.0	182.0	170-182	3A	10
W-401	05-Nov-87	159.0	153.0	109-153	2	25
W-402	13-Oct-87	104.0	102.0	92-102	1 B	40
W-403	16-Nov-87	585.0	495.0	485-495	7	3
W-404	04-Dec-87	245.0	158.0	150-158	2	33
W-405	04-Jan-88	244.0	162.0	132-162	2	50
W-406	20-Jan-88	213.0	94.0	79-84	1 B	2
W-407	04-Feb-88	215.0	205.0	192-205	3 A	4
W-409	07-Mar-88	272.0	78.0	71-78	1 B	30
W-410	30-Mar-88	369.0	205.0	193-205	3 A	35
W-411	12-Apr-88	192.0	138.0	131-138	2	8
W-412	18-Apr-88	104.0	74.0	67-74	1 B	2.5
W-413	28-Apr-88	163.0	115.0	100-115	2	25
W-414	20-May-88	179.0	74.0	69.5-74	2	0.5
W-416	10-Jun-88	152.0	80.5	72-80.5	1 B	30
W-417	20-Jun-88	152.0	60.0	51-60	1 B	5
W-418	24-Jun-88	124.0	118.0	108-118	2	2.5
W-419	29-Jun-88	82.0	75.5	62.5-75.5	1 B	3
W-420	26-Jul-88	127.0	111.0	105-111	2	5
W-421	23-Aug-88	181.0	90.0	75-90	1 B	4.5
W-422	02-Sep-88	203.0	139.5	133-139.5	2	5
W-423	09-Sep-88	308.0	118.0	106-118	2	14
W-424	04-Oct-88	208.0	144.0	137-144	3A	3
W-441	14-Oct-87	250.0	144.0	135-144	5	2.5

Well number	Date completed	Borehole depth (ft)	Casing depth (ft)	Perforated interval (ft)	HSU ^a monitored	Well development flow rate (gpm) ^b
W-446	18-Dec-87	202.0	196.0	186-196	3A	3
W-447	05-Feb-88	353.0	274.0	256-274	4	5
W-448	17-Feb-88	235.0	127.5	120.5-127.5	2	15
W-449	07-Mar-88	172.0	165.0	152-165	2	3
W-450	21-Mar-88	300.0	200.0	193-200	5	2
W-451	06-Apr-88	202.0	112.0	106-112	2	1.5
W-452	15-Apr-88	210.0	79.5	64-79.5	1 B	5
W-453	27-Apr-88	185.0	130.3	121-130	2	4
W-454	09-May-88	196.0	83.5	73-83.5	1 B	3
W-455	19-May-88	184.0	162.5	148-162.5	2	5
W-456	09-Jun-88	343.0	180.5	172-180.5	3 A	2
W-458	30-Jun-88	212.5	116.0	108-116	2	2
W-459	20-Jul-88	76.0	73.0	59.5-73	1 B	1.5
W-460	22-Jul-88	361.0	140.5	135-140.5	2	30
W-461	16-Aug-88	133.0	51.5	41.5-51.5	2	<0.5
W-462	12-Sep-88	385.0	336.5	331-336.5	5	5
W-463	16-Sep-88	93.0	92.5	87-92.5	1 B	5
W-464	30-Sep-88	253.0	104.5	96-104.5	2	3.5
W-481	04-Nov-88	224.5	105.0	100-105	1 B	2
W-482	15-Jan-88	218.0	170.0	165-170	2	<0.5
W-483	26-Jan-88	140.0	130.0	115-130	2	2.5
W-484	11-Feb-88	255.0	188.0	185-188	3 A	0.5
W-485	25-Feb-88	249.0	157.0	151-157	2	2
W-486	11-Mar-88	167.0	108.0	100-108	2	2
W-487	17-Mar-88	180.0	151.0	148-151	3 B	1
W-501	13-Oct-88	174.0	92.0	84-92	1 B	6.5
W-502	25-Oct-88	158.0	59.0	55-59	1 B	<0.5
W-503	02-Nov-88	187.0	80.0	74-80	1 B	1
W-504	21-Nov-88	358.0	167.0	157-167	2	3
W-505	15-Dec-88	278.0	180.0	167-180	3A	60
W-506	22-Dec-88	120.0	115.0	101-115	1 B	30
W-507	18-Jan-89	158.0	139.0	129-139	2	50
W-508	17-Feb-89	316.0	305.0	287-305	7	60
W-509	03-Mar-89	305.0	184.0	179-184	5	1
W-510	15-Mar-89	300.0	119.0	111-119	2	<0.5

Well number	Date completed	Borehole depth (ft)	Casing depth (ft)	Perforated interval (ft)	HSU ^a monitored	Well development flow rate (gpm) ^b
W-511	31-Mar-89	316.0	176.0	167-176	3B	1
W-512	13-Apr-89	261.0	176.0	166-176	5	2.5
W-513	26-Apr-89	259.0	115.0	102-115	2	1
W-514	17-May-89	386.0	115.5	92-115.5	1 B	2
W-515	30-May-89	211.0	78.0	68-78	1 B	3.5
W-516	09-Jun-89	203.0	119.0	114-119	2	15
W-517	20-Jun-89	215.0	88.0	80-88	1 B	6.7
W-519	14-Aug-89	186.5	80.5	60-80.5	1 B	25
W-521	13-Sep-89	166.0	95.0	86-95	1 B	1
W-551	18-Oct-88	308.0	155.5	151-155.5	2	20
W-552	25-Oct-88	70.5	64.0	48.5-64	1 B	3
W-553	03-Nov-88	186.0	106.5	99-106.5	2	1
W-554	22-Nov-88	239.0	141.5	126.5-141.4	2	60
W-555	05-Dec-88	122.0	116.5	102.5-116.5	1 B	20
W-556	15-Dec-88	192.0	81.5	76-81.5	1 B	6
W-557	22-Dec-88	122.5	118.0	102-118	2	2
W-558	17-Jan-89	117.0	110.5	101-110.5	1 B	20
W-559	24-Jan-89	105.0	100.0	93-100	1 B	0.75
W-560	07-Feb-89	263.0	206.5	201-206.5	3 B	10
W-561	23-Feb-89	180.0	152.0	143-152	5	4
W-562	08-Mar-89	263.0	158.0	145-158	5	2
W-563	17-Mar-89	192.0	105.0	95-105	2	2
W-564	30-Mar-89	184.0	85.0	79.5-85	1 B	3
W-565	06-Apr-89	177.0	82.5	75-82.5	1 B	15
W-567	27-Apr-89	194.0	61.5	51-61	1 B	10
W-568	05-Jun-89	156.0	101.0	97-101	2	30
W-569	16-May-89	215.0	109.5	101-109.5	2	4
W-570	09-Jun-89	180.0	175.0	161-175	5	1
W-571	15-Jun-89	223.5	207.5	102-107	1 B	22
W-591	29-Nov-88	112.0	107.5	97-107.5	2	<0.5
W-592	12-Dec-88	136.5	113.0	101-113	2	1.5
W-593	06-Feb-89	159.0	92.5	82-92.5	3A	1.5
W-594	27-Feb-89	156.0	61.0	55-61	2	0.5
W-604	27-Nov-89	111.0	83.0	76-82	1B	0.5
W-605	08-Dec-89	246.0	136.0	130-136	2	10

Well number	Date completed	Borehole depth (ft)	Casing depth (ft)	Perforated interval (ft)	HSU ^a monitored	Well development flow rate (gpm) ^b
W-606	21-Dec-89	145.0	89.0	73-89	1 B	2
W-607	24-Jan-90	186.0	55.0	49-55	1 B	3
W-608	07-Feb-90	162.0	66.0	55-66	1 B	3
W-611	04-Apr-90	161.0	98.0	87.5-98	1 B	2
W-612	19-Apr-90	222.0	136.0	126-136	2	10
W-613	02-May-90	93.0	88.0	81.5-88	1 B	7
W-615	01-Jun-90	121.0	99.0	91-99	1 B	3
W-616	14-Jun-90	255.0	188.0	178-188	3 A	8
W-617	26-Jun-90	200.0	110.0	103-110	2	6
W-618	17-Jul-90	357.0	205.0	201-205	3 B	10
W-619	07-Aug-90	330.0	252.0	232-252	3B/4	30
W-622	28-Sep-90	206.0	112.0	104-112	5	<0.5
W-651	22-Feb-90	155.0	89.0	82-89	1 B	0.5
W-652	15-Mar-90	318.0	256.0	245-256	7	2
W-653	29-Mar-90	225.0	128.0	122-128	3 A	0.5
W-654	11-Apr-90	240.0	158.0	140-158	2	20
W-702	24-Oct-90	180.5	95.0	77-95	1 B	10
W-703	03-Dec-90	586.0	325.0	298-325	5	10
W-705	26-Dec-90	126.00	90.0	77-90	1 B	2
W-706	16-Jan-91	178.0	84.0	71-84	1 B	2
W-714	02-Jul-91	135.0	128.0	107-128	2	7.5
W-901	24-Feb-93	97.8	88.0	79-83	1 B	1
W-902	22-Jan-93	95.5	88.0	80-83	1 B	1
W-905	07-Apr-93	221.0	144.5	134-144	2	4
W-908	18-Aug-93	239.0	197.0	180-197	5/6	<0.5
W-909	04-Nov-93	252.0	113.5	80.5-108.5	2	2
W-911	20-Dec-93	180	113.5	73.5-108.5	2	3
W-912	07-Oct-93	239	174	168-174	5	3
W-913	08-Dec-93	454	255	235-255	4	25
W-1001	20-Dec-93	105	92	85-92	1 B	1.4
W-1002	31-Jan-94	292.5	260	246-260	5	16
W-1003	08-Feb-94	184.0	147	140-147	2	1.5
W-1005	14-Mar-94	192.0	110.0	98-110	1B	20

Well number	Date completed	Borehole depth (ft)	Casing depth (ft)	Perforated interval (ft)	HSU ^a monitored	Well development flow rate (gpm) ^b
W-1006	10-Mar-94	154.0	149.0	141-149	2	15
W-1007	31-Mar-94	199.5	182.0	172-182	3 A	2
W-1008	13-Apr-94	246	238	229.5-238	7	10
W-1010	24-May-94	463	142	128-142	2	20
W-1011	06-Jun-94	106	89	75-89	1 B	3
W-1012	20-Jun-94	161	117	96-112	2	5
W-1013	29-Jun-94	147	73	65-73	1 B	1.4
W-1014	12-Jul-94	99	89	65-89	1 B	30
W-1101	10-Nov-94	200.0	79.0	76.0-79.0	1 B	0.5
W-1105	17-Jan-95	110	93	78-93	1 B	3.5-4
W-1106	08-Feb-95	245	86	76-85	1 B	15
W-1107	06-Mar-95	199.5	93	74-88	1 B	<0.5
W-1108	27-Mar-95	250	156	142-156	5	12
W-1110	04-May-95	252	92.2	68-92	1 B	7
W-1112	28-Jun-95	263	210	201-210	5	3
W-1113	18-Jul-95	260	214	204-214	5	2.5
W-1115	12-Oct-95	126.5	118.2	108-118	3 A	1
W-1117	11-Sep-95	154	132.3	122-132	3 A	1
W-1118	27-Sep-95	225	125	115-125	3A	3.5
W-1201	18-Oct-95	225	133	125-133	3A	1
W-1202	26-Oct-95	99.3	99	83-99	2	5+
W-1203	07-Nov-95	224	206.2	196-206	5	18+
W-1204	20 Nov-95	225	126.2	118-126	3 A	2.5
W-1205	27-Nov-95	91	82	72-82	2	<0.5
W-1206	06-Dec-95	220	191	174-186	4	40+
W-1207	13-Dec-95	92	90	70-90	2	<0.5
W-1208	09-Jan-96	166	163	135-163	3A/3B	40
W-1209	26-Jan-96	210	164	148-164	4	3
W-1210	12-Feb-96	250	223	213-223	5	3
W-1211	05-Mar-96	273	205	185-200	4	25+
W-1212	19-Mar-96	150	75	52-75	1 B	3
W-1213	02-Apr-96	129	76	64-76	1 B	5+
W-1214	22-Apr96	180	100	80-100	1 B	2
W-1215	17-Apr-96	175	120	103-120.5	2	8.5

Well number	Date completed	Borehole depth (ft)	Casing depth (ft)	Perforated interval (ft)	HSU ^a monitored	Well development flow rate (gpm) ^b
W-1216	07-May96	200	124	94-124	2	14
W-1217	15-May96	182	98.5	78-98	1 B	<0.5
W-1218	29-May-96	240	145.5	127-145	3 A	6.7
W-1219	04-Jun-96	201	142	138-142	4	<0.5
W-1220	12-Jun-96	120	117	90-112	2	18
W-1221	01-Jul-96	220	172	162-172	4	4
W-1222	26-Jun-96	175	125.5	115-125	3 A	6
W-1223	23-Jul-96	175	102	87-97	2	4
W-1224	05-Sep-96	125	104.5	99-104	1 B	4.3
W-1225	14-Aug-96	150	121.2	113-121	3 A	2
W-1226	06-Aug-96	155	126.5	116-126	2	1
W-1227	09-Oct-96	200	134	126-134	2	11
W-1250	07-Jun-96	210	200	130-135	4	0.85
W-1251	03-Jul-96	210	200	134-139	4	1.3
W-1252	25-Jul-96	208	202.3	135-140	4	<0.5
W-1253	15-Aug-96	206	200.1	127-132	4	<0.5
W-1254	15-Aug-96	125	200	131-141	4	26
W-1255	27-Aug-96	208	200.7	124-129	4	<0.5
W-1301	04-Dec-96	180	120.3	112-120	3A	15
W-1302	21-Jan-97	145	138.9	116.5-122.2 125.8-133.8	3A	7.5
W-1304	20-Feb-97	149.5	125	120-125	3 A	0.75
W-1308	22-Jul-97	150	116	81-111	2	7
W-1309	11-Aug-97	220	157	142-152	4	6.0
W-1310	08-Sep-97	220	198	173-193	5	28
W-1311	25-Sep-97	153	120.5	100-120	2	14
W-1401	15-Oct-97	250	120	105-120	2	7
W-1402	04-Nov-97	135	112	102-112	3A	4
W-1403	12-Nov-97	175	142	132-142	4	3.5
W-1404	20-Nov-97	162	97.8	87-97	2	3.1
W-1405	24-Nov-97	100	97.8	87-97	2	4.5
W-1406	15-Dec-97	201	150.0	139.2-149.2	4	9.2
W-1407	12-Dec-97	224	118	105-118	2	1.5

Well number	Date completed	Borehole depth (ft)	Casing depth (ft)	Perforated interval (ft)	HSU ^a monitored	Well development flow rate (gpm) ^b
TW-11	09-Jun-81	112.5	107.0	97-107	2	NA
TW-11A	16-Mar-84	163.0	160.0	133-160	2	NA
TW-21	12-Jun-81	111.5	95.0	85-95	1B	NA
GEW-710	02-Aug-91	159.0	158.0	94-137	3A/3B	25
GSW-1A	12-Jun-86	208.0	133.0	115-133	3 B	12
GSW-2	14-Feb-85	113.0	107.0	87-107	3 A	NA
GSW-3	07-Feb-85	115.0	105.0	85-105	3 A	NA
GSW-4	22-Feb-85	112.0	106.0	86-106	3 A	NA
GSW-5	19-Mar-85	110.0	104.0	94-104	3 A	NA
GSW-6	28-Feb-86	212.0	137.0	121-137	3 B	6
GSW-7	14-Mar-86	176.5	123.4	110.8-123.4	3 B	2
GSW-8	01-Apr-86	176.0	133.0	127.5-133	3 B	2
GSW-9	14-Apr-86	197.5	152.5	147-152.5	3 B	1
GSW-10	29-Apr-86	205.5	127.5	114-127.5	3 B	8
GSW-11	07-May-86	182.5	126.0	116-126	3 B	2
GSW-12	27-May-86	205.0	191.0	186.5-191	5	1
GSW-13	27-Jun-86	198.0	134.5	125-134.5	3B	1
GSW-15	14-Aug-87	148.0	145.0	20.5-28	1 B	3.5
				38-44	1 B	
				50-56	2	
				60-64	2	
				68-73	2	
				77-83	2	
				95-105	3 A	
				120-130	3B	
GSW-16	19-Oct-87	146.0	145.0	23-28	1 B	20.5-30
				38-43	1 B	
				50-55	2	
				61-66	2	
				78-83	2	
				95-105	3A	
				120-130	3B	
GSW-208	06-Feb-86	211.0	123.0	108-118	3B	<2

Well number	Date completed	Borehole depth (ft)	Casing depth (ft)	Perforated interval (ft)	HSU ^a monitored	Well development flow rate (gpm) ^b
GSW-209	27-Feb-86	204.0	135.2	112.8-132.8	3B	2
GSW-215	22-Apr-86	213.5	133.5	127-133.5	3 A	2
GSW-216	09-May-86	193.0	120.5	110.5-120.5	3 B	3
GSW-266	08-May-86	220.0	166.0	159-166	3B	1
GSW-326	02-Oct-87	230.0	134.0	129-134	4	0.5
GSW-367	29-Apr-87	159.0	124.0	114-124	2	2
GSW-403-6	11-May-84	138.0	113.6	90-110	3A	NA
GSW-442	27-Oct-87	270.0	145.0	138-145	3 B	0.5
GSW-443	09-Nov-87	291.0	141.0	123-141	2	5
GSW-444	20-Nov-87	278.0	120.0	110-120	3 B	0.3
GSW-445	09-Dec-87	319.0	161.0	155-161	4	3
Dynamic Stripp	ving Project We	ells ^C				
GSP-SNL-001	07-Jan-92	147.0	104.0 131.0	99-104 118-131	3A 3B	NA NA
GEW-808	05-Jun-92	164.0	150.0	50-140	2/3A/3B	25
GIW-813	25-Jun-92	140.7	87.0 104.0	67-87 89-99	2 3A	NA
			127.0	107-127	3A/3B	NA
GIW-814	19-Jun-92	149.6	106.5 117.0	86.5-106.5 110-120	2/3A 3A	NA
			132.0	121-141	3B	NA
GIW-815	15-Jun-92	143.0	97.0 117.0	77-97 102-112	2/3A 3A	NA
			132.0	112.8-132	3B	NA
GEW-816	03-Jun-92	161.7	150.0	50-140	3A/3B	40
GIW-817	29-Jun-92	150.1	102.0 122.0	82-102 107-117	2/3A 3A	NA
			141.0	121-141	3B	NA
GIW-818	06-Jul-92	150.0	102 125	82-102 110-120	2/3A 3A	NA
			140	120-140	3B	NA
GIW-819	10-Jul-92	150.0	98.6 123	78.6-98.6 108-118	2/3A 3A/3B	NA
			141	121-141		NA

Well number	Date completed	Borehole depth (ft)	Casing depth (ft)	Perforated interval (ft)	HSU ^a monitored	Well developmen flow rate (gpm) ^b
GIW-820	16-Jul-92	143.3	105 132	85-105 112-132	2/3A 3A3B	NA NA
HW-GP-001	17-Apr-92	120.0	77.0 113.0	67-77 103-113	2 3A	NA NA
HW-GP-002	13-May-92	120.0	78.0 117.0	68-78 107-117	2 3A	NA NA
HW-GP-003	20-May-92	119.0	76.5 119.0	66.5-76.5 109-119	2 3A	NA NA
HW-GP-102	13-Aug-93	140.0	137.5	72.5-133.5	2/3A/3B	NA
HW-GP-103	23-Aug-93	138.0	137.5	71.5-132.5	2/3A/3B	NA
HW-GP-104	02-Sep-93	138.0	137.2	72.2-132.2	2/3A/3B	NA
HW-GP-105	28-Sep-93	138.0	137.5	72.5-132.5	2/3A/3B	NA
TEP-GP-106	21-Sep-93	137.5	135.5			
Extraction We	ells					
W-109	02-Apr-85	289.0	147.0	137-147	2	12
W-262	20-Mar-86	256.0	100.0	91-100	1 B	7
W-351	17-Oct-86	191.0	151.0	146-152	4	2.9
W-357	12-Jan-87	197.0	123.0	107-123	2	8
W-408	16-Feb-88	131.0	122.5	101-122.5	1 B	35
W-415	12-Aug-88	205.0	183.7	79-179	1B/2	>50
W-457	22-Jun-88	289.0	149.5	130-149.5	2	20
W-518	08-Aug-89	251.0	139.0	131-139	2	2.5
W-520	30-Aug-89	160.0	101.5	94-101.5	1 B	12
W-522	05-Oct-89	145.5	141.5	134-141.5	2	25
W-566	19-Apr-89	317.0	207.0	197-207	5	12
W-601	13-Oct-89	146.0	96.0	88-96	1B	15
W-602	06-Nov-89	168.0	100.0	90-100	1 B	10
W-603	15-Nov-89	150.0	147.0	141-147	2	5
W-609	21-Feb-90	120.0	112.0	104-112	2	4

Well number	Date completed	Borehole depth (ft)	Casing depth (ft)	Perforated interval (ft)	HSU ^a monitored	Well development flow rate (gpm) ^b
W-610	16-Mar-90	453.0	84.5	69-84.5	1 B	4
W-614	18-May-90	262.0	123.0	100-123	2	12
W-620	30-Aug-90	206.0	88.5	75-88.5	1 B	5
W-621	09-Sep-90	149.0	120.0	113-120	2	4
W-655	25-Apr-90	193.0	130.0	121-129.5	2	2
W-701	10-Oct-90	159.0	86.0	74-86	1 B	10
W-704	01-Feb-91	135.0	107.0	67-76 88-97	1 B	20
W-712	29-Aug-91	200.0	185.5	170-185.5	3A	8
W-903	28-Apr-93	223.0	145	132-140	2	20
W-904	06-May-93	212.0	154.0	121-133 140-149	2	20
W-906	27-Jul-93	200.0	132.0	58-132	2/3A	10
W-907	02-Sep-93	239.0	220.0	172.7-188.8 204.5-215.0	4 5	25 NA
W-1004	23-Feb-94	99.0	97.0	71-91	1 B	7
W-1009	02-May-94	191	140	134-140	2	20
W-1015	10-Aug-94	437	94	84-94	1B	20
W-1102	29-Nov-94	163.0	95.5	76.0-94.0	1 B	8
W-1103	15-Dec-94	200.0	82.0	70.0-82.0	1 B	3.5
W-1104	18-Jan-95	165.0	99.0	77-87 92-98	1 B	35+
W-1109	11-Apr-95	121	113	94-108	2	3
W-1111	01-Jun-95	152	129	88-108 120-124	1B/2 2	10.5 NA
W-1116	17-Aug-95	214	101	72-98	1 B	9
W-1303	06-Feb-97	199.5	107	78-102	2	10
W-1306	06-May-97	200	106	81-101	2	3.3
W-1307	07-Feb-97	150	142	126-136	4	20
Other Wells						
7D2	07-Jun-76	74	72.3	63.2-67.3	3A	NA
11C1	08-Jun-76	68	66.2	56.2-61.2	1B	NA

Well number	Date completed	Borehole depth (ft)	Casing depth (ft)	Perforated interval (ft)	HSU ^a monitored	Well development flow rate (gpm) ^b
11H5	08-Nov-85	NA	255	NA	NA	NA
11 J2	26-Apr-79	112	110	90-92	1 B	NA
				102-108	2	
11Q4	NA	NA	NA	NA	NA	NA
11Q5	NA	NA	NA	NA	NA	NA
14A3	07-Dec-77	NA	110	100-105	1 B	NA
14A11 ^d	NA	NA	NA	NA	NA	NA
14B1	13-Aug-59	300	234	146-149	2	NA
				192-195	3 A	
				198	3 A	
				200	3 A	
				203	3 A	
				205	3 A	
				207	3A	
				209-213	3A	
				226	3A	
				230	3B	
				234	3B	
14B4	Aug-60	NA	260	143-148	2	NA
	-			155-159	2	
				186-189	3A	
				205-215	3A	
				245-250	4	
14 B 7	NA	NA	NA	NA	NA	NA
14H1	NA	NA	288	NA	NA	NA
14H2 ^d	NA	NA	NA	NA	NA	
18D1 ^d	NA	NA	NA	NA	7	NA
Source Invest	igation Piezome	ters				
SIP-141-201	02-Feb-96	77	74.2	57-74	1 B	NA
SIP-141-202	12-Feb-96	80	74	64-74	1 B	NA
SIP-141-203	20-Feb-96	87	83	72-83	1 B	NA
SIP-191-001	15-Apr-94	50	45	40-45	1A	NA
SIP-191-002	21-Apr-94	50	61	45-61	1 B	NA
SIP-191-003	26-Apr-94	50.5	45	35-45	1B	NA
SIP-191-004	29-Apr-94	57.5	53.5	47.5-53.5	1 B	NA

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Well number	Date completed	Borehole depth (ft)	Casing depth (ft)	Perforated interval (ft)	HSU ^a monitored	Well development flow rate (gpm) ^b
SIP-191-005	04-May-94	54	48	42-48	1A	NA
SIP-191-101	18-Nov-94	68.5	64	58-64	1 B	NA
SIP-212-101	14-Mar-96	94	90.5	87-90.5	2	NA
SIP-293-001	05-Dec-90	56.5	50	45-50	1 B	NA
SIP-331-001	21-Sep-91	122	116.5	106.5-116.5	2	NA
SIP-419-101	08-Sep-98	127	123	112-123	3B	NA
SIP-419-201	29-Feb-96	126	107	97-107	3A/3B	NA
SIP-419-202	06-Mar-96	110	106.5	97-106.5	3A	NA
SIP-490-102	08-Nov-95	75	73.5	53.5-73.5	2	NA
SIP-501-004	20-0ct-94	60	56.9	48-56.9	1 B	NA
SIP-501-006	11-Nov-92	59.5	56	50-56	1 B	NA
SIP-501-007	16-Nov-92	64	59	53-59	1 B	NA
SIP-501-101	10-May-94	77.5	73	69-73	1 B	NA
SIP-501-102	16-May-94	77	73	67-73	1 B	NA
SIP-501-103	20-Mar-94	63	57.5	51-57.5	1 B	NA
SIP-501-104	15-Jul-94	67	62	50-62	1 B	NA
SIP-501-105	01-Sep-94	73	68	63-68	1 B	NA
SIP-501-201	29-Nov-94	65	58.5	54-58.5	1 B	NA
SIP-501-202	01-Jul-95	70	64.5	58-64.5	1 B	NA
SIP-511-101	25-Jan-96	110	106.7	100-106.7	3A	NA
SIP-511-102	02-Apr-96	114	110.3	108-110	3B	NA
SIP-514-107	03-Jan-90	21.5	17	9-17	1 B	NA
SIP-514-109	05-Jan-90	21.5	20	7-22	1 B	NA
SIP-514-112	08-Jan-90	21.5	18	7-18	1 B	NA
SIP-514-114	09-Jan-90	21.5	17	4-17	1 B	NA
SIP-514-116	10-Jan-90	21.5	17	7-17	1 B	NA
SIP-514-117	11-Jan-90	21.5	17.5	7-17.5	1 B	NA
SIP-514-119	12-Jan-90	21.5	16	6-16	1 B	NA
SIP-514-123	17-Jan-90	26.5	23	11.5-23	1 B	NA
SIP-514-124	18-Jan-90	21.5	17	6-17	1 B	NA
SIP-514-125	19-Jan-90	21.5	15	6-15	1 B	NA
SIP-514-126	18-Jan-90	26.5	21.5	4-21.5	1 B	NA
SIP-518-203	19-Sep-95	127	127	121-127	5	NA
SIP-543-101	31-Jan-95	111	104	43-103	2	NA
SIP-ALP-001	03-May-90	66	60	45-60	2	NA
SIP-ALP-002	07-May-90	62	57.5	47.5-57.5	1B/2	NA

Well Borehole Casing Perforated development HSU^a Well depth flow rate Date depth interval number completed (ft) (ft) (ft) monitored (gpm)^b SIP-AS-001 30-Apr-90 100 100.5 81-90.5 **1B** NA SIP-CR-049 26-Feb-90 42 40 36-40 **1B** NA SIP-EGD-001 16-Oct-90 101.5 85 75-85 3A NA SIP-ETC-201 106 101 81-101 2 NA 26-Mar-96 05-Feb-91 85-90 SIP-ETS-201 95 90 3A NA 87-97 SIP-ETS-204 07-May-91 93 97 3A NA SIP-ETS-205 20-Jun-91 103 95 89.5-95 3A NA SIP-ETS-207 11-Jul-91 89.75-98.5 3A 5 103.5 98.5 SIP-ETS-209 25-Jul-91 96.6 90 2 NA 79.75-90 SIP-ETS-211 06-Aug-91 103 98.5 95-98.5 3A NA SIP-ETS-212 14-Aug-91 106.5 1023 97.5-1023 2 NA SIP-ETS-213 15-Nov-91 118.5 116.5 108.5-116.5 3A NA 3A SIP-ETS-214 22-Nov-91 101 101 86-101 NA SIP-ETS-215 03-Dec-91 94.5 94.5 84.5-94.5 3A NA SIP-ETS-302 30-Mar-92 117.4 97-113 3A NA 113 110.7 95-102 3A NA SIP-ETS-303 02-Apr-92 102 NA SIP-ETS-304 27-Aug-92 100 97 90-97 3A 80-5-93 SIP-ETS-306 11-Sep-92 101 93 3A NA SIP-ETS-401 02-Aug-95 122 121 116-121 3A NA 08-Aug-95 SIP-ETS-402 110 97-107 2 NA 107 SIP-ETS-404 99 95.5 2 NA 22-Aug-95 83.5-95.5 3A NA SIP-ETS-405 29-Aug-95 126 123 114.5-123 SIP-ETS-501 16-Nov-95 110 106.5 100-1006.5 3A NA SIP-ETS-502 05-Dec-95 95 88 80-88 2 NA 92.75 75 2 NA SIP-HPA-001 20-Apr-90 65-75 SIP- HPA-003 91.5 2 NA 19-Apr-90 66 61-66 72 2 NA SIP- HPA-102 08-Dec-94 76 67-72 2 77 72.5 NA SIP-HPA-103 01-Mar-95 67-72.7 2 NA SIP- HPA-201 14-May-96 97.5 76 71-76 SIP-IES-001 16-Sep-92 50.2 46.5 44-46.5 1B NA SIP-IES-002 05-Oct-92 41.5 39.2 33-39.2 1A NA 5 NA SIP-ITR-001 19-Apr-91 121.6 115 105-115 84 79-84 2 NA SIP-ITR-002 02-Apr-91 100 SIP-ITR-003 25-Apr-91 121.5 106 98.5-106 5 NA SIP-NEB-101 23-Sep-92 68.7 66 57-66 2 NA UP-292-006 07-Nov-90 74 57.5 47.5-57.5 **1B** NA

Well number	Date completed	Borehole depth (ft)	Casing depth (ft)	Perforated interval (ft)	HSU ^a monitored	Well development flow rate (gpm) ^b
UP-292-007	26-Nov-90	71	56	46-56	1 B	NA
UP-292-012	31-Oct-91	67.7	60	45-60	1 B	NA
UP-292-014	07-Nov-91	66	66	50-66	1 B	NA
UP-292-015	11-Nov-91	61.5	60.5	49.5-60.5	1 B	NA
UP-292-020	30-Oct-92	68.5	64	56.5-64	1 B	NA
SIP-PA-002	29-Jan-90	16.5	16.5	4-16.5	1B	NA
SIP-PA-003	26-Jan-90	18	14	4-14	1B	NA
SIP-PA-005	04-Jan-90	11.5	8	3-8	1B	NA
SIP-PA-006	04-Jan-90	13.5	12	5-12	1B	NA
SIP-PA-007	04-Jan-90	11.5	5	1-5	1B	NA
SIP-PA-010	25-Jan-90	11.5	9	3-9	1B	NA
SIP-PA-012	29-Jan-90	11.5	9	2-9	1B	NA
SIP-PA-013	24-Jan-90	16.5	13	8-13	1B	NA
SIP-PA-015	25 -Jan-90	21.5	17.5	2-17.5	1 B	NA
SIP-PA-016	24 -Jan-90	11.5	11.5	7-11.5	1B	NA
SIP-PA-017	24 -Jan-90	16.5	14	7-14	1 B	NA
SIP-PA-018	25 -Jan-90	11.5	8	6-8	1 B	NA
SIP-PA-019	26 -Jan-90	16.5	12	2-12	1B	NA
SIP-PA-021	23 -Jan-90	11.5	10	2-10	1B	NA
SIP-PA-024	23 -Jan-90	16.5	15	5-15	1 B	NA
SIP-PA-025	23 -Jan-90	11.5	7	4-7	1B	NA
SIP-PA-026	29 -Jan-90	11.5	10	2-10	1 B	NA
SIP-PA-027	29 -Jan-90	8.5	7	2-7	1B	NA
SIP-PA-028	23 -Jan-90	11	8	5-8	1B	NA
SIP-PA-030	24 -Jan-90	11.5	8	4-8	1 B	NA
SIP-PA-034	04-Jan-90	6.5	5	3-5	1B	NA
SIP-PA-035	04 -Jan-90	11.5	11.5	6.5-11.5	1B	NA
Soil Vapor Ins	tallations					
SVI-518-101	21-Sep-90	125	61	55-61	2	NA
SVI-518-201	03-Mar-93	59.8	50	34-50	1B/2	NA
SVI-518-202	03-Nov-93	120.6	73.8	19-73.8	1B/2	NA
SVI-518-204	05-Nov-93	121.5	46	24-46	1B/2	NA
SEA-518-301	11-Sep-95	102.6	100	NA ^e	1B/2/5	NA
SVI-518-302	22-Jun-95	104.5	39.3	11-39	1 B	NA
SVI-518-303	29-Jun-95	104.5	42	6-40	1 B	NA
SEA-518-304	11-Sep-95	100	50	NA ^e	1B/2/5	NA

Well number	Date completed	Borehole depth (ft)	Casing depth (ft)	Perforated interval (ft)	HSU ^a monitored	Well development flow rate (gpm) ^b
SEA-ETS-305	03-9-92	85	85	NA ^e		NA
SVI-ETS-504	09-Jul-96	76.5	67	42-67	2	NA
SVI-ETS-505	18-Jul-96	80.5	77.5	45-75	2	NA
SEA-ETS-506	24-Jul-96	75	66	NA ^e	1B/2	NA
SEA-ETS-507	30-Jul-96	75	66	NA ^e	1 B /2	NA

Notes: Boreholes B-707, B-708, B-709, B-713, B-715, and B-750 were drilled for the Dynamic Underground Stripping Demonstration Project "Clean Site."

NA = Not applicable or not available.

^a Hydrostratigraphic Units (HSUs) are numbered consecutively downward from ground surface. An HSU is defined as sediments that are grouped together based on the hydrogeologic and contaminant transport properties. The permeable layers within an HSU are considered to be in good hydraulic communication, whereas permeable layers in different HSUs are considered to be in poor hydraulic communication. HSU contacts are interpreted and are subject to change.

^b Flow rate after 4 hours of air-lift pumping/surging.

^c Wells installed for the Dynamic Underground Stripping Demonstration Project include extraction wells (GEW series), injection wells (GIW series), temperature monitoring wells (TEP series), and heating wells (HW series). TEP wells consist of two nested 1-in. inside diameter (ID) piezometers surrounding a blank fiberglass 2-in. ID casing instrumented with geophysical sensors. The screened intervals listed therefore refer to the two individual piezometers.

^d Well number was changed in December 1988 to be consistent with Alameda County Flood Control and Water Conservation District, Zone 7 well identification. Well number changes made on this table are:

4A6 -----> 14H2 18D81 -----> 18D1 14A84 ----> 14A11

^e FLUTe/SEAMIST membranes with vapor ports set at varying depths.

Well number	Date installed	Borehole depth (ft)	Casing depth (ft)	Perforated interval (ft)	HSU monitored	Closure date
Monitor Wells	3					
W-14A	26-Aug-80	111.0	109.0	80,95,105	2	11-Dec-87
W-15	17-Nov-80	285.0	267.0	239-265	7	13-May-88
W-18	22-Aug-80	161.0	152.5	80-90	2	11-Nov-85
				100-105	2	
				112-117	3A	
				128-133	5	
				143-153	5	
GSW-1	05-Feb-85	112.0	109.0	85-106	3A	06-Jun-86
GSW-20	18-May-84	134.0	101.3	95-101.3	3A	03-Sep-87
W-149	23-Aug-85	201.0	169.0	161-169	2	29-Aug-96
W-150	13-Sep-85	212.0	162.0	157-162	2	11-Apr-90
W-352	29-Oct-86	235.0	201.0	181-201	4	18-Dec-97
W-358	04-Feb-87	248.0	239.0	230-239	7	15-Apr-94
W-1114	07-Aug-95	223	205	177-200	5	22-Apr-97
Extraction We	lls					
GEW-711	24-May-91	167.5	157.0	94-137	3A,3B	16-Jun-92
Other Wells						
1N1	15-Jan-48	600	600	427-442	7	21-Oct-88
				450-453	1 B	
				465-469	NA	
				500-515	NA	
				575-588	NA	
11A1	08-Jun-76	66	64.7	54.7-59.7	NA	18-Aug-88
2R9 (11A5) ^a	NA	NA	NA	NA	NA	19-Jul-88
11BA ^b	NA	NA	NA	NA	NA	10-Jun-87
11H1	04-Nov-41	NA	519	157-161	NA	31-Oct-88
				169-177	NA	
				224-228	NA	
				243-245	NA	
				254-256	NA	
				306-314	NA	
				319-327	NA	

Table A-2. Well closure data, Lawrence Livermore National Laboratory and vicinity, Livermore, California.

Well number	Date installed	Borehole depth (ft)	Casing depth (ft)	Perforated interval (ft)	HSU monitored	Closure date
				339-342	NA	
				414-419	NA	
				424-431	NA	
				477-479	NA	
11H4	05-Apr-60	272	272	166-170	NA	07-Oct-88
	-			174-176	NA	
				183-185	NA	
				200-202	NA	
				211-214	NA	
				224-230	NA	
				250-252	NA	
				260-265	NA	
11J1	1941	160	NA	NA	NA	03-Aug-88
11J4 ^c	1965	NA	NA	NA	NA	11-Oct-88
11K1	06-Jan-42	NA	621	247-255	NA	26-Sep-88
				272-276	NA	
				297-304	NA	
				322-339	NA	
				554-557	NA	
				580-602	NA	
11K2	NA	NA	232	NA	NA	03-Oct-88
11 Q 2	NA	NA	264	NA	NA	16-Aug-88
11Q3	NA	NA	120	NA	NA	10-Aug-88
11Q6 ^c	NA	NA	280	NA	NA	11-Jan-89
11R3	08-May-61	140	117	NA	NA	03-Sep-85
11 R 4	NA	NA	NA	NA	NA	03-Sep-85
11R5 ^c	NA	NA	NA	NA	NA	26-Jul-85
12M1	09-Dec-42	702	702	375-378	NA	15-Apr-84
				420-426	NA	
				452-473	NA	
				560-564	NA	
				609-621	NA	
				626-657	NA	
12N1	14-Apr-42	702	681	392-399	NA	24-Jan-89
				514-518	NA	

Well number	Date installed	Borehole depth (ft)	Casing depth (ft)	Perforated interval (ft)	HSU monitored	Closure date
				527-536	NA	
				666-670	NA	
				678-681	NA	
13D1 ^c	29-Oct-56	NA	400	200-400	NA	23-Aug-88
14A1 ^c	12-Jul-43	246	227	102-107	NA	13-Sep-88
				113-119	NA	
				144-148	NA	
				176-179	NA	
				188-190	NA	
				192-194	NA	
				219-222	NA	
				223-227	NA	
14A2 ^c	15-Nov-56	NA	229	122-130	NA	12-Sep-88
				140-150	NA	
				160-180	NA	
14A4 ^c	15-Jun-59	NA	252	167-170	NA	29-Aug-88
				175-179	NA	
				192-202	NA	
				235-246	NA	
14A8	NA	NA	86	NA	NA	22-Jul-88
14B2	22-Aug-56	NA	312	185-312	NA	11-Nov-88
14B8	NA	NA	385	NA	NA	23-Oct-89
TEP-GP-001	21-Jan-92	165.0	97.0 117.0 160.5	87-97 107-117	3A 3B	09-Feb-93
TEP-GP-003	28-Jan-92	161.0	129.5 161.0	124.5-129.5	3 B	13-Feb-93
TEP-GP-004	05-Feb-92	161.0	106.0 134.0 161.0	96-106 124-134	3A 3B	13-Feb-93
TEP-GP-005	18-Feb-92	161.0	124.5 161.0	114.5-124.5	3B	13-Feb-93
TEP-GP-006	26-Feb-92	161.0	127.0 161.0	107-127	3B	13-Feb-93
TEP-GP-007	13-Mar-92	161.0	161.0			NA

Well number	Date installed	Borehole depth (ft)	Casing depth (ft)	Perforated interval (ft)	HSU monitored	Closure date
TEP-GP-008	03-Mar-92	161.0	110.0 161.0	100-110	3 A	13-Feb-93
TEP-GP-009	06-May-92	161.7	107.0 130.5 161.0	98-107 120.5-130.5	3A 3B	13-Feb-93
TEP-GP-010	24-Mar-92	161.0	124.5	114.5-124.5	3 B	12-Feb-93
TEP-GP-011	07-Apr-92	161.0	108.0 161.0	98-108	3A	13-Feb-93
TEP-GP-002	24-Jun-92	161.4	133.0 161.0	102-112.5 122-133	3A 3B	NA
Source Investig	gation Piezomet	ters				
SIP-ETS-105	11-Feb-90	110	103	87-103	3A	18-Nov-93
SIP-PA-029	22 -Jan-90	11.5	7	5-7	1 B	18-Nov-93
SIP-490-101	01-Nov-95	59	56	53-56	2	21-Dec-95
SIP-514-101	28-Dec-29	26	22	7-22	1 B	03-Sep-96
UP-292-001	03-Dec-90	54.6	49.5	44.5-49.5	1 B	25-Sep-95

Note:

NA = Not applicable or not available.

^a Well 11A5 was renamed 2R9 by the Alamada County Flood Control and Water Conservation District, Zone 7 in November 1997. Well 11A5 now corresponds to monitor well W-409.

^b Well not recognized by Alameda County Flood Control and Water Conservation District, Zone 7.

^c Well number was changed in December 1988 to be consistent with Alameda County Flood Control and Water Conservation District, Zone 7 well identification. Well identification changes made on this table are:

11J81 -----> 1J4 11R81 -----> 11R5 11Q81 -----> 11Q6 13D81 -----> 13D1 14A81 -----> 14A1 14A82 -----> 14A2 14A83 -----> 14A4 **Appendix B**

Hydraulic Test Results

Well	Date	Type of test ^b	Flow rate (Q) (gpm)	Transmis- sivity (T) (gpd/ft)	Hydraulic conductivity (K) ^c (gpd/sq ft)	Data quality ^d
W-001	1-Dec-83	Drawdown	5.7	2,000	110	Fair
W-001	23-Jan-85	Drawdown	7.1	3,100	170	Good
W-001A	22-Jan-85	Drawdown	1.4	190	19	Good
W-002	1-Dec-83	Slug	0.0	110	34	Poor
W-002A	24-Jan-85	Drawdown	10.3	2,700	200	Good
W-004	1-Dec-83	Drawdown	3.3	63	13	Good
W-005	1-Dec-83	Drawdown	4.3	110	20	Good
W-005	24-Jan-85	Drawdown	7.9	1,100	210	Fair
W-005A	23-Jan-85	Drawdown	13.0	1,300	130	Poor
W-007	1-Dec-83	Slug	0.0	43	14	Fair
W-008	1-Dec-83	Drawdown	2.9	29	4.9	Fair
W-011	1-Dec-83	Drawdown	4.1	130	15	Good
W-017	1-Dec-83	Slug	0.0	38	2.5	Good
W-017	21-Feb-86	Slug	0.0	85	5.7	Good
W-018	1-Dec-83	Drawdown	2.6	20	2.7	Poor
W-102	25-Mar-86	Drawdown	6.4	1,100	76	Good
W-102	5-Sep-86	Drawdown	24.0	770	53	Good
W-102	15-Sep-86	Longterm	27.5	4,200	290	Good
W-103	25-Apr-86	Drawdown	6.7	15,000	1,500	Good
W-104	3-Mar-88	Drawdown	5.4	1,200	170	Fair
W-104	25-Mar-88	Drawdown	3.3	450	45	Fair
W-105	6-Apr-87	Drawdown	0.8	73	7.3	Fair
W-106	19-Feb-86	Slug	0.0	7.4	1.3	Excel
W-107	17-Jun-85	Drawdown	1.0	94	9.4	Poor
W-108	29-Oct-85	Drawdown	7.9	750	63	Poor
W-109	5-Mar-86	Drawdown	8.1	3,200	530	Good
W-109	4-Sep-87	Drawdown	20.0	1,600	270	Good
W-109	29-Sep-87	Longterm	11.6	130	22	Fair
W-109	16-Oct-87	Drawdown	8.0	2,300	380	Fair
W-110	18-Jun-85	Drawdown	5.0	1,300	130	Good
W-111	13-Jun-85	Drawdown	1.0	370	37	Good
W-111	21-Nov-85	Drawdown	1.0	370	37	Good
W-112	18-Nov-86	Drawdown	13.4	2,100	170	Fair
W-112	15-Dec-86	Longterm	13.2	3,100	260	Fair

Table B-1. Results of hydraulic tests^a.

Flow Transmis-Hydraulic rate sivity conductivity Type of (Q) (T) (K)^c Data qualityd test^b Well Date (gpd/ft) (gpd/sq ft) (gpm) W-112 5-Nov-96 Longterm 13.7 3,300 260 Fair W-113 0.0 7.4 1.2 17-Apr-86 Slug Excel Drawdown 30 W-115 5-Mar-86 1.1 180 Good 0.0 7.5 Good W-116 24-Dec-85 Slug 37 W-117 20-Feb-86 Slug 0.0 2 0.4 Good W-118 5-Mar-86 Drawdown 10.0 230 Good 2,100 W-119 Drawdown 1,600 110 Good 8-Aug-85 2.0 W-120 22-Apr-86 Drawdown 1.1 23 5.6 Poor W-121 10-Sep-85 Drawdown 2.0 120 7.5 Good W-121 23-Sep-85 Drawdown 4.0 23 1.5 Excel W-121 14-Oct-85 Drawdown 3.0 34 2.2 Excel W-121 15-Oct-85 Drawdown 4.5 45 3.0 Excel W-122 28-Oct-85 Drawdown 490 49 10.8 Good W-123 28-Oct-85 Drawdown 5.8 40 4.4 Poor W-142 330 3-Mar-88 Slug 0.0 2,600 Excel W-143 3-Mar-88 Slug 0.0 1,200 240 Excel Drawdown 19 Good W-149 9-Sep-85 4.0 120 W-149 Drawdown 8.0 95 Excel 11-Sep-85 16 Drawdown 9.7 Excel W-149 11-Oct-85 4.8 58 W-149 11-Oct-85 Drawdown 7.0 70 12 Good W-150 2-Oct-85 Drawdown 640 210 Fair 3.1 W-150 3-Oct-85 Drawdown 6.0 720 240 Fair W-150 10-Oct-85 Drawdown 8.8 630 210 Fair Fair W-150 10-Oct-85 Drawdown 12.0 620 210. Poor W-151 28-Oct-85 Drawdown 5.8 550 61 W-201 5-Mar-86 Drawdown 10.0 740 86 Excel W-203 2-Mar-88 Drawdown 6.6 1,100 110 Good W-204 Drawdown 100 15 Fair 23-Jan-86 1.9 W-205 14-Feb-86 Slug 0.0 5.9 1.9 Good W-205 18-Feb-86 Slug 0.0 5.9 1.9 Good W-206 14-Apr-86 Slug 0.0 120 11 Good W-207 2-Mar-88 Slug 0.0 380 32 Excel 9-Jun-86 W-210 Slug 0.0 0.6 0.1 Good 2.9 37 W-211 22-Oct-86 Drawdown 12 Fair W-211 15 Fair 8-Dec-86 Longterm 1.0 44

Flow Transmis-Hydraulic rate sivity conductivity Type of (Q) (T) (K)^c Data quality^d test^b Well Date (gpd/ft) (gpd/sq ft) (gpm) W-211 16-Sep-97 Longterm 1.1 14 1.4 Good W-212 Drawdown 0.8 18 3.1 12-May-86 Poor 38 W-213 22-Apr-86 Drawdown 3.8 190 Good 350 Good W-214 7-Oct-86 Longterm 27.6 2,300 W-217 15-Jul-86 Slug 0.0 750 120 Good W-218 17-Jun-86 Drawdown Good 11.7 6,400 1,100 4,000 670 Good W-218 12-Nov-86 Longterm 7.7 76 Good W-219 15-Jul-86 Drawdown 4.3 620 W-219 23-Feb-87 Longterm 5.2 66 8.0 Fair W-220 21-Aug-86 Slug 0.0 28 5.5 Excel W-221 Drawdown 2.1 120 16 Fair 5-Aug-86 W-222 12-Aug-86 Drawdown 16.0 1,700 160 Excel W-222 180 8-Mar-85 Longterm 7.7 1,100 Good W-223 27-Aug-86 Drawdown 4.0 510 110 Good W-224 28-Oct-86 Drawdown 400 7.6 3,600 Excel W-225 23-Oct-86 Drawdown 4.0 85 11 Good W-225 12-Jan-87 Longterm 2.0 62 8.5 Fair W-226 160 Fair 31-Mar-87 Slug 0.0 1,700 W-252 Drawdown 4.0 50 Fair 4-Nov-85 920 W-252 19-Nov-85 Drawdown 5.6 800 43 Fair W-254 27-Jan-86 Drawdown 340 38 Fair 4.2 W-254 27-Feb-86 Drawdown 3.2 370 41 Good W-255 21-Jan-86 Drawdown 5.0 2,800 250 Fair W-255 21-Jan-86 Drawdown 6.0 2,000 180 Fair Fair W-255 6-Jan-87 Longterm 2.0 400 36 W-256 11-Apr-86 Slug 0.0 11 5.5 Good W-257 15-Apr-86 Slug 0.0 120 24 Good W-258 Slug 0.0 35 9.0 Excel 5-Jun-86 W-258 32 29-Oct-86 Slug 0.0 8.0 Good W-259 26-Mar-88 Slug 0.0 15 5.0 Good W-260 25-Mar-86 Drawdown 3.0 140 22 Good W-260 1-Oct-86 Longterm 1.4 120 18 Good 7 W-261 27-May-86 Slug 0.0 2.3 Excel 250 W-262 11-Apr-86 Drawdown 12.5 2,000 Excel W-262 22.0 340 Good 23-Sep-86 Longterm 2,750

Flow Transmis-Hydraulic rate sivity conductivity Type of (Q) (T) (K)^c Data quality^d test^b Well Date (gpd/ft) (gpd/sq ft) (gpm) W-262 27-Apr-87 Longterm 23.1 6,800 810 Good W-263 Drawdown 37 7.4 22-Apr-86 1.2 Poor 15 W-263 4-Nov-86 Longterm 1.8 76 Excel Drawdown 930 100 Good W-264 7-May-86 8.1 W-264 29-Oct-86 Longterm 23.0 480 50 Good W-265 Drawdown 0.7 34 Fair 19-May-86 180 W-267 Drawdown 0.5 420 85 2-Jun-86 Poor Drawdown Good W-268 14-Nov-86 5.0 230 18 W-269 14-Jul-86 Drawdown 5.0 570 95 Good W-270 30-Dec-86 Slug 0.0 14 2.0 Good W-271 Drawdown 5.5 340 76 Fair 4-Aug-86 W-272 19-Aug-86 Drawdown 0.8 150 30 Fair Drawdown 600 90 W-273 27-Aug-86 3.2 Good W-274 25-Mar-85 0.0 38 7.6 Fair Slug W-275 30-Oct-86 Drawdown 7.0 730 150 Fair W-275 2-Mar-87 Longterm 5.5 830 170 Fair 110 W-276 21-Nov-86 Drawdown 13.0 960 Good W-276 4-May-87 300 Fair Longterm 24.0 2,700 W-277 Drawdown 0.9 25 Fair 3-Nov-86 74 W-290 5-Jan-87 Slug 0.0 14 4.0 Excel W-291 27-Jan-87 0.0 25 7.1 Fair Slug W-292 28-Aug-86 Drawdown 6.0 400 56 Excel W-294 29-Dec-86 Drawdown 5.3 5,300 29 Fair W-294 29-Dec-86 Drawdown 5.9 5,400 300 Good Good W-301 30-Oct-86 Drawdown 6.0 460 100 W-302 18-Nov-86 Drawdown 1.0 100 27 Good W-302 18-Nov-86 Drawdown 2.0 76 21 Fair W-303 12-Nov-86 Drawdown 70 Good 11.1 210 W-304 Drawdown 0.9 74 25 Fair 13-Mar-87 W-305 26-Nov-86 Drawdown 19.0 720 72 Excel W-305 18-May-87 Longterm 20.1 640 64 Excel W-306 31-Mar-87 Drawdown 9.5 270 68 Good W-307 26-Mar-87 Drawdown 0.9 66 33 Fair W-308 27 4-Dec-87 Drawdown 2.6 5.4 Good W-310 Drawdown 6.7 850 Good 17-Feb-87 58

Flow Transmis-Hydraulic rate sivity conductivity Type of (Q) (T) (K)^c Data quality^d test^b (gpd/sq ft) Well Date (gpd/ft) (gpm) W-311 19-Mar-87 Drawdown 9.8 130 12 Good 17-Nov-87 9.9 W-311 370 26 Good Longterm 300 W-312 27-Mar-87 Drawdown 20.5 1,800 Poor 280 Good W-312 3-Nov-87 Longterm 18.8 1,700 W-313 25-Mar-87 Drawdown 7.9 3.000 600 Good W-313 5-Oct-87 9.6 680 Good Longterm 3,400 Drawdown 390 Good W-314 10-Apr-87 26.4 2,900 Fair W-314 13-Jul-87 Longterm 13.6 2,500 330 W-314 14-Oct-97 Longterm 12 1,400 100 Fair W-315 9-Apr-87 Drawdown 15.4 150 11 Good W-315 571 41 Excel 5-Jan-85 Longterm 24.5 W-316 4-May-87 Drawdown 7.8 1,400 280 Good W-317 Drawdown 12-May-87 12.1 300 43 Fair W-317 15-Dec-87 Longterm 8.2 120 17.1 Good 0.0 W-318 7-Aug-87 Slug 120 16 Good W-319 29-Jul-87 Drawdown 48.0 7,200 1,500 Good W-320 15-May-87 Drawdown 1.8 17 Fair 58 W-320 3.0 22 3.7 Fair 15-May-87 Drawdown 49 14 Fair W-320 26-Jun-87 Drawdown 2.1 W-321 28-Jul-87 Drawdown 40.0 6,600 450 Good W-322 3-Aug-87 Drawdown 15 Good 3.1 85 59 W-323 11-Aug-87 Drawdown 3.4 205 Good W-324 10-Sep-87 Drawdown 6.6 200 50 Good W-325 10-Sep-87 Drawdown 6.0 160 13 Excel Poor W-351 12-Nov-86 Drawdown 5.7 27 14 W-352 30-Dec-86 Drawdown 20.0 280 14 Good W-352 7-Jul-87 Longterm 19.5 120 6.0 Excel W-353 20-Nov-86 Drawdown 60 17 Good 2.1 W-354 220 30-Dec-86 Drawdown 17.6 2,000 Fair W-354 30-Dec-86 Drawdown 18.0 2,400 260 Good W-354 20-Apr-87 Longterm 17.8 310 34 Good W-355 29-Dec-86 Drawdown 2.1 19 5.0 Fair W-356 17-Mar-87 Drawdown 5.7 180 59 Good 230 W-356 16-Jul-96 Longterm 4.9 57 Poor W-357 Good 18-Feb-87 Drawdown 15.0 1,300 110

Flow Transmis-Hydraulic rate sivity conductivity Type of (Q) (T) (K)^c Data quality^d test^b (gpd/sq ft) Well Date (gpd/ft) (gpm) W-357 21-Jul-87 Longterm 9.2 210 18 Good W-358 Drawdown 9.2 210 32 18-Mar-87 Excel 290 W-359 9-Mar-87 Longterm 19.0 2,800 Fair Good W-359 20-Mar-87 Drawdown 18.6 1,100 110 W-360 22-May-87 Drawdown 30.0 4.800 210 Excel W-361 16-Mar-87 Drawdown Good 4.3 67 11 5.3 30 Good W-361 12-Jan-85 Longterm 178 49 Good W-362 23-Mar-87 Drawdown 16.4 470 W-362 21-Sep-87 Longterm 13.6 370 39 Good W-363 24-Jul-87 Slug 0.0 20 3.0 Excel W-364 Drawdown 10 Fair 8-Apr-87 8.6 51 W-364 1-Jun-87 Longterm 4.8 110 22 Good W-365 14-May-87 Drawdown 10.0 36 15 Fair 92 W-366 11-May-87 Drawdown 19.0 780 Fair 2.9 8.5 W-368 11-May-87 Drawdown 81 Fair W-369 25-Jun-87 Drawdown 7.0 580 96 Good 89 W-369 10-Nov-87 Longterm 5.5 18 Good W-370 23-Jun-87 Drawdown 10 Fair 4.4 84 15 3.0 Good W-371 24-Jun-87 Drawdown 3.3 W-372 23-Nov-87 Slug 0.0 310 62 Excel W-373 28-Jul-87 Drawdown 4.0 77 Fair 660 W-373 28-Jul-87 Drawdown 6.5 50 6.0 Poor W-376 26-Jan-88 Drawdown 2.9 65 8.5 Fair W-380 23-Oct-87 Drawdown 4.0 33 4.7 Excel Excel W-401 23-Oct-87 Drawdown 42.0 950 24 W-402 22-Oct-87 Drawdown 41.0 13,500 1,400 Good W-403 3-Dec-87 Drawdown 9.7 370 26 Good W-404 4-Feb-85 Drawdown 530 Good 45.0 3,200 W-405 16-Feb-85 Drawdown 47.2 546 14 Good W-406 Drawdown 7.4 7,500 940 Fair 28-Jan-85 W-407 23-Feb-85 Drawdown 14.4 75 7.5 Fair 3,100 W-408 5-Apr-85 Drawdown 45.0 43,000 Good W-409 22-Mar-85 Drawdown 20.0 230 38 Good 570 W-410 28-Apr-85 Drawdown 35.0 6,800 Fair W-411 83 Good 5-May-85 Drawdown 14.0 50

Flow Transmis-Hydraulic rate sivity conductivity Type of (Q) (T) (K)^c Data quality^d test^b (gpd/sq ft) Well Date (gpd/ft) (gpm) W-412 6-May-88 Drawdown 4.1 700 64 Fair W-414 27-Jul-85 Slug 0.0 150 38 Good 78 W-415 31-Aug-85 Drawdown 10.0 3,100 Fair 11-Jul-85 Drawdown 330 Good W-416 50.0 2,600 W-417 27**Jun-88** Drawdown 5.3 340 57 Fair W-420 Drawdown 100 Excel 16-Aug-85 3.5 710 12-Sep-85 27 W-421 Drawdown Excel 4.8 320 W-422 Drawdown 42 Good 19-Sep-85 8.6 230 W-423 12-Oct-85 Drawdown 22.0 1,500 130 Good W-424 17-Oct-85 Drawdown 4.5 130 19 Good W-441 30-Oct-87 Drawdown 6.0 500 56 Good W-441 13-Apr-88 Drawdown 13.0 2,200 240 Poor W-441 52 19-Apr-88 Longterm 14.0 470 Good W-447 26-Feb-88 Drawdown 7.1 124 850 Poor W-448 24-Mar-85 Drawdown 600 24.5 4,200 Good W-449 21-Mar-85 Drawdown 6.2 170 11 Good 650 W-450 14-Apr-88 Drawdown 3.3 38 Fair W-451 27-Apr-88 Drawdown 80 Good 2.1 16 W-452 2-May-88 Drawdown 5.2 310 21 Excel W-453 3-May-88 Drawdown 5.8 67 7.4 Fair W-455 22-Jun-88 Drawdown 13 Good 5.8 160 W-456 14-Jul-85 Drawdown 4.5 260 33 Fair W-457 29-Jul-85 Drawdown 20.5 450 24 Excel Fair W-458 2-Aug-85 Drawdown 0.8 24 150 Fair W-460 1-Sep-85 Drawdown 17.0 1,900 380 W-461 7-Sep-85 Slug 0.0 690 140 Good 27-Sep-85 W-462 Drawdown 19.0 360 60 Good W-463 11-Oct-85 Drawdown 1,600 200 Good 24.0 W-464 Drawdown 9.0 Good 8-Nov-88 370 53 W-481 2-Dec-87 Drawdown 8 1.7 Good 1.1 W-486 23-Mar-85 Drawdown 6.0 230 30 Good W-487 14-Apr-88 Drawdown 2.2 45 15 Good W-501 21-Oct-85 Drawdown 9.7 170 21 Good 12 W-502 14-Nov-85 Slug 0.0 30 Good W-503 Drawdown 1.3 15 Fair 11-Nov-88 3.0

Flow Transmis-Hydraulic rate sivity conductivity Type of (Q) (T) (K)^c Data quality^d test^b (gpd/sq ft) Well Date (gpd/ft) (gpm) W-504 8-Dec-85 Drawdown 10.0 590 84 Good W-505 Drawdown 34.2 653 76 Good 21-Mar-89 W-506 10-Feb-89 Drawdown 31.0 7,423 460 Good W-507 Drawdown 39.0 290 Good 6-Feb-89 2,900 W-508 29-Mar-89 Drawdown 30.0 47.000 2,600 Good W-509 11-May-89 Drawdown 0.9 Fair 10 2.0 11-May-89 W-510 0.0 110 Good Slug 220 11 Fair W-511 11-May-89 Drawdown 1.7 63 W-512 27-Apr-89 Drawdown 2.9 85 9.4 Good W-513 9-May-89 Drawdown 0.6 33 3.0 Fair W-514 26-May-89 Drawdown 84 530 Fair 1.4 W-515 6-Jun-89 Drawdown 2.8 37 4.2 Fair W-516 Drawdown 19-Jun-89 19.5 1,428 286 Good W-517 27-Jun-89 Drawdown 7.3 370 53 Good 178 Good W-518 10-Aug-89 Drawdown 6.2 1,421 W-519 31-Aug-89 Drawdown 31.5 5,700 475 Excel W-520 24-Jan-90 Drawdown 22.8 3,300 560 Excel W-521 1-Feb-90 Drawdown Fair 0.6 44 4.9 W-522 5-Feb-90 Drawdown 620 Fair 20.0 3,700 W-551 8-Nov-85 Drawdown 37.0 350 88 Good W-552 12-Dec-88 Drawdown 390 Good 38.0 4,700 W-553 17-Nov-85 Drawdown 2.2 55 7.9 Fair 10-Jan-89 W-554 Drawdown 21.5 1.800 150 Good W-555 28-Dec-88 Drawdown 14.0 460 23 Fair Fair W-556 25-Jan-89 Drawdown 17.0 850 170 W-557 23-Jan-89 Drawdown 1.2 570 36 Poor W-558 23-Mar-89 Drawdown 24.7 5,200 650 Good W-560 8-Mar-89 Drawdown Fair 1.7 30 7.6 W-561 13-Mar-89 Drawdown 1.1 12 2.1 Fair W-562 28-Mar-89 Drawdown 1.0 2.3 Fair 16 W-563 31-Mar-89 Drawdown 1.1 14 2.3 Fair W-564 26-Apr-89 Drawdown 1.6 44 5.0 Poor W-565 18-Apr-89 Drawdown 15.6 1,600 260 Good 780 W-566 2-May-89 Drawdown 17.0 86 Good W-566 22.5 2580 520 Fair 31-Aug-93 Longterm

Flow Transmis-Hydraulic rate sivity conductivity Type of (Q) (T) (K)^c Data quality^d test^b Well Date (gpd/ft) (gpd/sq ft) (gpm) W-567 4-May-89 Drawdown 10.4 2,600 320 Excel W-568 20-Jun-89 Drawdown 18.3 160 Fair 620 15 W-569 24-May-89 Drawdown 2.8 100 Fair Drawdown 7 Fair W-570 8-Jun-89 1.1 1.1 W-571 17-Jul-89 Drawdown 17.7 1.000 200 Excel W-592 23-Jan-89 Drawdown 2,200 280 Poor 2.2 W-593 22-Feb-89 Drawdown 57 Good 2.2 11.4 0.0 54 Excel W-594 16-Mar-89 Slug 380 W-601 8-Feb-90 Drawdown 22.5 6,900 770 Excel W-602 29-Jan-90 Drawdown 24.0 5,300 620 Good W-603 7-Feb-90 Drawdown 100 20 Fair 6.1 W-604 20-Feb-90 Slug 0.0 380 63 Good W-605 28-Feb-90 Drawdown 4.8 50 12 Good W-606 21-Feb-90 Slug 0.0 120 20 Fair W-607 22-Feb-90 Drawdown 800 100 1.4 Good W-608 28-Feb-90 Drawdown 1.2 230 30 Fair W-609 470 70 9-Mar-90 Drawdown 6.7 Good W-610 Drawdown 5.8 380 Good 28-Mar-90 5,500 16-Apr-90 Drawdown 110 Fair W-611 3.5 1,000 W-612 24-May-90 Drawdown 13.5 550 55 Good W-612 05-Apr-94 230 40 Good Longterm 14 W-613 23-May-90 Drawdown 4.8 2,550 360 Good W-614 7-Jun-90 Drawdown 6.7 1,650 130 Good W-615 21-Jun-90 Drawdown 1.3 130 19 Fair 27-Jun-90 Fair W-616 Drawdown 2.0 390 40 W-617 12-Jul-90 Drawdown 2.8 53 6.8 Good W-618 1-Aug-90 Drawdown 1.9 24 4.8 Fair W-619 Drawdown 190 11 Good 30-Aug-90 11.8 W-620 Drawdown 650 1-Oct-90 5.8 6,500 Good W-621 4-Oct-90 Drawdown 310 39 Good 3.8 W-622 12-Oct-90 Slug 0.0 130 16 Fair W-651 16-Mar-90 Slug 0.0 530 180 Fair W-652 22-Mar-90 Drawdown 1.0 11 3.8 Good 2 W-653 11-Apr-90 Drawdown 0.3 1.9 Fair W-654 390 25 25-Apr-90 Drawdown 21.7 Fair

Flow Transmis-Hydraulic rate sivity conductivity Type of (Q) (T) (K)^c Data quality^d test^b (gpd/sq ft) Well Date (gpd/ft) (gpm) W-655 12-May-90 Drawdown 12.2 1,000 220 Good W-701 23-Oct-90 Drawdown 6,800 650 Good 14.5 W-701 3-Oct-92 16.5 5,200 430 Good Step Drawdown 370 Good W-701 1-Apr-93 24 3,700 W-702 29-Nov-90 Drawdown 2.5 150 30 Good W-702 25-Feb-93 7 Step 4.6 36 Poor W-703 19-Dec-90 Drawdown 7.0 9.1 Good 230 Drawdown 140 Fair W-704 4-Mar-91 19.0 1,800 W-705 20-Feb-91 Drawdown 0.8 40 6.1 Fair W-706 29-Jan-91 Drawdown 0.2 8 1 Fair W-712 25-Feb-92 Drawdown 7.8 48 750 Good W-712 18-Mar-93 Longterm 15.1 1440 93 Good W-714 6-Dec-91 Drawdown 2.9 140 6.7 Good W-902 25-Mar-93 Drawdown 0.6 2 Fair 6 W-909 18-Oct-95 Drawdown 150 2.7 5.1 Good W-911 2-Feb-96 Drawdown 1.4 53 2.1 Good W-912 10-Nov-95 Drawdown 4.1 65 11 Poor W-913 23.5 36 Good 16-Aug-95 Drawdown 730 170 25 Fair W-1001 13-Aug-95 Drawdown 1.3 W-1002 19-Jun-97 Drawdown 16.8 680 49 Good W-1003 Drawdown 0.7 Poor 26-Jun-97 1.2 5.1 W-1006 17-Jun-97 Drawdown 17.4 180 23 Fair W-1007 23-Sep-95 Drawdown 1.6 13 1.3 Fair W-1008 17-Jan-97 Drawdown 7.3 110 13 Good Fair W-1010 10-Jul-95 Drawdown 20.3 1,650 140 W-1011 11-Jul-95 Drawdown 3.8 240 17 Good W-1012 13-Jul-95 Drawdown 3.3 35 2.2 Fair W-1013 13-Jul-95 Drawdown 2,000 250 Poor 2.7 W-1014 320 28-Aug-96 Drawdown 31.1 7,700 Good W-1101 22-Nov-95 Drawdown 0.8 9.9 3.3 Good W-1102 29-Jan-96 Drawdown 14.7 81 4.5 Fair W-1103 29-Nov-95 Drawdown 3 19 1.6 Fair W-1105 17-Jul-95 Drawdown 2.4 320 26 Fair W-1106 24-Jul-96 Drawdown 7.1 5,200 580 Good 6.7 250 W-1107 9-Apr-97 Drawdown 3,500 Poor

Flow Transmis-Hydraulic rate sivity conductivity Type of (Q) (T) (K)^c Data quality^d test^b (gpd/sq ft) Well Date (gpd/ft) (gpm) W-1108 3-Nov-95 Drawdown 12.3 950 68 Good W-1108 1,000 70 25-Jun-96 Longterm 11.6 Poor W-1109 26-Jun-95 Drawdown 8.7 460 33 Fair W-1109 4-Jun-96 Longterm 6.8 760 40 Poor W-1110 22-Jan-96 Drawdown 6.3 690 29 Fair W-1111 20-Oct-95 Drawdown 95 Good 15.8 2,100 160 7.9 W-1111 9-Dec-96 Longterm 11.2 Poor 6.4 10 Fair W-1112 24-May-96 Drawdown 94 W-1113 26-Aug-96 Drawdown 1 5.5 0.6 Good W-1114 27-Oct-95 Longterm 15.1 270 12 Fair W-1116 23-Feb-96 Drawdown 290 11 Fair 6.6 W-1117 23-Aug-96 Drawdown 0.7 3.4 0.34 Fair Drawdown 350 W-1118 18-Jan-96 5.6 35 Good W-1201 1-Nov-96 Drawdown 1 8.3 0.92 Poor Drawdown 900 90 W-1203 2-May-96 18.8 Good W-1204 22-Feb-96 Drawdown 1.3 17 2.2 Poor 0 330 W-1205 27-Nov-96 Slug 33 Fair 0 45 W-1207 27-Nov-96 900 Poor Slug Drawdown 0.98 W-1209 17-May-96 11 0.69 Good W-1210 30-May-96 Drawdown 3.8 7.3 0.73 Fair W-1211 26-Jul-96 Drawdown 5,000 330 Good 28.6 W-1212 14-May-96 Drawdown 1.9 35 2.5 Good W-1212 10-Sep-96 Longterm 1.3 85 3.6 Poor Fair W-1213 22-Jul-96 Drawdown 11.6 500 42 37 W-1213 30-Jul-96 Longterm 9.6 440 Poor W-1214 28-Apr-97 Drawdown 2.2 110 5.4 Fair W-1215 15-Aug-96 Drawdown 11.6 610 61 Fair W-1215 8-Oct-96 9.8 3,000 300 Poor Longterm W-1216 14-Aug-96 Drawdown 11.4 210 6.9 Good W-1216 15-Oct-96 160 5.4 Poor Longterm 11.1 W-1218 11-Nov-96 Drawdown 5.8 83 4.6 Fair W-1218 8-Jul-97 Longterm 4.8 210 12 Fair W-1219 27-May-97 Drawdown 0.4 2.5 0.63 Poor W-1220 13-Nov-96 Drawdown 20.3 2,600 120 Good W-1220 15-Jul-97 20 4,700 Fair Longterm 210

Flow Transmis-Hydraulic rate sivity conductivity Type of (Q) (T) (K)^c Data qualityd test^b (gpd/sq ft) Well Date (gpd/ft) (gpm) W-1221 27-Dec-96 Drawdown 3.1 29 2.9 Fair W-1222 Drawdown 6.1 430 43 Good 31-Oct-96 5 55 W-1224 22-May-97 Drawdown 11 Good W-1225 Drawdown 83 10 Good 31-Mar-97 4.1 W-1226 27-Feb-97 Drawdown 2.2 14 1.4 Excel W-1227 11-Apr-97 Drawdown 380 **48** Fair 15.1 W-1254 19-Nov-96 18.9 110 Fair Longterm 1,130 15 Fair W-1301 10-Mar-97 Longterm 4.7 120 W-1303 18-Mar-97 Longterm 7.8 490 21 Fair W-1304 2-Jul-97 Drawdown 0.7 2.6 0.52 Poor W-1306 Drawdown 24 30-Apr-97 2.8 1.2 Good W-1306 18-Jun-97 Longterm 1.6 54 2.7 Poor 110 W-1307 31-Jul-97 Drawdown 11.6 1,100 Good W-1308 Drawdown 6.5 150 5.1 Good 14-Aug-97 7-Oct-977 530 Fair W-1308 Longterm 4 18 W-1309 15-Oct-97 Drawdown 9.1 90 8.9 Fair 27.9 W-1310 10-Mar-97 Drawdown 53 Good 1,060 29-Oct-97 Drawdown 290 15 Good W-1311 12.2 7 100 Excel W-1401 11-Nov-97 Drawdown 6.8 W-1402 12-Dec-97 Drawdown 2.6 100 10.2 Fair Drawdown 20 Good TW-11 24-Jan-85 0.3 200 3,100 **TW-11A** 24-Jan-85 Drawdown 10.0 110 Fair **GSW-01** 11-Dec-85 Slug 0.0 72 0.2 Fair GSW-01A 14-Jul-86 Drawdown 13.4 12,000 790 Good Good **GSW-02** 17-Dec-85 Slug 0.0 240 10 **GSW-03** 23-Dec-85 Slug 0.0 510 41 Good **GSW-04** 19-Dec-85 Slug 0.0 17 0.9 Good **GSW-05** 12-Feb-86 0.0 99 9 Excel Slug 310 **GSW-06** 23-Iun-86 Drawdown 25.0 4,800 Good **GSW-06** 20.0 5,500 350 Good 16-Jun-87 Longterm **GSW-07** 3-Apr-86 Drawdown 4.3 230 23 Excel **GSW-08** 19-Nov-86 Drawdown 2.0 230 38 Good **GSW-09** 28-May-86 Drawdown 1.9 500 63 Poor 2,000 **GSW-10** 22-May-86 Drawdown 14.3 21,000 Good **GSW-11** 4.7 390 45 2-Jun-86 Drawdown Excel

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147 11		Type of	Flow rate (Q)	Transmis- sivity (T)	Hydraulic conductivity (K) ^c	Data
Well	Date	test ^b	(gpm)	(gpd/ft)	(gpd/sq ft)	quality ^d
GSW-12	7-Jun-86	Drawdown	0.8	51	11	Fair
GSW-13	4-Aug-86	Slug	0.0	110	13	Excel
GSW-13	8-Aug-86	Slug	0.0	62	7	Good
GSW-15	23-Feb-88	Drawdown	25.8	1,500	190	Good
GSW-208	8-May-86	Drawdown	1.9	440	80	Good
GSW-209	8-May-86	Drawdown	6.1	1,200	120	Good
GSW-215	4-Jun-86	Drawdown	1.9	220	40	Poor
GSW-216	16-Jan-92	Drawdown	10.5	3,500	440	Fair
GSW-266	20-Jun-86	Drawdown	2.1	470	72	Good
GSW-266	18-Nov-86	Drawdown	3.0	450	64	Good
GSW-266	18-Nov-86	Drawdown	4.7	410	59	Good
GSW-367	11-May-87	Drawdown	6.9	200	29	Fair
GSW-403-6	8-Dec-85	Slug	0.0	4	0.2	Good
GSW-442	23-Nov-87	Drawdown	1.2	32	4.6	Good
GSW-443	30-Nov-87	Drawdown	10.3	260	8.7	Good
GSW-444	28-Jan-88	Slug	0.0	9	0.86	Good
GSW-445	26-Jan-85	Drawdown	4.7	43	4.30	Fair
GEW-710	23-Sept-91	Step	36.0	4,800	220	Excel
GEW-816	15-Aug-92	Drawdown	39.0	12,000	1,100	Good
11H4	15-Jan-85	Drawdown	24.6	2,000	77	Good
11H4	19-Jan-85	Longterm	29.5	1,780	18	Good
11J4	10-Jun-88	Drawdown	17.0	1,000	15	Excel
11J4	14-Jun-85	Longterm	16.0	1,100	16	Good
13D1	9-Feb-85	Longterm	50.0	4,800	48	Excel

Table B-1. (Continued)

Footnotes appear on the following page.

- ^a The pumping test results were obtained by using the analytic techniques of Theis (1935), Cooper and Jacob (1946), Papadopulos and Cooper (1967), Hantush and Jacob (1955), Hantush (1960), or Boulton (1963). The particular method used is dependent on the character of the data obtained. The slug test results were obtained using the method of Cooper *et al.* (1967). (See references below.)
- b "DRAWDOWN" denotes 1-h pumping tests; "LONGTERM" denotes 24- to 48-h pumping tests; "STEP" denotes a step drawdown test, flow rate given is the maximum or final step.
- ^c K is calculated by dividing T by the thickness of permeable sediments intercepted by the sand pack of the well. This thickness is the sum of all sediments with moderate to high estimated conductivities determined from the geologic and geophysical logs of the well.
- d Hydraulic test quality criteria:
 - Excel: High confidence that type curve match is unique. Data are smooth and flow rate well controlled.
 - Good: Some confidence that curve match is unique. Data are not too "noisy." Well bore storage effects, if present, do not significantly interfere with the curve match. Boundary effects can be separated from properties of the pumped zone.
 - Fair: Low confidence that curve match is unique. Data are "noisy." Multiple leakiness and other boundary effects tend to obscure the curve match.
 - Poor: Unique curve match cannot be obtained due to multiple boundaries, well bore storage, uneven flow rate, or equipment problems. Usually, the test is repeated.

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Appendix C

1998 Ground Water Sampling Schedule

Weil numbersampling frequencyNext quarter sample dateMetals, RAD, etc. $(1-90)$ VOCsW-001O4-99E601W-002O3-99E601W-002O3-99E601W-002A4-98E601W-002A4-98E601W-002A1-98E601W-003A1-98E601W-004O3-99E601W-005A1-98E601W-006A4-98WCMGW-007O3-99E601W-008A4-98WGMGW-010AS1-98E601W-011S1-98E601W-012Q1-98E601W-017AE3-98E601W-019E4-98E601W-102O2-99E601W-103O3-99E601W-104Q1-98E601W-105Q1-98E601W-106E3-98E601W-107O2-99E601W-108O2-99E601W-104Q1-98E601W-105Q1-98E601W-106E3-98E601W-107O2-99E601W-108O2-99E601W-109E4-98E601W-106Q1-98E601W-107O2-99E601 <th></th> <th>1998 VOC</th> <th></th> <th></th> <th></th>		1998 VOC			
W-001 O $4-99$ $E601$ $W-001A$ O $4-99$ $E601$ $W-002$ O $3-99$ $E601$ $W-002$ O $3-99$ $E601$ $W-002$ A $4-99$ $E601$ $W-004$ O $4-99$ $E601$ $W-005$ A $1-98$ $E601$ $W-005A$ O $3-99$ $E601$ $W-007$ O $3-99$ $E601$ $W-008$ A $4-98$ $WGMG$ $E601$ $W-010A$ S $1-98$ $E601$ $W-017$ $W-017$ E $4-98$ $E601$ $W-017$ E $4-98$ $E601$ $W-017$ E $4-98$ $E601$ $W-019$ E $4-98$ $E601$ $W-101$ A $1-98$ $E601$ $W-102$ O $2-99$ $E601$ $W-103$ O $3-99$ $E601$ $W-106$ E $3-98$ $E601$		sampling			
W-001A O 4-99 Edd1 W-002 O 3-99 Ed01 W-002A A 4-98 Ed01 W-004 O 4-99 Ed01 W-005 A 1-98 Ed01 W-005 A 1-98 Ed01 W-005A O 3-99 Ed01 W-007 O 3-99 Ed01 W-008 A 4-98 WGMG Ed01 W-010A S 1-98 Ed01 W-011 S 1-98 Ed01 W-017 E 4-98 Ed01 W-017 E 4-98 Ed01 W-017 E 4-98 Ed01 W-101 A 1-98 Ed01 W-102 O 2-99 Ed01 W-103 O 3-99 Ed01 W-104 Q 1-98 Ed01 W-105 Q 1-98 Ed01 W-106 E 3-98 Ed01 W-107 O 2-99		frequency		(1-98)	VOCs
W-00203-99E601W-002AA4.98E601W-004O4.99E601W-005A1.98E601W-005AO3.99E601W-007O3.99E601W-008A4.98WGMGE601W-010AS1.98E601W-011S1.98E601W-012Q1.98E601W-017E4.98E601W-017AE3.98E601W-017AE3.98E601W-017AE3.98E601W-017AE4.98E601W-017AE4.98E601W-017AE3.99E601W-017AE3.99E601W-017AE3.98E601W-102O2.99E601W-103O3.99E601W-104Q1.98E601W-105Q1.98E601W-106E3.98E601W-107O2.99E601W-110Q1.98E601W-111S2.98E601W-113E4.98E601W-114A1.98E601W-115O3.99E601W-116Q1.98E601W-117E4.98E601W-118A1.98E601W-116Q1.98E601 <td< td=""><td></td><td></td><td></td><td></td><td>E601</td></td<>					E601
W-002A A 4-98 E601 W-004 O 4-99 E601 W-005 A 1-98 E601 W-005A O 3-99 E601 W-007 O 3-99 E601 W-008 A 4-98 WGMG E601 W-010A S 1-98 E601 W-011 S 1-98 E601 W-012 Q 1-98 E601 W-017 E 4-98 E601 W-017 Q 1-98 E601 W-102 O 2-99 E601 W-103 Q 1-98 E601 W-104 Q 1-98 E601 W-105 Q 1-98 E601 W-106 E 3-98 E601 W-107 O 2-99	W-001A	0	4-99		E601
W-004 O 4-99 E601 W-005 A 1-98 E601 W-005A O 3-99 E601 W-007 O 3-99 E601 W-008 A 4-98 WGMG E601 W-010A S 1-98 E601 W-011 S 1-98 E601 W-012 Q 1-98 E601 W-017 E 4-98 E601 W-017 Q 1-98 E601 W-102 O 2-99 E601 W-102 Q 1-98 E601 W-104 Q 1-98 E601 W-105 Q 2-99 E601 W-106 E 3-98 E601 W-10	W-002	0	3-99		E601
W-005A1-98E601W-005AO3-99E601W-007O3-99E601W-008A4-98WGMGE601W-010AS1-98E601W-011S1-98E601W-012Q1-98E601W-017E4-98E601W-017AE3-98E601W-017AE4-98E601W-017AE3-98E601W-017AQ2-99E601W-102O2-99E601W-103O3-99E601W-104Q1-98E601W-105Q1-98E601W-106E3-98E601W-107O2-99E601W-108O2-99E601W-110Q1-98E601W-113E4-98E601W-114A1-98E601W-115O3-99E601W-116Q1-98E601W-117E4-98E601W-118A1-98E601W-119Q1-98E601W-119Q1-98E601W-119Q1-98E601W-119Q1-98E601W-119Q1-98E601W-120Q1-98E601W-121Q1-98E601W-122A1-98E601W-12	W-002A	Α	4-98		E601
W-005AO3-99E601W-007O3-99E601W-008A4-98WGMGE601W-010AS1-98E601W-011S1-98E601W-012Q1-98E601W-017E4-98E601W-017E4-98E601W-019E4-98E601W-019E4-98E601W-102O2-99E601W-103O3-99E601W-104Q1-98E601W-105Q1-98E601W-106E3-98E601W-107O2-99E601W-110Q1-98E601W-111S2-98E601W-113E4-98E601W-114A1-98E601W-115O3-99E601W-116Q1-98E601W-117E4-98E601W-116Q1-98E601W-117Q1-98E601W-119Q1-98WGMGE601W-119Q1-98WGMGE601W-120Q1-98WGMGE601W-121Q1-98WGMGE601W-122A1-98WGMGE601W-122A1-98KGMGE601W-122A1-98KGMGE601W-122A1-98 <t< td=""><td>W-004</td><td>0</td><td>4-99</td><td></td><td>E601</td></t<>	W-004	0	4-99		E601
W-007O $3-99$ E001W-008A $4-98$ WGMGE601W-010AS $1-98$ E601W-011S $1-98$ E601W-012Q $1-98$ E601W-017E $4-98$ E601W-017E $4-98$ E601W-017E $4-98$ E601W-017A $1-98$ E601W-017Q $2-99$ E601W-101A $1-98$ E601W-102O $2-99$ E601W-103Q $1-98$ E601W-104Q $1-98$ E601W-105Q $1-98$ E601W-106E $3-99$ E601W-107O $2-99$ E601W-110Q $1-98$ E601W-111S $2-98$ E601W-113E $4-98$ E601W-114A $1-98$ E601W-115O $3-99$ E601W-114A $1-98$ E601W-115Q $1-98$ E601W-116Q $1-98$ E601W-117E $4-98$ E601W-118A $1-98$ E601W-119Q $1-98$ WGMGW-119Q $1-98$ WGMGW-119Q $1-98$ WGMGW-112Q $1-98$ WGMGW-122A $1-98$ WGMGW-124Q $1-98$ WGMGW-	W-005	Α	1-98		E601
W-008 A 4-98 WGMG E001 W-010A S 1-98 E601 W-011 S 1-98 E601 W-012 Q 1-98 E601 W-017 E 4-98 E601 W-017 Q 2-99 E601 W-101 A 1-98 E601 W-102 Q 1-98 E601 W-103 Q 1-98 E601 W-104 Q 1-98 E601 W-105 Q 1-98 E601 W-106 E 3-98 E601 W-107 Q 1-98 E601 W-110 Q 1-98 E601 W-113	W-005A	0	3-99		E601
W-010A S 1-98 E601 W-011 S 1-98 E601 W-012 Q 1-98 E601 W-017 E 4-98 E601 W-017 E 4-98 E601 W-017 E 4-98 E601 W-017 E 4-98 E601 W-019 E 4-98 E601 W-101 A 1-98 E601 W-102 O 2-99 E601 W-103 O 3-99 E601 W-104 Q 1-98 E601 W-105 Q 1-98 E601 W-106 E 3-98 E601 W-107 O 2-99 E601 W-108 O 2-99 E601 W-110 Q 1-98 E601 W-113 E 4-98 E601 W-114 A 1-98 E601 W-115 O <td>W-007</td> <td>0</td> <td>3-99</td> <td></td> <td>E601</td>	W-007	0	3-99		E601
W-011 S 1-98 E601 W-012 Q 1-98 E601 W-017 E 4-98 E601 W-017A E 3-98 E601 W-017 E 4-98 E601 W-017A E 3-98 E601 W-019 E 4-98 E601 W-101 A 1-98 E601 W-102 O 2-99 E601 W-103 O 3-99 E601 W-104 Q 1-98 E601 W-105 Q 1-98 E601 W-106 E 3-98 E601 W-107 O 2-99 E601 W-108 O 2-99 E601 W-110 Q 1-98 E601 W-113 E 4-98 E601 W-114 A 1-98 E601 W-115 O 3-99 E601 W-116 Q 1-98 E601 W-118 A 1-98 E601	W-008	Α	4-98	WGMG	E601
W-012Q1-98E601W-017E4-98E601W-017AE3-98E601W-019E4-98E601W-101A1-98E601W-102O2-99E601W-103O3-99E601W-104Q1-98E601W-105Q1-98E601W-106E3-98E601W-107O2-99E601W-108O2-99E601W-110Q1-98E601W-113E4-98E601W-114A1-98E601W-115O3-99E601W-116Q1-98E601W-117E4-98E601W-118A1-98E601W-119Q1-98WGMGE601W-120Q1-98WGMGE601W-121Q1-98WGMGE601W-122A1-98E601W-122A1-98E601	W-010A	S	1-98		E601
W-017 E 4-98 E601 W-017A E 3-98 E601 W-019 E 4-98 E601 W-101 A 1-98 E601 W-102 O 2-99 E601 W-103 O 3-99 E601 W-104 Q 1-98 E601 W-105 Q 1-98 E601 W-106 E 3-98 E601 W-107 O 2-99 E601 W-106 E 3-98 E601 W-107 O 2-99 E601 W-108 O 2-99 E601 W-110 Q 1-98 E601 W-111 S 2-98 E601 W-113 E 4-98 E601 W-114 A 1-98 E601 W-115 O 3-99 E601 W-116 Q 1-98 E601 W-118 A <td>W-011</td> <td>S</td> <td>1-98</td> <td></td> <td>E601</td>	W-011	S	1-98		E601
W-017A E 3-98 E601 W-019 E 4-98 E601 W-101 A 1-98 E601 W-102 O 2-99 E601 W-103 O 3-99 E601 W-104 Q 1-98 E601 W-105 Q 1-98 E601 W-106 E 3-98 E601 W-107 O 2-99 E601 W-108 O 2-99 E601 W-101 Q 1-98 E601 W-106 E 3-98 E601 W-107 O 2-99 E601 W-108 O 2-99 E601 W-110 Q 1-98 E601 W-113 E 4-98 E601 W-114 A 1-98 E601 W-116 Q 1-98 E601 W-118 A 1-98 E601 W-119 Q <td>W-012</td> <td>Q</td> <td>1-98</td> <td></td> <td>E601</td>	W-012	Q	1-98		E601
W-019E4-98E601W-101A1-98E601W-102O2-99E601W-103O3-99E601W-104Q1-98E601W-105Q1-98E601W-106E3-98E601W-107O2-99E601W-108O2-99E601W-110Q1-98E601W-111S2-98E601W-113E4-98E601W-114A1-98E601W-115O3-99E601W-116Q1-98E601W-118A1-98E601W-119Q1-98WGMGE601W-120Q1-98WGMGE601W-121Q1-98WGMGE601W-122A1-98E601	W-017	Ε	4-98		E601
W-101A1-98E601W-102O2-99E601W-103O3-99E601W-104Q1-98E601W-105Q1-98E601W-106E3-98E601W-107O2-99E601W-108O2-99E601W-110Q1-98E601W-111S2-98E601W-112O3-99E601W-114A1-98E601W-115O3-99E601W-116Q1-98E601W-117E4-98E601W-118A1-98WGMGW-119Q1-98WGMGW-120Q1-98E601W-121Q1-98E601W-122A1-98E601	W-017A	Ε	3-98		E601
W-102O2-99E601W-103O3-99E601W-104Q1-98E601W-105Q1-98E601W-106E3-98E601W-107O2-99E601W-108O2-99E601W-110Q1-98E601W-111S2-98E601W-113E4-98E601W-114A1-98E601W-115O3-99E601W-116Q1-98E601W-117E4-98E601W-118A1-98E601W-119Q1-98WGMGW-110Q1-98E601W-112Q1-98E601W-120Q1-98E601W-121Q1-98E601W-122A1-98E601	W-019	Ε	4-98		E601
W-103O $3-99$ EddW-104Q $1-98$ Edo1W-105Q $1-98$ Edo1W-106E $3-98$ Edo1W-107O $2-99$ Edo1W-108O $2-99$ Edo1W-110Q $1-98$ Edo1W-111S $2-98$ Edo1W-113E $4-98$ Edo1W-114A $1-98$ Edo1W-115O $3-99$ Edo1W-116Q $1-98$ Edo1W-117E $4-98$ Edo1W-118A $1-98$ Edo1W-119Q $1-98$ WGMGEdo1W-120Q $1-98$ WGMGEdo1W-121Q $1-98$ Edo1Edo1W-122A $1-98$ Edo1Edo1	W-101	Α	1-98		E601
W-104 Q 1-98 E601 W-105 Q 1-98 E601 W-106 E 3-98 E601 W-107 O 2-99 E601 W-108 O 2-99 E601 W-110 Q 1-98 E601 W-111 S 2-98 E601 W-113 E 4-98 E601 W-114 A 1-98 E601 W-115 O 3-99 E601 W-116 Q 1-98 E601 W-117 E 4-98 E601 W-118 A 1-98 E601 W-117 E 4-98 E601 W-118 A 1-98 E601 W-119 Q 1-98 WGMG E601 W-120 Q 1-98 E601 E601 W-121 Q 1-98 E601 E601 W-122 A 1-98 E60	W-102	0	2-99		E601
W-105 Q 1-98 E601 W-106 E 3-98 E601 W-107 O 2-99 E601 W-108 O 2-99 E601 W-110 Q 1-98 E601 W-111 S 2-98 E601 W-113 E 4-98 E601 W-114 A 1-98 E601 W-115 O 3-99 E601 W-116 Q 1-98 E601 W-117 E 4-98 E601 W-118 A 1-98 E601 W-119 Q 1-98 WGMG E601 W-119 Q 1-98 WGMG E601 W-120 Q 1-98 WGMG E601 W-121 Q 1-98 E601 E601 W-122 A 1-98 E601 E601	W-103	0	3-99		E601
W-106 E 3-98 E601 W-107 O 2-99 E601 W-108 O 2-99 E601 W-110 Q 1-98 E601 W-111 S 2-98 E601 W-113 E 4-98 E601 W-114 A 1-98 E601 W-115 O 3-99 E601 W-116 Q 1-98 E601 W-117 E 4-98 E601 W-118 A 1-98 E601 W-119 Q 1-98 WGMG E601 W-120 Q 1-98 WGMG E601 W-121 Q 1-98 E601 E601 W-122 A 1-98 E601 E601	W-104	Q	1-98		E601
W-107 Q 2-99 E601 W-108 Q 2-99 E601 W-110 Q 1-98 E601 W-111 S 2-98 E601 W-113 E 4-98 E601 W-114 A 1-98 E601 W-115 O 3-99 E601 W-116 Q 1-98 E601 W-117 E 4-98 E601 W-118 A 1-98 E601 W-119 Q 1-98 WGMG E601 W-120 Q 1-98 E601 E601 W-121 Q 1-98 E601 E601 W-122 A 1-98 E601 E601 </td <td>W-105</td> <td>Q</td> <td>1-98</td> <td></td> <td>E601</td>	W-105	Q	1-98		E601
W-108 O 2-99 E601 W-110 Q 1-98 E601 W-111 S 2-98 E601 W-113 E 4-98 E601 W-114 A 1-98 E601 W-115 O 3-99 E601 W-116 Q 1-98 E601 W-117 E 4-98 E601 W-118 A 1-98 E601 W-119 Q 1-98 KGMG E601 W-119 Q 1-98 KGMG E601 W-119 Q 1-98 KGMG E601 W-120 Q 1-98 KGMG E601 W-121 Q 1-98 KGMG E601 W-121 Q 1-98 KGM1 E601 W-122 A 1-98 E601 E601	W-106	Ε	3-98		E601
W-110Q1-98E601W-111S2-98E601W-113E4-98E601W-114A1-98E601W-115O3-99E601W-116Q1-98E601W-117E4-98E601W-118A1-98E601W-119Q1-98WGMGW-119Q1-98WGMGW-120Q1-98E601W-121Q1-98E601W-122A1-98E601	W-107	0	2-99		E601
W-111 S 2-98 E601 W-113 E 4-98 E601 W-114 A 1-98 E601 W-115 O 3-99 E601 W-116 Q 1-98 E601 W-117 E 4-98 E601 W-118 A 1-98 E601 W-119 Q 1-98 WGMG E601 W-120 Q 1-98 E601 E601 W-121 Q 1-98 E601 E601 W-122 A 1-98 E601 E601 W-120 Q 1-98 E601 E601 W-121 Q 1-98 E601 E601 W-122 A 1-98 E601 E601	W-108	0	2-99		E601
W-111 S 2-98 E601 W-113 E 4-98 E601 W-114 A 1-98 E601 W-115 O 3-99 E601 W-116 Q 1-98 E601 W-117 E 4-98 E601 W-118 A 1-98 E601 W-119 Q 1-98 WGMG E601 W-120 Q 1-98 E601 E601 W-121 Q 1-98 E601 E601 W-122 A 1-98 E601 E601 W-120 Q 1-98 WGMG E601 W-121 Q 1-98 E601 E601 W-122 A 1-98 E601 E601	W-110	Q	1-98		E601
W-114 A 1-98 E601 W-115 O 3-99 E601 W-116 Q 1-98 E601 W-117 E 4-98 E601 W-118 A 1-98 E601 W-119 Q 1-98 WGMG E601 W-120 Q 1-98 E601 E601 W-121 Q 1-98 E601 E601 W-122 A 1-98 E601 E601	W-111	S	2-98		E601
W-114 A 1-98 E601 W-115 O 3-99 E601 W-116 Q 1-98 E601 W-117 E 4-98 E601 W-118 A 1-98 E601 W-119 Q 1-98 WGMG E601 W-120 Q 1-98 E601 E601 W-121 Q 1-98 E601 E601 W-122 A 1-98 E601 E601	W-113	Ε	4-98		
W-115O $3-99$ E601W-116Q $1-98$ E601W-117E $4-98$ E601W-118A $1-98$ E601W-119Q $1-98$ WGMGE601W-120Q $1-98$ E601W-121Q $1-98$ E601W-122A $1-98$ E601	W-114	Α	1-98		
W-116Q1-98E601W-117E4-98E601W-118A1-98E601W-119Q1-98WGMGE601W-120Q1-98E601W-121Q1-98E601W-122A1-98E601	W-115	0	3-99		
W-117 E 4-98 E601 W-118 A 1-98 E601 W-119 Q 1-98 WGMG E601 W-120 Q 1-98 E601 E601 W-121 Q 1-98 E601 E601 W-122 A 1-98 E601 E601	W-116	Q	1-98		
W-118 A 1-98 E601 W-119 Q 1-98 WGMG E601 W-120 Q 1-98 E601 E601 W-121 Q 1-98 E601 E601 W-122 A 1-98 E601 E601	W-117		4-98		
W-119 Q 1-98 WGMG E601 W-120 Q 1-98 E601 W-121 Q 1-98 E601 W-122 A 1-98 E601	W-118	Α	1-98		
W-120 Q 1-98 E601 W-121 Q 1-98 E601 W-122 A 1-98 E601	W-119	Q	1-98	WGMG	
W-121 Q 1-98 E601 W-122 A 1-98 E601	W-120		1-98	_	
W-122 A 1-98 E601	W-121		1-98		
	W-122		1-98		
		Ε			

Table C-1. 1998 LLNL Livermore Site	ground water sampling schedule.
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Well number	1998 VOC sampling frequency	Next quarter sample date	Metals, RAD, etc. (1-98)	VOCs
W-141	Е	2-98		E601
W-142	Α	2-98		E601
W-143	S	2-98		E601
W-146	Α	4-98		E601
W-147	Α	4-98		E601
W-148	0	4-99		E601
W-151	Q	1-98		E601
W-201	0	4-99		E601
W-202	Ε	4-98		E601
W-203	Ε	2-98		E601
W-204	0	1-99	WGMG	E601
W-205	Q	1-98		E601
W-206	Q	1-98		E601
W-207	Q	1-98		E601
W-210	Α	4-98	E906	E601
W-212	Ε	4-98		E601
W-213	Ο	3-99		E601
W-214	0	2-99		E601
W-217	Q	1-98		E601
W-219	Q	1-98		E601
W-220	Α	1-98		E601
W-221	0	3-99	WGMG	E601
W-222	Q	1-98		E601
W-223	Α	1-98		E601
W-224	Α	1-98		E601
W-225	S	2-98		E601
W-226	0	3-99		E601
W-251	Q	1-98		E601
W-252	0	2-99		E601
W-253	0	4-99		E601
W-254	Q	1-98		E601
W-255	Q	1-98		E601
W-256	0	1-99		E601
W-257	Q	1-98	E906	E601
W-258	0	2-99		E601
W-259	Q	1-98	E906	E601

Well number	1998 VOC sampling frequency	Next quarter sample date	Metals, RAD, etc. (1-98)	VOCs
W-260	S	1-98		E601
W-261	Ε	3-98		E601
W-263	Q	1-98		E601
W-264	Α	2-98		E601
W-265	0	2-99		E601
W-267	S	1-98		E601
W-268	Α	2-98		E601
W-269	Α	4-98		E601
W-270	0	1-99		E601
W-271	Q	1-98		E601
W-272	S	1-98		E601
W-273	0	4-99		E601
W-274	Q	1-98		E601
W-275	S	2-98		E601
W-276	Α	3-98		E601
W-277	Α	1-98		E601
W-290	Ε	4-98		E601
W-291	0	2-99		E601
W-292	Α	1-98		E601
W-293	Ε	2-98		E601
W-294	0	2-99		E601
W-301	0	4-99		E601
W-302	0	3-99		E601
W-303	Α	1-98		E601
W-304	0	3-99		E601
W-305	Q	1-98		E601
W-306	0	3-99		E601
W-307	S	2-98		E601
W-308	Ε	4-98		E601
W-310	Ε	3-98		E601
W-311	Q	1-98		E601
W-312	A	2-98		E601
W-313	Α	1-98		E601
W-315	Q	1-98		E601
W-316	Q	1-98		E601
W-317	A	4-98		E601

Well number	1998 VOC sampling frequency	Next quarter sample date	Metals, RAD, etc. (1-98)	VOCs
W-318	0	2-99		E601
W-319	Ε	4-98		E601
W-320	Α	1-98		E601
W-321	0	1-99		E601
W-322	Q	1-98		E601
W-323	Q	1-98		E601
W-324	Ε	2-98		E601
W-325	Ε	4-98		E601
W-353	S	2-98		E601
W-354	Q	1-98		E601
W-355	Q	1-98		E601
W-356	Q	1-98		E601
W-359	Q	1-98		E601
W-360	S	2-98		E601
W-361	Q	1-98		E601
W-362	0	2-99		E601
W-363	Q	1-98	WGMG	E601
W-364	Q	1-98		E601
W-365	0	3-99		E601
W-366	0	2-99		E601
W-368	Α	1-98		E601
W-369	Q	1-98		E601
W-370	Α	2-98		E601
W-371	Ε	3-98		E601
W-372	Ε	3-98		E601
W-373	0	4-99	WGMG	E601
W-375	Q	1-98		E601
W-376	0	2-99		E601
W-377	0	2-99		E601
W-378	0	4-99		E601
W-379	Α	2-98		E601
W-380	Ε	4-98		E601
W-401	Ε	2-98		E601
W-402	Ε	4-98		E601
W-403	Ε	3-98		E601
W-404	Q	1-98		E601

Well number	1998 VOC sampling frequency	Next quarter sample date	Metals, RAD, etc. (1-98)	VOCs
W-405	Q	1-98		E601
W-406	Α	1-98		E601
W-407	Q	1-98		E601
W-409	Α	2-98		E601
W-410	Q	1-98		E601
W-411	Q	1-98		E601
W-412	Α	1-98		E601
W-413	Α	1-98		E601
W-414	Ε	3-98		E601
W-416	Ε	2-98		E601
W-417	Ε	2-98		E601
W-418	Α	4-98		E601
W-419	Q	1-98		E601
W-420	Α	2-98		E601
W-421	Q	1-98		E601
W-422	Α	3-98		E601
W-423	Q	1-98		E601
W-424	S	2-98		E601
W-446	Α	4-98		E601
W-447	Α	3-98		E601
W-448	0	2-99		E601
W-449	Α	4-98		E601
W-450	Α	1-98		E601
W-451	e	1-98		E601
W-452	Ε	4-98		E601
W-453	Ε	3-98		E601
W-454	S	2-98		E601
W-455	Α	1-98		E601
W-456	0	2-99		E601
W-458	Ε	4-98		E601
W-459	Α	4-98		E601
W-460	0	4-99		E601
W-461	Α	2-98		E601
W-462	0	3-99		E601
W-463	Α	1-98		E601
W-464	Α	3-98		E601

Well number	1998 VOC sampling frequency	Next quarter sample date	Metals, RAD, etc. (1-98)	VOCs
W-481	Q	1-98		E601
W-482	Α	4-98		E601
W-483	S	2-98		E601
W-484	0	3-99		E601
W-485	Ο	2-99		E601
W-486	Α	1-98	E906	E601
W-487	Α	1-98		E601
W-501	S	2-98		E601
W-502	0	2-99		E601
W-503	0	2-99		E601
W-504	0	4-99		E601
W-505	0	2-99		E601
W-506	S	1-98		E601
W-507	Ε	3-98		E601
W-509	S	1-98		E601
W-510	Ε	3-98		E601
W-511	0	3-99		E601
W-512	0	4-99		E601
W-513	Α	2-98		E601
W-514	0	2-99		E601
W-515	Q	1-98		E601
W-516	Ε	4-98		E601
W-517	Q	1-98		E601
W-519	0	3-99		E601
W-521	Α	4-98		E601
W-551	S	2-98		E601
W-552	0	4-99		E601
W-553	Ε	4-98		E601
W-554	0	2-99		E601
W-555	0	2-99		E601
W-556	0	4-99		E601
W-557	Ε	3-98		E601
W-558	Q	1-98		E601
W-559	Ε	3-98		E601
W-560	0	4-99		E601
W-561	Е	2-98		E601

Well number	1998 VOC sampling frequency	Next quarter sample date	Metals, RAD, etc. (1-98)	VOCs
W-562	А	4-98		E601
W-563	Ε	2-98		E601
W-564	Q	1-98		E601
W-565	Ε	4-98		E601
W-567	Α	1-98		E601
W-568	S	1-98		E601
W-569	S	1-98		E601
W-570	0	2-99		E601
W-571	0	2-99		E601
W-591	Ε	3-98		E601
W-592	0	3-99		E601
W-593	0	4-99		E601
W-594	0	1-99		E601
W-604	S	2-98		E601
W-605	Α	3-98		E601
W-606	S	1-98		E601
W-607	0	2-99		E601
W-608	0	1-99		E601
W-611	S	2-98		E601
W-612	0	2-99		E601
W-613	Α	1-98		E601
W-615	Α	2-98		E601
W-616	0	4-99		E601
W-617	Α	3-98		E601
W-618	Q	1-98		E601
W-619	0	3-99		E601
W-622	Q	1-98		E601
W-651	Q	1-98		E601
W-652	0	1-99		E601
W-653	Q	1-98		E601
W-654	S	1-98		E601
W-702	S	2-98		E601
W-705	S	1-98		E601
W-706	0	3-99		E601
W-750	Q	1-98		E601
W-714	Α	4-98		E601

Well number	1998 VOC sampling frequency	Next quarter sample date	Metals, RAD, etc. (1-98)	VOCs
W-901	Q	1-98		E601
N-902	Q	1-98		E601
W-905	0	4-99		E601
W-908	Q	1-98		E601
W-909	Q	1-98		E601
W-911	Q	1-98		E601
W-912	Q	1-98		E601
W-913	Q	1-98		E601
W-1001	Q	1-98		E601
W-1002	Α	2-98		E601
W-1003	0	4-99		E601
W-1005	S	1-98		E601
W-1006	Q	1-98		E601
W-1007	Α	1-98		E601
W-1008	Ε	4-98		E601
W-1010	0	4-99		E601
W-1011	0	2-99		E601
W-1012	0	4-99	WGMG	E601
W-1013	Α	3-98		E601
W-1014	Q	1-98		E601
W-1101	0	2-99		E601
W-1105	0	1-99		E601
W-1106	S	1-98		E601
W-1107	Q	1-98		E601
W-1108	Q	1-98		E601
W-1110	S	1-98		E601
W-1112	Q	1-98		E601
W-1113	S	1-98		E601
W-1115	Q	1-98		E601
W-1117	Q	1-98		E601
W-1118	S	2-98		E601
W-1201	Q	1-98		E601
W-1202	Q	1-98		E601
W-1203	Q	1-98		E601
W-1204	Q	1-98		E601
W-1205	Q	1-98		E601

Well number	1998 VOC sampling frequency	Next quarter sample date	Metals, RAD, etc. (1-98)	VOCs
W-1207	Q	1-98		E601
W-1209	Q	1-98		E601
W-1210	S	1-98		E601
W-1211	Q	1-98		E601
W-1212	Q	1-98		E624
W-1214	S	2-98		E601
W-1217	Q	1-98		E601
W-1218	Q	1-98		E601
W-1219	Q	1-98		E601
W-1220	Q	1-98		E601
W-1221	Q	1-98		E601
W-1222	Q	1-98		E601
W-1223	Q	1-98	E906	E601
W-1224	Q	1-98		E601
W-1225	Q	1-98		E601
W-1226	Q	1-98		E601
W-1227	Q	1-98		E601
W-1250	Q	1-98		E601
W-1251	S	2-98		E601
W-1252	S	2-98		E601
W-1253	Q	1-98		E601
W-1254	S	2-98		E601
W-1255	Q	1-98		E601
W-1304	Q	1-98		E601
W-1401	Q	1-98		E601
W-1402	Q	1-98		E601
TW-11	0	2-99		E601
TW-11A	Α	4-98		E601
ГW-21	Α	4-98		E601
11 J2	Α	4-98		E601
I1C1	Ε	1-98		E601
14A11	0	4-99		E601
14A3	Α	3-98		E601
14B1	0	3-99		E601
14B4	0	2-99		E601
14C1	0	3-99		E602

Well number	1998 VOC sampling frequency	Next quarter sample date	Metals, RAD, etc. (1-98)	VOCs
14C2	0	3-99		E602/14d
14C3	Α	4-99		E601
14H1	Ε	2-98		E602/14d
18D1	Ε	2-98		E602/14d
7D2	0	4-98		E602/14d
GEW-710	Α	4-98		E602/14d
GSW-006	Α	4-98	E602	E602/14d
GSW-007	0	4-99		E602/14d
GSW-008	0	4-99	E602	E601
GSW-009	Q	1-98	E602	E601
GSW-011	S	1-98		E601
GSW-013	0	4-99	E602	E624
GSW-215	Q	1-98	E602	E601
GSW-266	Α	4-98	E602	E601
GSW-326	Ε	4-98		E601
GSW-367	S	1-98		E601
GSW-442	Α	4-98		E601
GSW-443	Α	2-98	2-98	
GSW-444	Ο	2-99		E601

Notes:

- O = Odd years.
- A = Annual.
- S = Semiannual.
- **Q** = **Quarterly**.
- **E** = Even years.

E601 = EPA Method 601 for purgeable halocarbons.

WGMG = Water Guidance and Monitoring Group.

E906 = EPA Method 906 for tritium.

E624 = EPA Method 624 for VOCs.

E602 = EPA Method 602 for aromatic volatile compounds.

Appendix D

1997 Drainage Retention Basin Annual Monitoring Program Summary

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1997 Drainage Retention Basin Annual Monitoring Program Summary

This Appendix summarizes the 1997 LLNL Operations and Regulatory Affairs Division routine maintenance activities, maintenance monitoring, and discharge data for the Drainage Retention Basin (DRB). The DRB, located in the central portion of the Livermore Site (Fig. D-1), is an artificial water body with about 43 acre-ft (approximately 1.4×10^7 gal) capacity. It was designed to receive storm water runoff and treated ground water.

Discharge samples are collected at the first planned release of the rainy season and, at a minimum, in conjunction with one additional storm water monitoring event, as requested by the Regional Water Quality Control Board-San Francisco Bay Region (RWQCB-SF). Release water samples are collected at sample location CDBX and are compared with the LLNL Arroyo Las Positas outfall samples collected at sample location WPDC (Fig. D-1). Release samples are used to determine compliance with current discharge limits. Discharge limits are established in the CERCLA *Record of Decision for the Lawrence Livermore National Laboratory, Livermore Site* (Department of Energy, 1992) and the *Explanation of Significant Differences for Metals Discharge Limits at the Lawrence Livermore National Laboratory, Livermore Site* (Berg, 1997).

Weekly maintenance field monitoring measurements are conducted at sample locations CDBA, CDBC, CDBD, CDBE, CDBF, CDBJ, CDBK, and CDBL (Fig. D-2). Monthly, quarterly, semi-annual and annual maintenance samples are collected at sampling location CDBE (Fig. D-2). Maintenance samples are used as the basis for management decisions regarding the DRB. Management action levels (MALs) are specified in the *Drainage Retention Basin Management Plan, Lawrence Livermore National Laboratory* (Limnion Corp., 1991). The MAL is the concentration at which corrective management responses should be implemented. In most cases, short-term variances outside the normal range are not significant, and management response is required only if the objective is substantially exceeded.

Complete analytical results of samples collected within the basin and from releases are reported in the LLNL Livermore Site Project Quarterly Self-Monitoring Reports for 1997.

D.1. Drainage Retention Basin Maintenance Monitoring

Samples collected during 1997 within the DRB at sample location CDBE did not meet the MALs for ammonia, chemical oxygen demand, dissolved oxygen, fecal coliform, nitrate (as nitrogen), pH, temperature, total dissolved solids, total phosphorus (as phosphorus) and turbidity. Results of the October 15, 1997, CDBE radiological analyses are still pending and will be reported in the first quarterly self-monitoring report of calendar year 1998. A summary of these constituents is provided in table D-1.

Analysis	Management action level	Maximum value	Minimum value	Samples exceeding MALs/ samples collected
Ammonia Nitrogen (mg/L)	>0.1	0.44	< 0.02	03/11
Chemical Oxygen Demand (mg/L)	>20	52.2	27	04/04
Dissolved Oxygen (mg/L)	<80% or < 5	14.9	3.4	11/39
Fecal Coliform (MPN)	>400	1,600	<2	01/04
Nitrate (as N) (mg/L)	>0.2	0.84	<0.1	08/11
pH (units)	<6.0 and >9.0	9.2	7.24	01/11
Temperature (degrees F)	<15 and > 26	26.7	6.3	15/39
Total Dissolved Solids (mg/L)	>400	463	200	03/11
Total Phosphorous (as P) (mg/L)	>0.02	0.66	0.2	29/29
Turbidity (meters)	<0.914	1.372	0.25	27/32

MPN = Most Probable Number.

Ammonia continued to occasionally exceed its MAL. Ammonia is an indication of anaerobic activity occurring within the DRB which was supported by several low dissolved oxygen readings obtained in 1997. The dissolved oxygen readings are believed to be low for two reasons. The first reason is the pumps to circulate the DRB were left off longer than usual in an effort to increase water clarity. Water clarity, measured by turbidity, is typically low in the winter when storm runoff increases sediment load. Water clarity was successfully improved with turbidity levels coming near or within the MAL for the first time since 1994. However, once the recirculation pumps were turned on to increase dissolved oxygen levels, water clarity began to decrease. The second reason for low dissolved oxygen readings was due to mechanical problems with the dissolved oxygen meter. Comparison sampling with rental meters indicate the dissolved oxygen readings using LLNL's ICM might be as much as 2 mg/L low.

Chemical oxygen demand was above the MAL for the first time during 1997. The maximum value occurred during first quarter monitoring. Heavy rains and runoff occurring last year at the end of December 1996 and beginning of January 1997 most likely introduced organic material into the DRB increasing oxygen demand. Oxygen demand within the DRB decreased over the course of the year. Fecal coliform measured high for the first time since the DRB began to operate during the first quarter monitoring event. High total coliform (1,600 Most Probable Number) was also reported in this sample. Subsequent coliform samples were substantially lower, below the MAL.

Total phosphorous continued to be above the MAL throughout 1997. Phosphorous concentration increases were correlated with times when Treatment Facility D (TFD) was diverted into the DRB to accommodate down stream construction activities. Nitrate as nitrogen concentrations also continued to exceed the MAL during 1997.

Although nutrient levels have been high since 1994, chlorophyll "a", which indicates the level of algae growth, remains well below the 10 mg/L MAL, ranging from <0.0013 mg/L to

0.0151 mg/L. Though the chlorophyll "a" levels did not increase significantly from last year, algae growth was visibly evident in 1997 for the first time since the fall of 1995 when toxicity tests indicated the water within the DRB had a toxic effect on the algae <u>Selanastrum</u> capricornutum.

In March 1995, LLNL began monitoring for active ingredients of commonly used herbicides which could inhibit algae growth. Quarterly monitoring in 1996 detected low levels of Bromocil (13 to 36 μ g/L) and Diuron (7 to 23 μ g/L). During the first part of 1997 both Diuron and Bromocil levels were reduced below detection levels. This coincided with the increase of algae growth in the DRB. LLNL began a toxicity study in August of 1996 that roughly followed the procedures of a Toxicity Reduction Evaluation (TRE). The toxicity study was completed in the fall of 1997. The results of the toxicity study indicate the toxicity in the DRB was not a result of metal concentrations but resulted from organic constituents. Further study confirmed a strong toxicity effect from concentrations of Diuron and Bromocil found in the DRB in March 1997 and a weak toxic effect from leachate derived from tanbark spread around the DRB. These studies indicate that the introduction of Bromocil and Diuron occurring in the fall of 1995 resulting from upstream use of these pesticides was most likely the caused the algae growth inhibition.

During September 1995, LLNL conducted chronic toxicity tests on algae and fish to determine if the lack of algae growth was the result of factors other than turbidity. The results of the test using the algae Selanastrum capricornutum, indicated algae growth inhibition occurred at a 12.5% concentration of DRB water. The test using the fathead minnow, Pimephales promelas showed no chronic toxicity in up to 100% DRB water. Follow-up chronic toxicity testing in September 1996 indicated that DRB water had no chronic toxicity to the fathead minnow, and actually had a growth inducing effect on the algae. However, the results contradicted what was observed regarding the lack of algae growth in the DRB. Three species were used in the chronic toxicity testing conducted in October 1997, Selanastrum capricornutum, Ceriodaphnia dubia, and Pimephales promelas. The results of these tests showed no toxic effects on the Pimephales promelas and Ceriodaphnia dubia. However, Selanastrum capricornutum showed greater than 16 toxic units for growth with a No Observable Effect Concentration (NOEC) at <6.25% concentration of DRB water and the Lowest Observable Effect Concentration (LOEC) at a 6.25% concentration of DRB water. This observed toxicity coincides with re-introduction of Diuron (33 micrograms per liter) detected in samples collected at CDBE in October. The introduction of Diuron came from the use of KARMEX DF herbicide for weed control in an upgradient storm water drainage swale.

Semiannual and annual maintenance sampling was conducted during April and October 1997. Quarterly sampling was conducted in January, April, July, and October. Results for oil and grease, volatile organic compounds, semi-volatile organic compounds, total petroleum hydrocarbons, polynuclear aromatic compounds, ethylene dibromide and total organic carbon all met their MALs. Radiological results for the October sample are still pending. Acute fish toxicity test using the fathead minnow (95% survival) met the 90% survival MAL.

In 1997, LLNL began quarterly microbiological monitoring as a tool to evaluate the nature and health of the DRB aquatic community as an expression of water quality. LLNL also began semi-annual biological monitoring to evaluate the impact the operation of the DRB has on surrounding and downstream ecosystems.

D-2. Drainage Retention Basin Discharge Monitoring

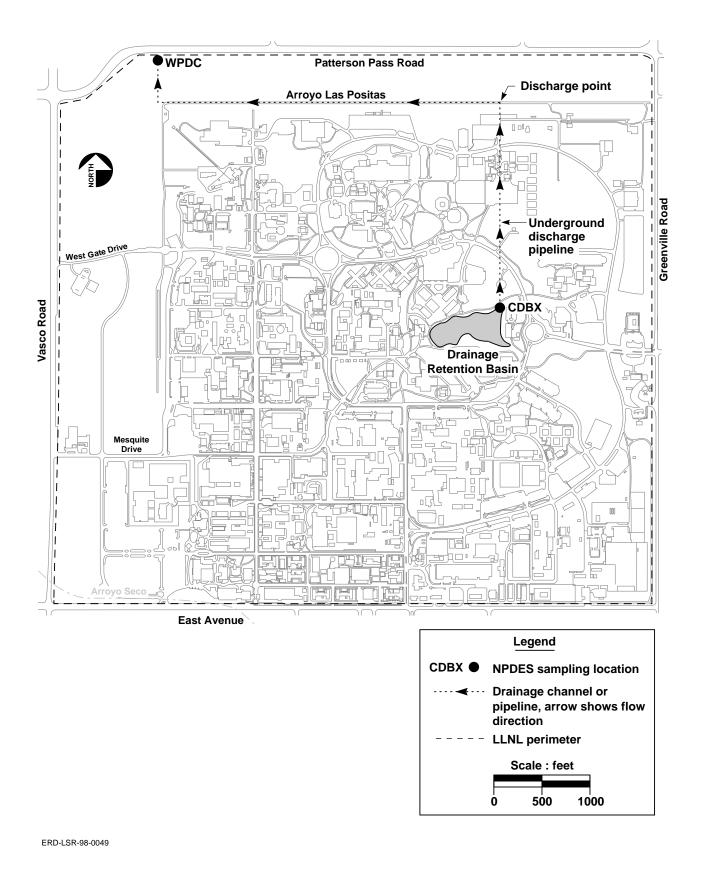
Four DRB release samples were collected in 1997 representing 37.6 million gallons of water discharged. Three releases occurred during the wet weather season (October 1 through May 31) totaling 30.1 million gallons. One discharge occurred during the dry weather (June 1 through September 30) totaling 7.5 million gallons. Discharges during 1997 occurred from the DRB in January, February, September, November, and December. The largest single day discharge occurred on January 2, 1997 (3.5 million gallons).

The dry season release occurred on September 17, 1997. The three wet season releases occurred January 15, November 26, and December 8, 1997. The September 17, 1997 release was necessary because of water discharged to the DRB from TFD to allow for construction activities in the discharge pipeline from the DRB. TFD discharges were diverted into the DRB until the construction activities were complete. The November 26, 1996 release was a manual release and was the first of the rainy season. The release was necessary to prevent flooding of areas around the DRB and the upstream channels. The January 15, 1996, and December 8, 1997, samples were collected from storm water overflowing the lowered weir gate and occurred concurrent with 1996/97 and 1997/98 storm water sampling events. Samples were collected during this release from locations CDBX and WPDC. Dry season (April 1–November 30) limits were used to evaluate the compliance of the September and November releases, wet weather limits (December 1–March 31) were used to evaluate the compliance of the January and December releases.

All samples collected from CDBX were below discharge limits except total petroleum hydrocarbons diesel (81 mg/L). The concentration of diesel fuel exceeded the discharge limit of 50 mg/L. Sample results are still pending for radiological samples. Diuron was found in samples collected at both CDBX (40 μ g/L) and WPDC (42 μ g/L). Diuron was also seen in influent sample coming on to the LLNL site (11 μ g/L and 47 μ g/L).

D-3. References

- Berg, L., E. Folsom, M. Dresen, R. Bainer, A. Lamarre (Eds.) (1997), Explanation of Significant Differences for Metals Discharge Limits at the Lawrence Livermore National Laboratory Livermore Site, Lawrence Livermore National Laboratory, Livermore, Calif. (UCRL-AR-125927).
- Lamarre, A., J. Littlejohn (1997), Letter from Lamarre to Remedial Project Managers, LLNL Livermore Site Remedial Project Managers' Meeting Summary and Quarterly Self-Monitoring Reports, dated May 23, 1997, August 29, 1997, November 26, 1997.
- The Limnion Corporation (1991), Drainage Retention Basin Management Plan: Lawrence Livermore National Laboratory, Concord, Calif.
- U.S. Department of Energy (DOE) (1992), *Record of Decision for the Lawrence Livermore National Laboratory, Livermore Site*, Lawrence Livermore National Laboratory, Livermore, Calif. (UCRL-AR-109105).





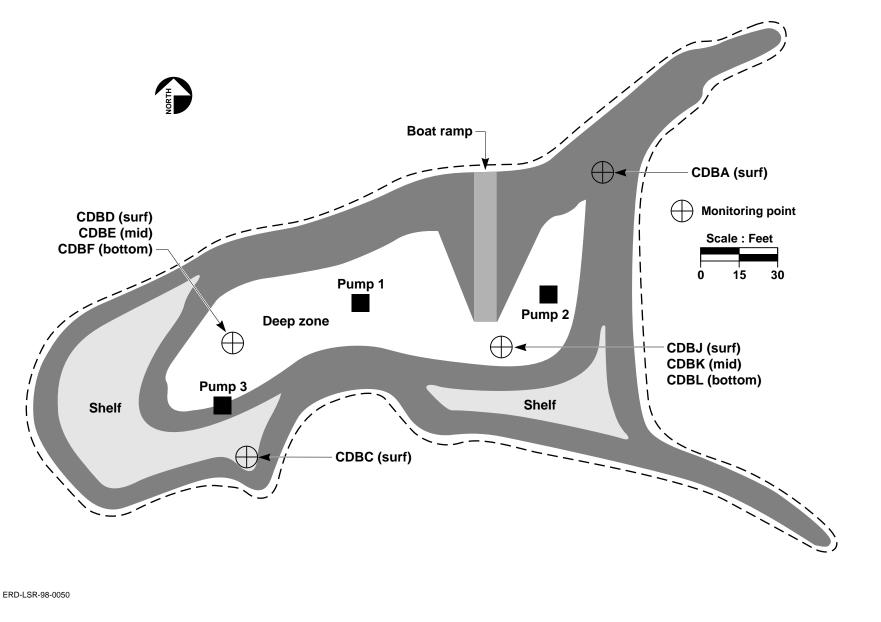


Figure D-2. Monitoring locations in the Drainage Retention Basin.